

Optical networks and equipment



www.ces.net



czechlight.cesnet.cz

Jan Radil

CESNET z.s.p.o.

- ◆ CESNET (Czech Educational and Scientific NETwork) - NREN in the Czech Republic
- ◆ Established as a legal entity – not for profit
- ◆ Association of Legal Entities (z.s.p.o.) in 1996
 - 27 Universities
 - Czech Academy of Sciences
- ◆ 52 staff members in Praha
- ◆ More than 150 part-time universities and Academy of Sciences staff working on projects

Participation on International Projects

- ◆ (GÉANT), GN2
- ◆ 6NET
- ◆ EGEE
- ◆ (SCAMPI), LOBSTER
- ◆ SEEFIRE
- ◆ PORTA OPTICA
- ◆ LUCIFER

Optical networks and equipment

CESNET z.s.p.o. - Funding

- ◆ Research plan: „Optical High Speed National Research Network and its New Applications“
- ◆ 2004 – 2010
- ◆ Funded by Ministry of Education, Youth and Sports of the Czech republic and Association Members - budged approx. 12 MEuro/year
- ◆ Research activity annual report is available www.ces.net/doc/2005/

CzechLight

- ◆ An experimental and breakable optical network
- ◆ For disruptive tests, not 24/7 NOC (Network Operation Centre)
- ◆ CzechLight optical equipment
- ◆ Parallel infrastructure together with a production network CESNET2

Motivations

- ◆ Utilization of dark fibres – Customer Empowered Fibre networks (the first DF line lighted in 1999, 2.5 Gb/s PoS, 327 km with 3 OEO regenerators)
- ◆ Now CESNET has 4200 km of leased dark fibres
- ◆ Cost effective deployment of multigigabit DF lines (N x 1 GE, N x 10 GE) with pluggable DWDM transceivers – GBIC, SFP, XENPAK, XFP
- ◆ Lack of optical equipment suitable for NRENs
- ◆ Development of our own optical amplifiers (and other equipment)
- ◆ Repeaterless or Nothing-in-line (NIL) approach, where possible and practicable

A little bit of History (1)

- ◆ Back to Antiquity (mirrors, fire beacons, smoke signals) [Agr]
- ◆ The end 18th century with lamps, flags
- ◆ 1792, Claude Chappe with mechanical „optical“ telegraph
- ◆ 1830 – the advent of telegraphy
- ◆ 1866 – the first transatlantic cable went into operation
- ◆ 1876 – the invention of telephone (A.G.Bell, U.S. Patent No. 174 465)
- ◆ 1940 – 3 MHz coax-cable system (repeater spacing 1 km)
- ◆ 1948 – 4 GHz microwave system
- ◆ 1960 – the invention of laser (suitable transmission medium?)
- ◆ 1960s – optical fibre (1000 dB/km)

A little bit of History (2)

- ◆ 1970 – fibres with losses 20 dB/km
- ◆ Evolution of optical communication systems
- ◆ 850 nm, 1310 nm, 1550 nm, TDM, WDM, CWDM, DWDM
- ◆ 1980 – 45 Mb/s (1st generation)
- ◆ 1980s – 1310 nm, 1 dB/km, 100 Mb/s, multi-mode fibres
- ◆ Late 1980s – 2 Gb/s, single mode fibres, repeater spacing 50 km (2nd generation)
- ◆ 1990s – 1550 nm (problem with lasers, dispersion of fibres), 2.5 Gb/s or 10 Gb/s (3rd generation)
- ◆ 1990s - DWDM, optical amplification (4th generation)
- ◆ Today – 10 and 40 G waves, 160 channels ie x Tb/s, thousands of kilometers

A little bit of Theory (1)

- ◆ All electromagnetic phenomena are described by Maxwell's equations
- ◆ An optical fibre (silica or non-silica) is a nonconducting medium without free charges

$$\nabla \times \mathbf{E} = - \frac{\partial \mathbf{B}}{\partial t} \quad \nabla \cdot \mathbf{D} = 0$$

$$\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t} \quad \nabla \cdot \mathbf{B} = 0$$

$$\mathbf{D} = \varepsilon_0 \mathbf{E} + \mathbf{P}$$

$$\mathbf{B} = \mu_0 \mathbf{H}$$

- ◆ \mathbf{E}, \mathbf{H} : electric/magnetic fields vectors
- ◆ \mathbf{D}, \mathbf{B} : electric/magnetic flux densities
- ◆ \mathbf{P} : induced electric polarization
- ◆ \mathbf{M} : induced magnetic polarization = 0
- ◆ ε_0 : the vacuum permittivity
- ◆ μ_0 : the vacuum permeability

A little bit of Theory (2)

◆ Div, grad, rot, Nabla, Laplace

$$\nabla = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right) \quad \nabla \cdot \nabla = \Delta \quad \Delta = \nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$$

$$\nabla \cdot f = \left(\frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right) = \text{grad } f$$

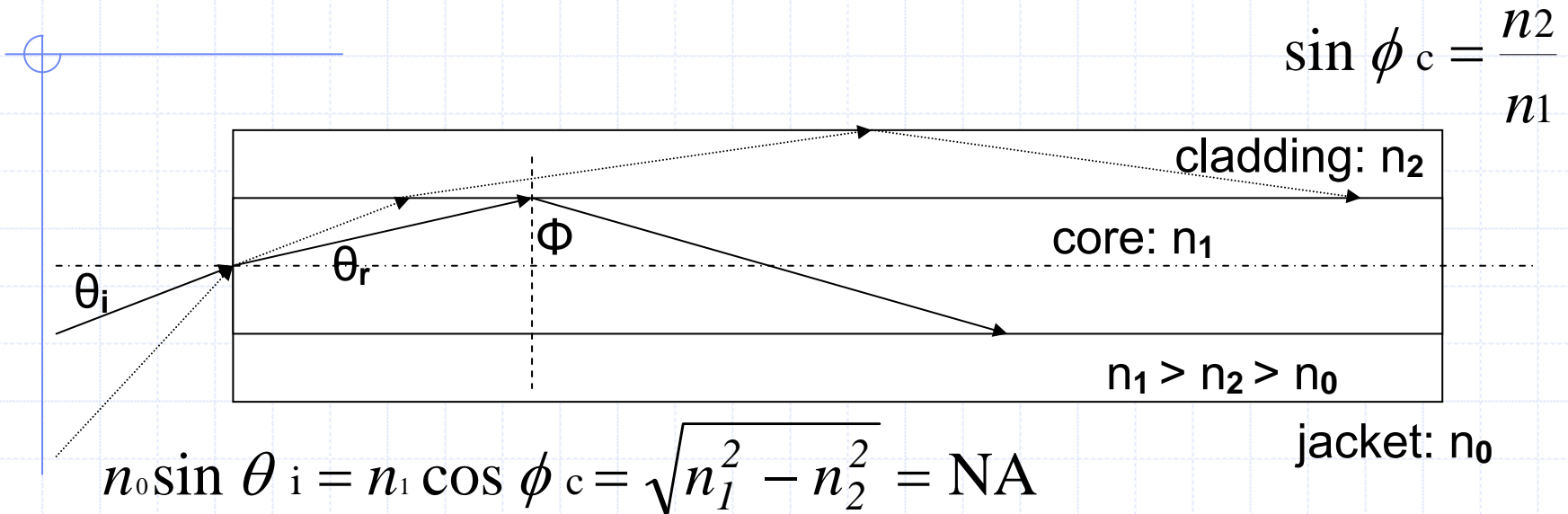
$$\nabla \cdot \mathbf{F} = \left(\frac{\partial f_1}{\partial x}, \frac{\partial f_2}{\partial y}, \frac{\partial f_3}{\partial z} \right) = \text{div } \mathbf{F}$$

$$\nabla \times \mathbf{F} = \text{rot } \mathbf{F}$$

Optical fibres

- ◆ Total internal reflection (discovered 1854)
- ◆ 1970: 20 dB/km (Kapron, Keck, Maurer), silica fibres
- ◆ Multimode (MM) and singlemode (SM) fibres
- ◆ Multimode: step-index (SI) or graded index (GI)
- ◆ MM SI: modal dispersion: different rays disperse in time because of the shortest (L) and longest ($L/\sin\Phi_c$) paths
- ◆ MM SI: 10 Mb/s, up to 10 km
- ◆ MM GI: parabolic index, lower modal dispersion, higher bit rates
- ◆ MM GI: 100 Mb/s, up to 100 km
- ◆ Plastic MM GI, for 1 GE (or even 10 Gb/s)
- ◆ Attenuation: 1 – 4 dB/km, <10 dB/km for plastic

Optical fibres



- ◆ Numerical aperture NA, the maximum angle of the incident ray to remain inside the core
- ◆ Core: MM: 50 μm /62,5 μm , SM: 8,6 μm – 9,5 μm
- ◆ Cladding: 125 μm

Optical fibres

- ◆ Single mode (SM, Standard SMF, G.652) fibres
- ◆ Supports only one so called „the fundamental mode of the fibre“ HE_{11} (TE_{11}), all higher modes are cut off @ the operating wavelength
- ◆ An optical mode refers to a specific solution of the wave equation (satisfies boundary conditions, spatial distribution is constant as light travels along a fibre)
- ◆ TE_{MN} or TM_{MN} , magnitude of the transverse electric field or the transverse magnetic field at the surface of the fibre core
- ◆ The cutoff wavelength is specified in ITU G.650, the V parameter (or normalized frequency), $V < 2,405$
- ◆ SM@1310 nm and 1550 nm, cutoff approx. 1200 nm
- ◆ 0,2 dB/km@1550 nm, 0,4 dB/km@1310 nm

Optical fibres – Dispersion (1)

- ◆ MM: Intermodal dispersion (pulse broadening, the most important limiting factor)
- ◆ SM: Intermodal dispersion is absent, pulse broadening is present still because of Intramodal dispersion (or Group-velocity dispersion GVD), even laser pulses have *finite* spectral width and pulses are *modulated*
- ◆ GVD: different spectral components of the pulse travel at different speeds
- ◆ Increases as the square of the bit rate
- ◆ $v_g = (d\beta(\omega)/d\omega)^{-1}$, β – the propagation constant
- ◆ Intramodal dispersion has two components:
 - Material dispersion
 - Waveguide (or wavelength) dispersion

Optical fibres – Dispersion (2)

- ◆ D – the dispersion parameter [ps/(nm*km)]

$$D = \frac{d}{d\lambda} \left(\frac{1}{v_g} \right) = - \frac{2\pi c}{\lambda^2} \beta_2$$

- ◆ β_2 - the GVD parameter

$$\beta_2 = \frac{d^2 \beta}{d\omega^2}$$

- ◆ $D = D_M + D_W$
- ◆ Material dispersion: dependence of the refractive index n on frequency ω , positive D
- ◆ Waveguide dispersion: nonlinear dependence of the propagation constant β on frequency ω , negative D

Optical fibres – Dispersion (3)

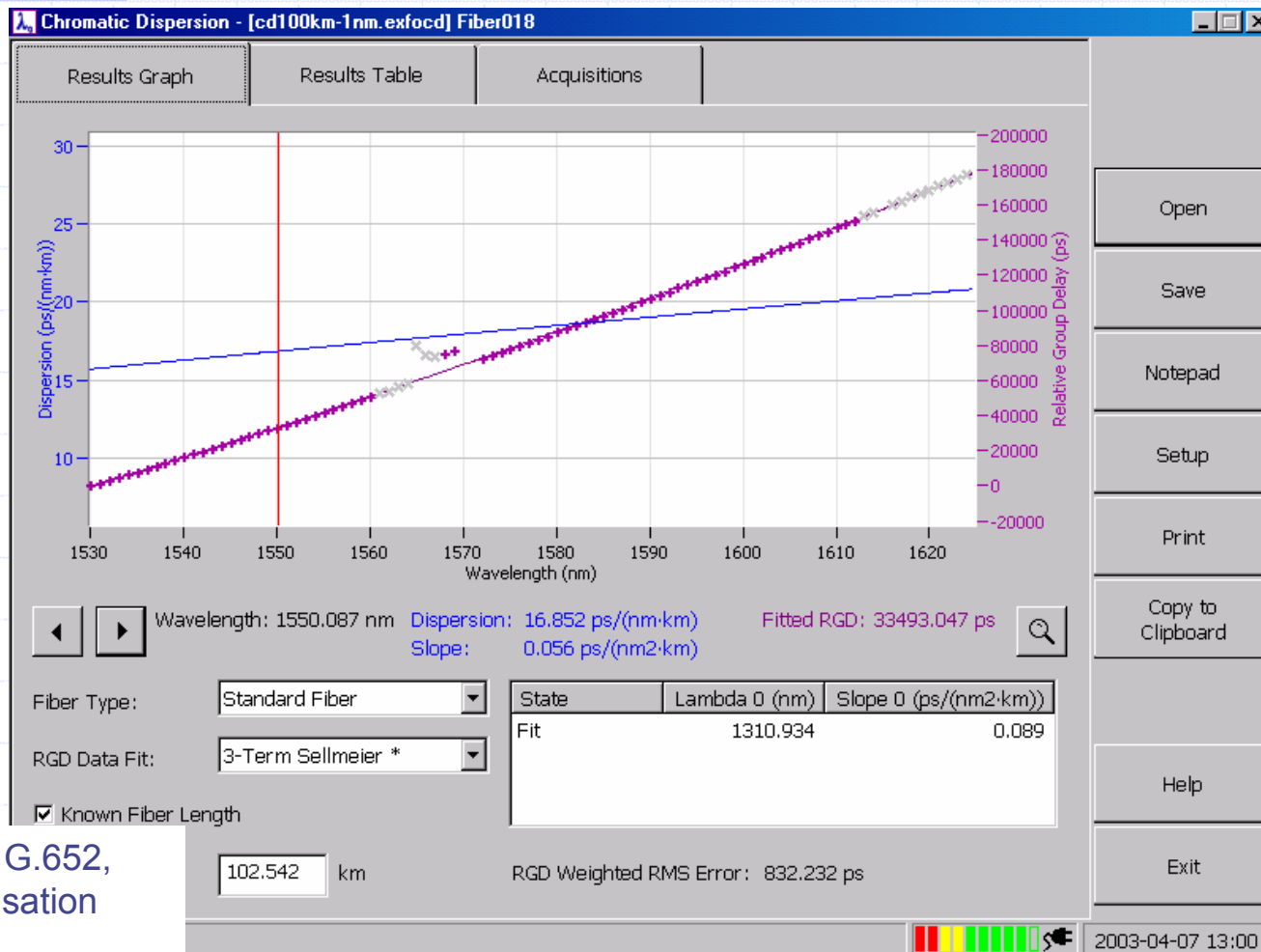
- ◆ ITU – Limits of Chromatic dispersion
- ◆ Maximum CDC and $D(\lambda)$, specified in G.652, G.653, G.655
- ◆ G.652 (SSMF): Zero dispersion at 1310 nm
- ◆ G.653 (DSF): Zero dispersion at 1550 nm
- ◆ G.655 (NZDSF): Small dispersion at 1550 nm, positive/negative
- ◆ Dispersion-flattened fibre (DFF), positive/negative
- ◆ Dispersion Compensating fibres (DCF)

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Optical fibres – Dispersion (4)

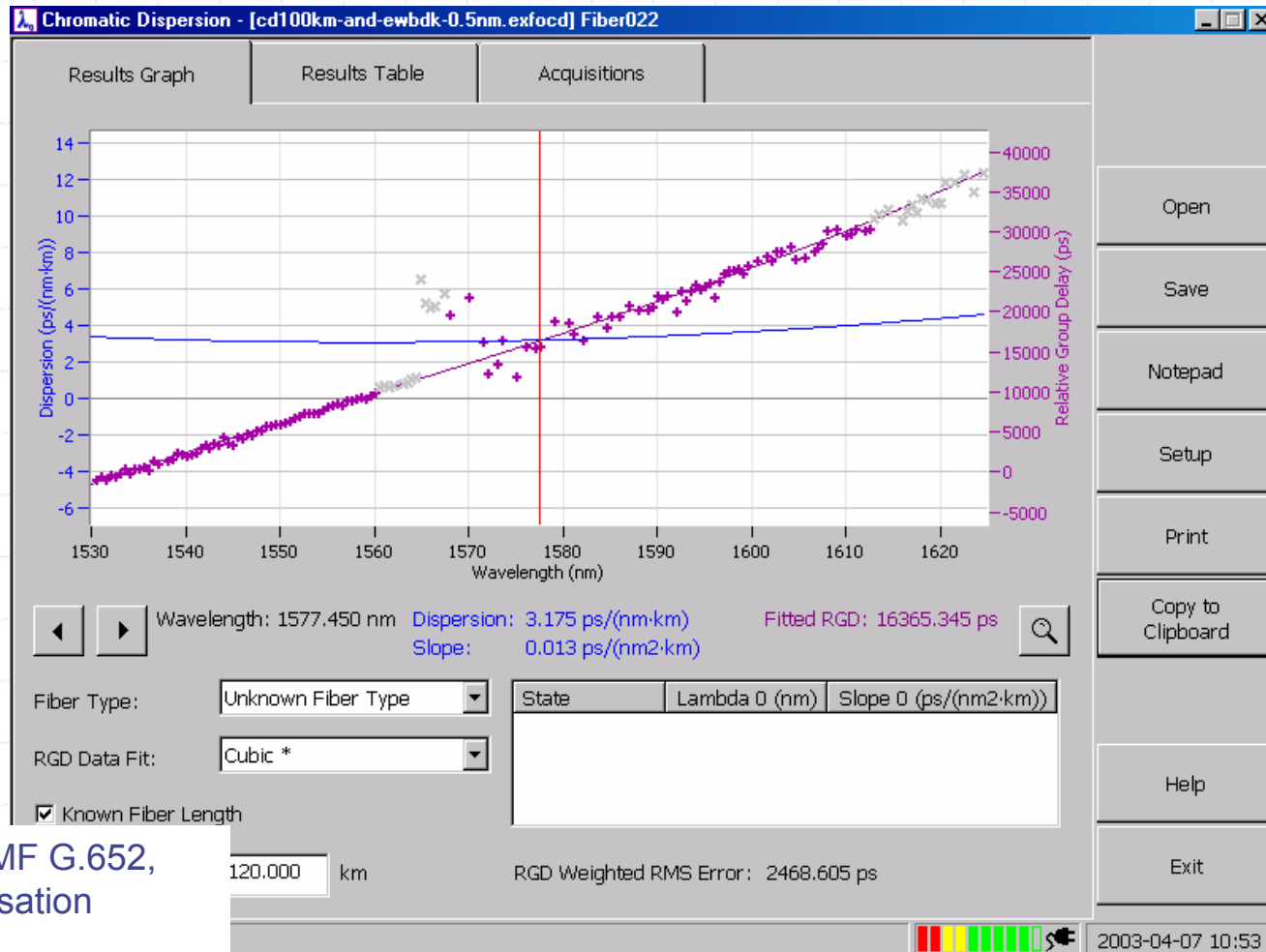
- ◆ Higher-Order Dispersion(s)
- ◆ Governed by the dispersion slope $S = dD/d\lambda$
- ◆ β_3 - the third order dispersion parameter

Optical fibres – Chromatic Dispersion (1)



100 km of SMF G.652, without compensation

Optical fibres – Chromatic Dispersion (2)



100 km of SMF G.652,
with compensation

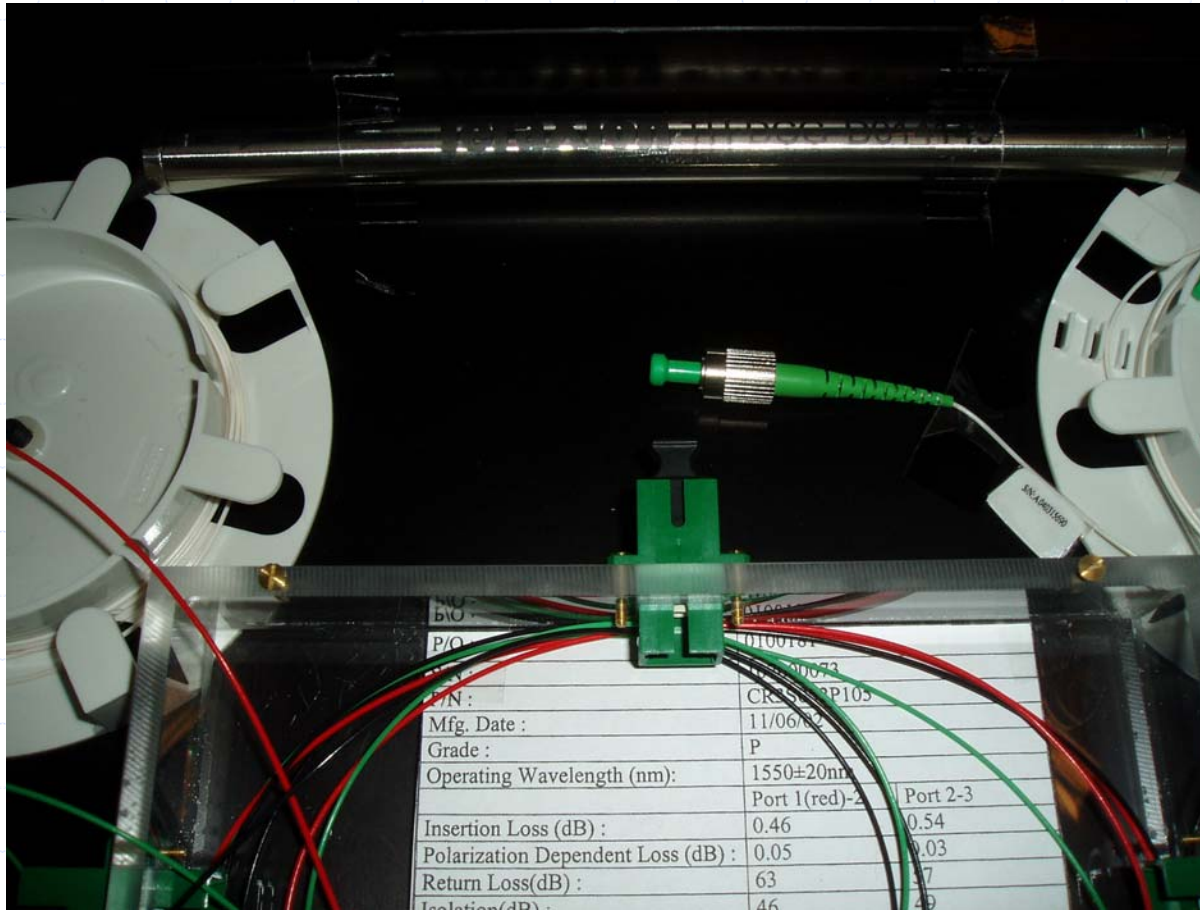
Chromatic Dispersion Compensation

- ◆ Dispersion compensating fibres (DCF)
 - A special kind of fibre, compensates all wavelengths (the only solution for „grey” transmitters)
 - Adds link loss (and money), especially for long-haul applications
 - Stronger non-linear effects (due to a smaller core diameter)
- ◆ Fibre Bragg gratings (FBG)
 - Narrow-band elements – a stabilized DWDM laser is a must
 - „Wide-band” FBGs available today (for 50 ITU DWDM channels)
 - Signal filtering, spectrum shaping, tuneable compensators
 - Cost effective solution

Chromatic Dispersion Compensation

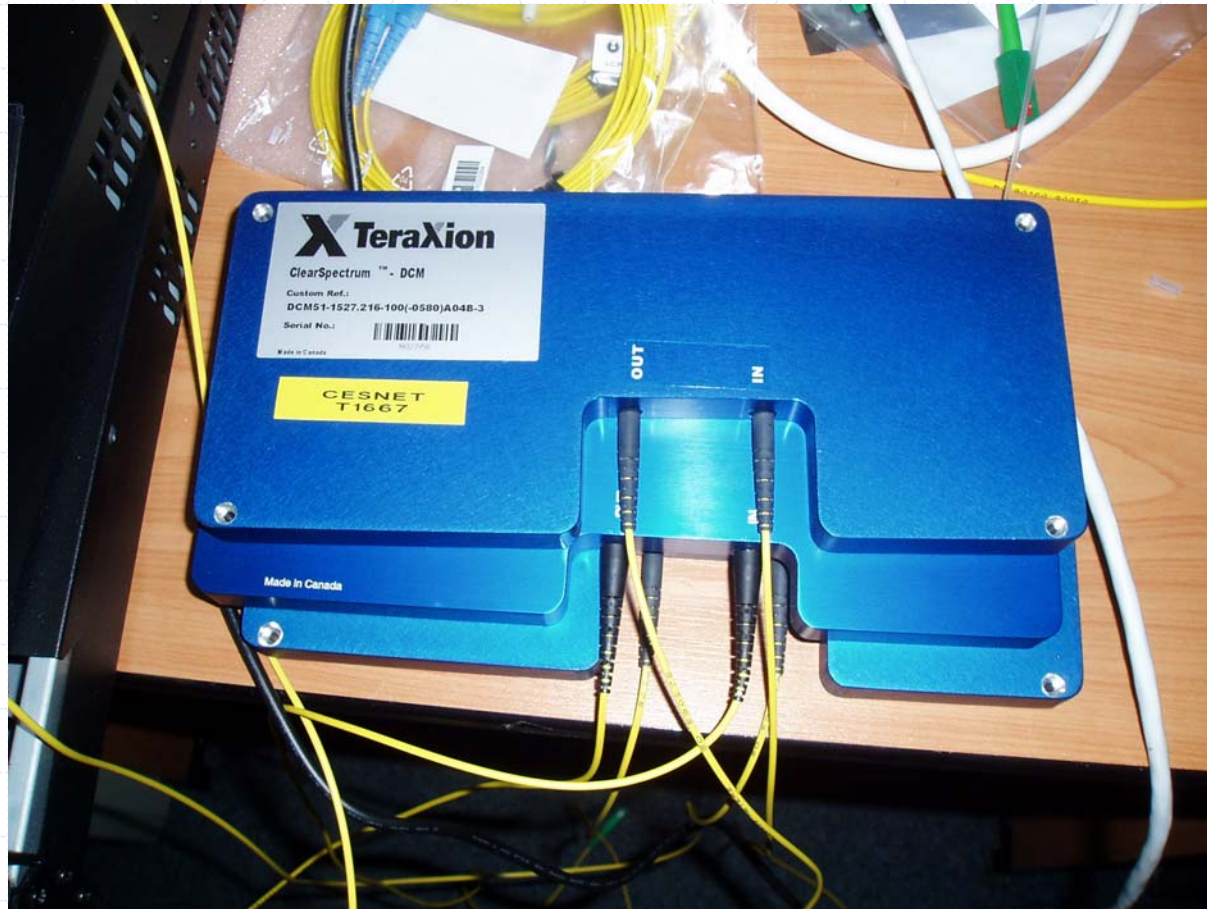
- ◆ Optical Phase Conjugation (OPC)
 - A nonlinear optical technique (midspan spectral inversion)
 - The complex conjugate of a pulse-propagation equation
 - Four-wave mixing in a nonlinear medium (phase conjugators)
- ◆ Electronic pre-compensation
 - A relatively new technique
 - An electrical signal is pre-distorted before converting into an optical domain
 - Dispersion can be tuned for up to thousands kilometers of G.652 fibre

Chromatic Dispersion Compensation (FBG)



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Chromatic Dispersion Compensation (FBG)



Chromatic Dispersion Compensation

- ◆ Typical values (receivers can have different tolerance to CD!)

Bit rate (Gbit/s)	Maximum length of G.652 link (km)
2,5	1000
10	80
40	4

Cromatic Dispersion Measurements

- ◆ Modulated Phase-Shift Method (FOTP 169)
- ◆ Differential Phase-Shift Method (FOTP 175)
 - Both phase-shift methods are accurate, measurement through optical amplifiers, expensive
- ◆ Spectral Group Delay Measurement in the Time Domain (FOTP 168)
 - Still accurate enough, no measurement through optical amplifiers
 - Relative group delay is measured and the dispersion coefficient D is calculated
- ◆ TIA/EIA

Optical fibres – PMD (1)

- ◆ Polarization Mode Dispersion (PMD)
- ◆ Fibre birefringence (stress, temperature, imperfections)
- ◆ The stochastic phenomenon
- ◆ The fundamental mode HE_{11} (TE_{11}) has two orthogonally polarized modes
- ◆ The two components with different propagating speeds disperse along the fiber
- ◆ The difference between the two propagation times is known as the Differential Group Delay (DGD)
- ◆ PMD is a wavelength averaged value of DGD

Optical fibres – PMD (2)

- ◆ PMD is measured and quoted in ps for a particular span and discrete components but its coefficient is in $\text{ps}/(\text{km})^{1/2}$
- ◆ PMD accumulates as the square root of distance of a link
- ◆ A single span with high PMD dominates the total PMD for the whole network
- ◆ A big issue for older fibres (late 1980s, 80 000 000 km) and higher bit rates (10 Gb/s)
- ◆ Modern fibres have PMD of less than $0,5 \text{ ps}/(\text{km})^{1/2}$
- ◆ Difficult to compensate (electronic)

Optical fibres – PMD (3)

- ◆ Second-order PMD
- ◆ For long-haul links, together with CD and laser chirping

ITU proposed PMD values

Bit rate (Gb/s)	Maximum PMD (ps)	PMD coefficient for 400 km fibre (ps/(km) ^{1/2})
2,5	40	2,0
10	10	0,5
20	5	0,25
40	2,5	0,125

PMD Measurements

- ◆ The Fixed Analyzer Method (FOTP 113)
 - Well known, low price, problem with accuracy
- ◆ The Interferometric Method (FOTP 124)
 - Well known, average PMD
- ◆ The Jones Matrix Method (FOTP 122)
 - „Golden Standard“
 - Measures DGD per wavelength
- ◆ TIA/EIA

Optical networks and equipment

Nonlinear Optical Effects

- ◆ When an intensity of electromagnetic fields becomes too high, the response of materials becomes nonlinear
- ◆ For optical systems, nonlinear effects can be both advantageous (Raman amplification) and degrading (Four Wave Mixing, Self Phase Modulation)

Nonlinear Optical Effects

- ◆ Stimulated Raman Scattering (SRS)
- ◆ A signal is scattered by molecular vibrations of fibre – optical phonons
- ◆ Can occur both in forward and backward directions
- ◆ Shifted to longer wavelengths (lower energy) by 10 to 15 THz in the 1550 nm window
- ◆ Wide bandwidth of about 7 THz (55 nm)
- ◆ Maybe used for amplification (Raman fibre lasers), so called counter directionally pumping schemes
- ◆ In DWDM systems: transfer of power from shorter wavelengths to longer ones

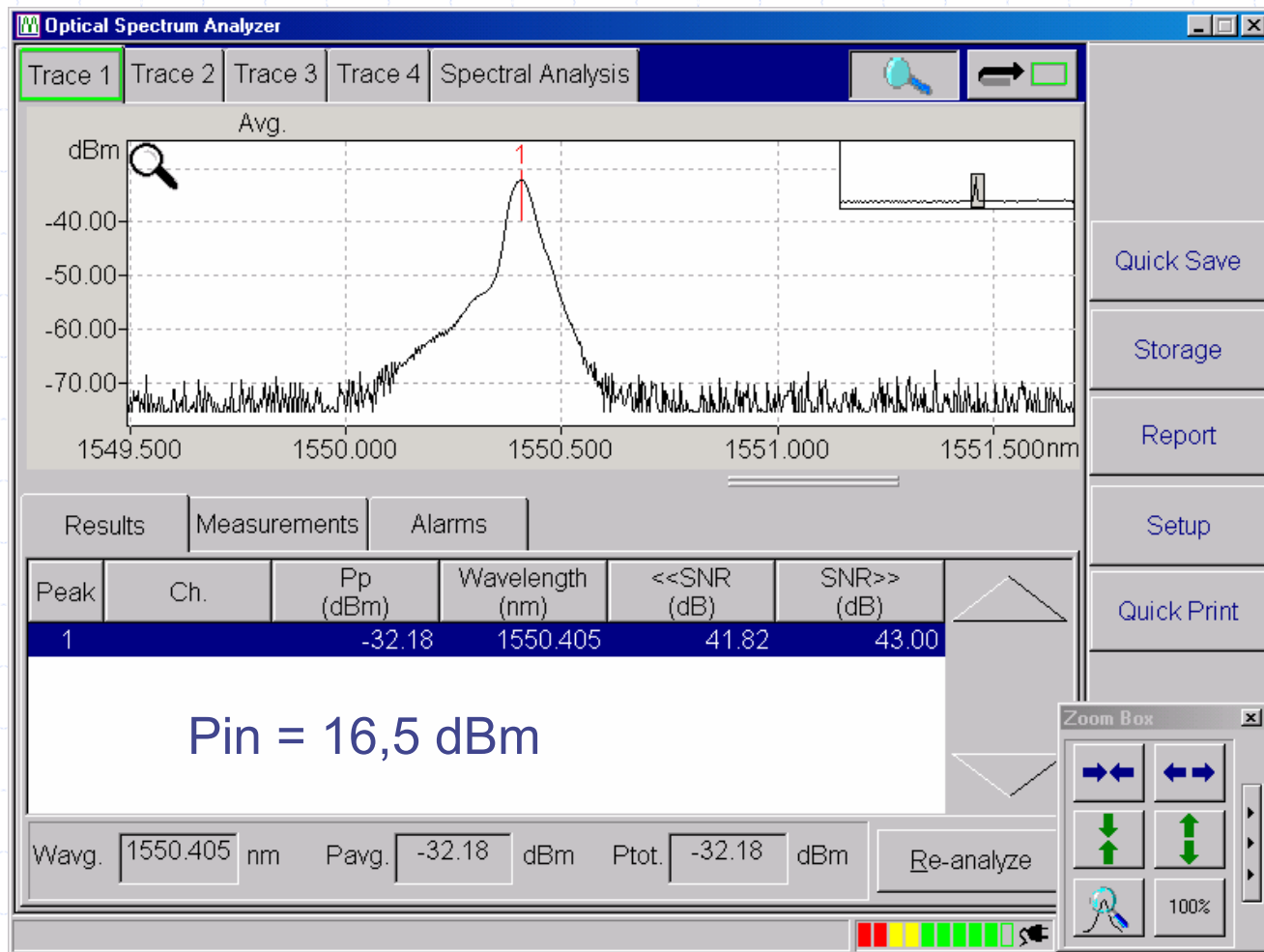
Nonlinear Optical Effects

- ◆ Stimulated Brillouin Scattering (SBS)
- ◆ A signal is scattered by sound waves – acoustic phonons
- ◆ Shifted to longer wavelengths (lower energy) by 11 GHz in the 1550 nm window
- ◆ Narrow bandwidth of about 30 MHz
- ◆ A problem for monochromatic unmodulated signals

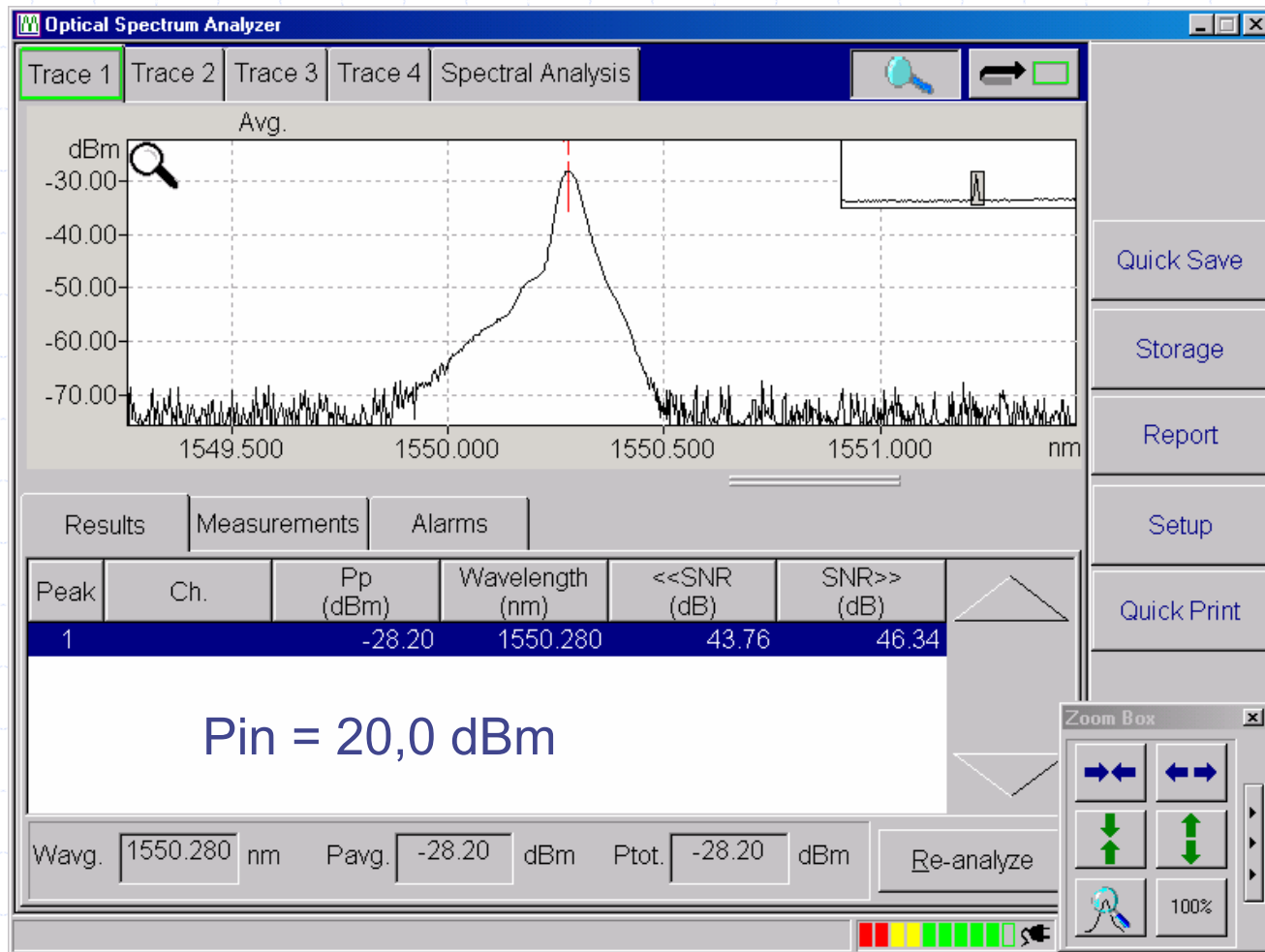
Nonlinear Optical Effects

- ◆ Self-Phase Modulation (SPM)
- ◆ When the intensity of the signal becomes too high, the signal can modulate its own phase
- ◆ The refractive index is no longer a constant
- ◆ Spectral broadening (positive chromatic dispersion) or spectral compression (negative CD)
- ◆ Significant for fibres with small effective areas (G.655, DCF)
- ◆ Higher bit rates (10 Gb/s)

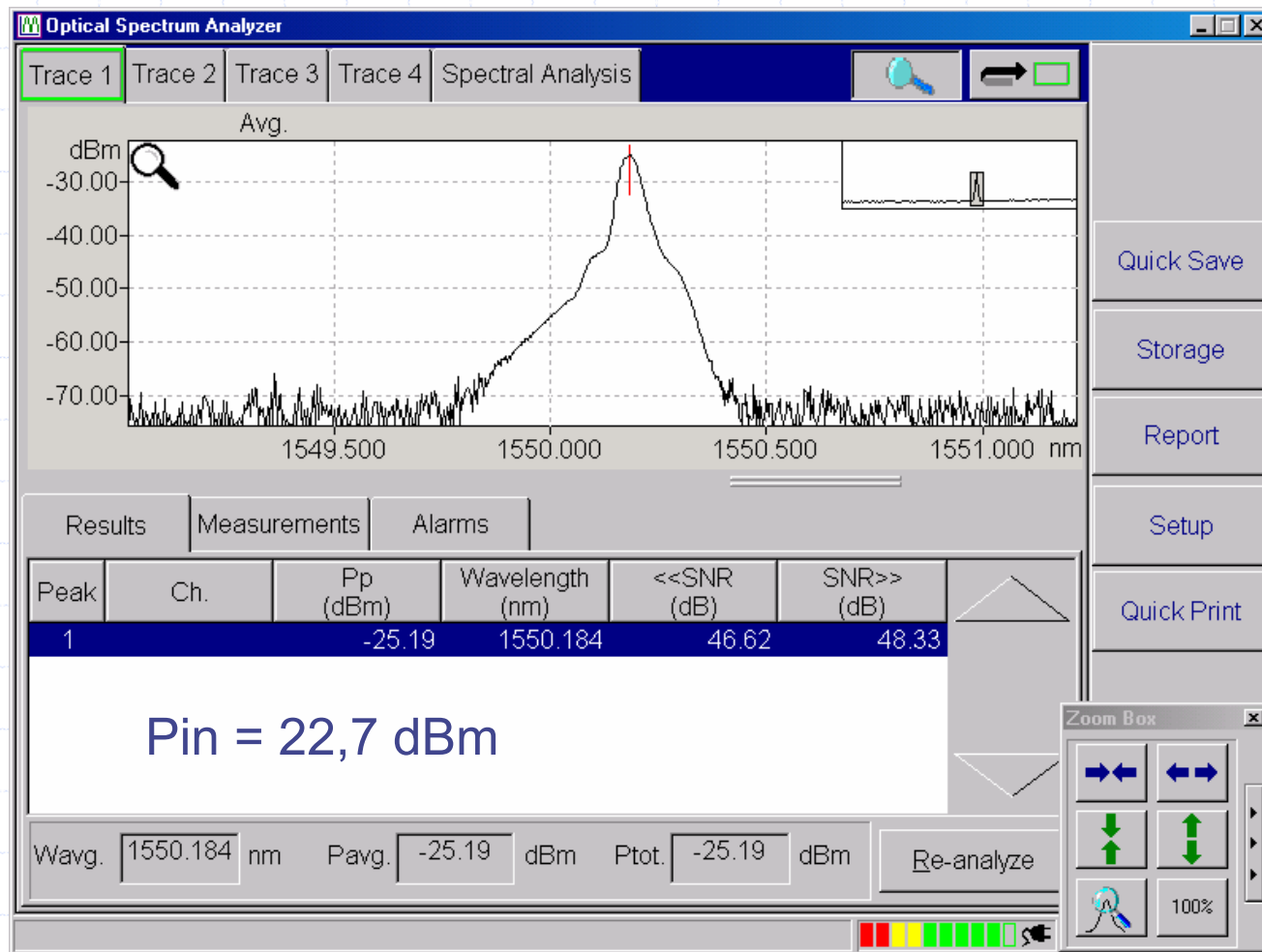
Nonlinear Optical Effects (SPM1)



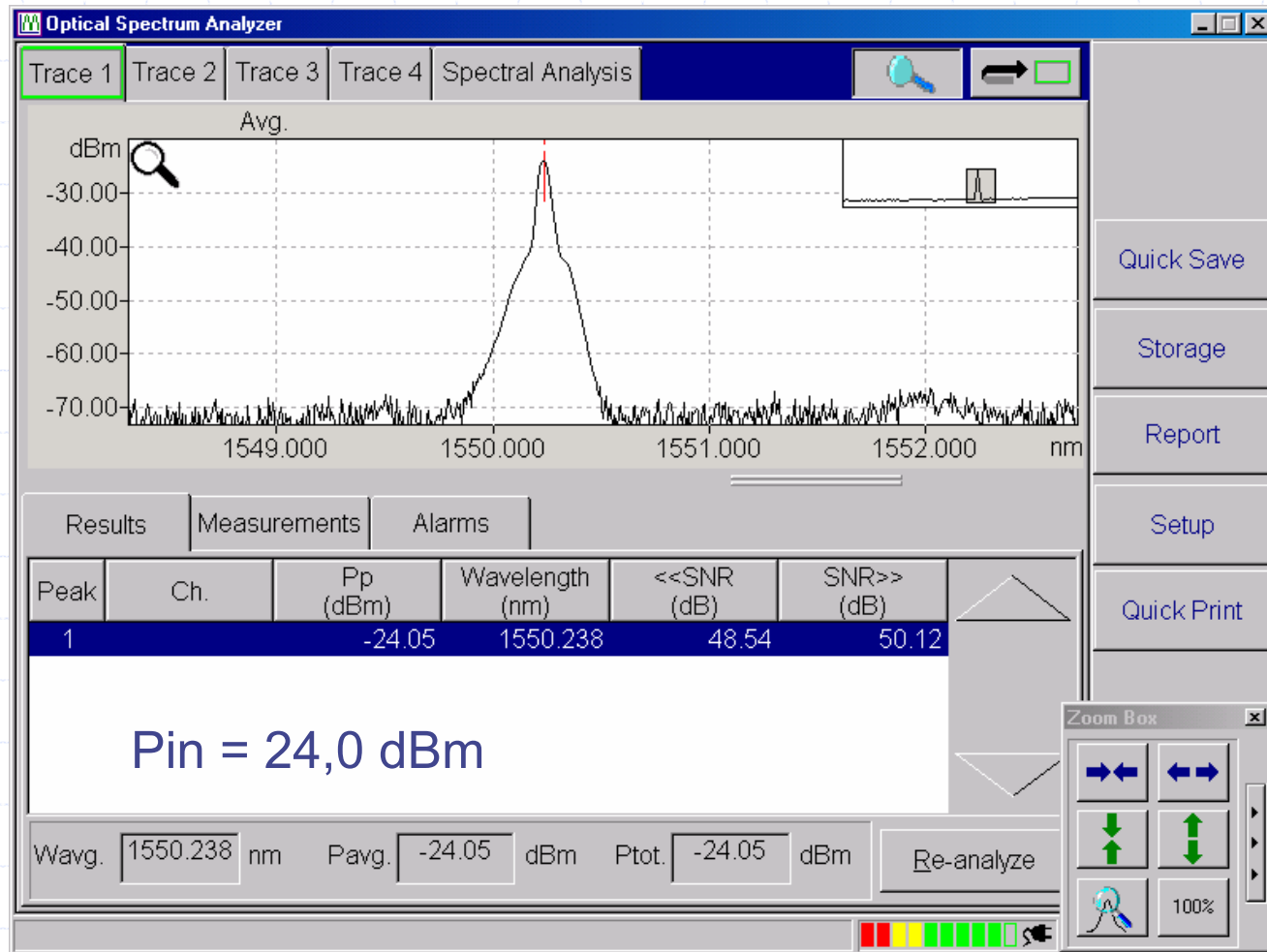
Nonlinear Optical Effects (SPM2)



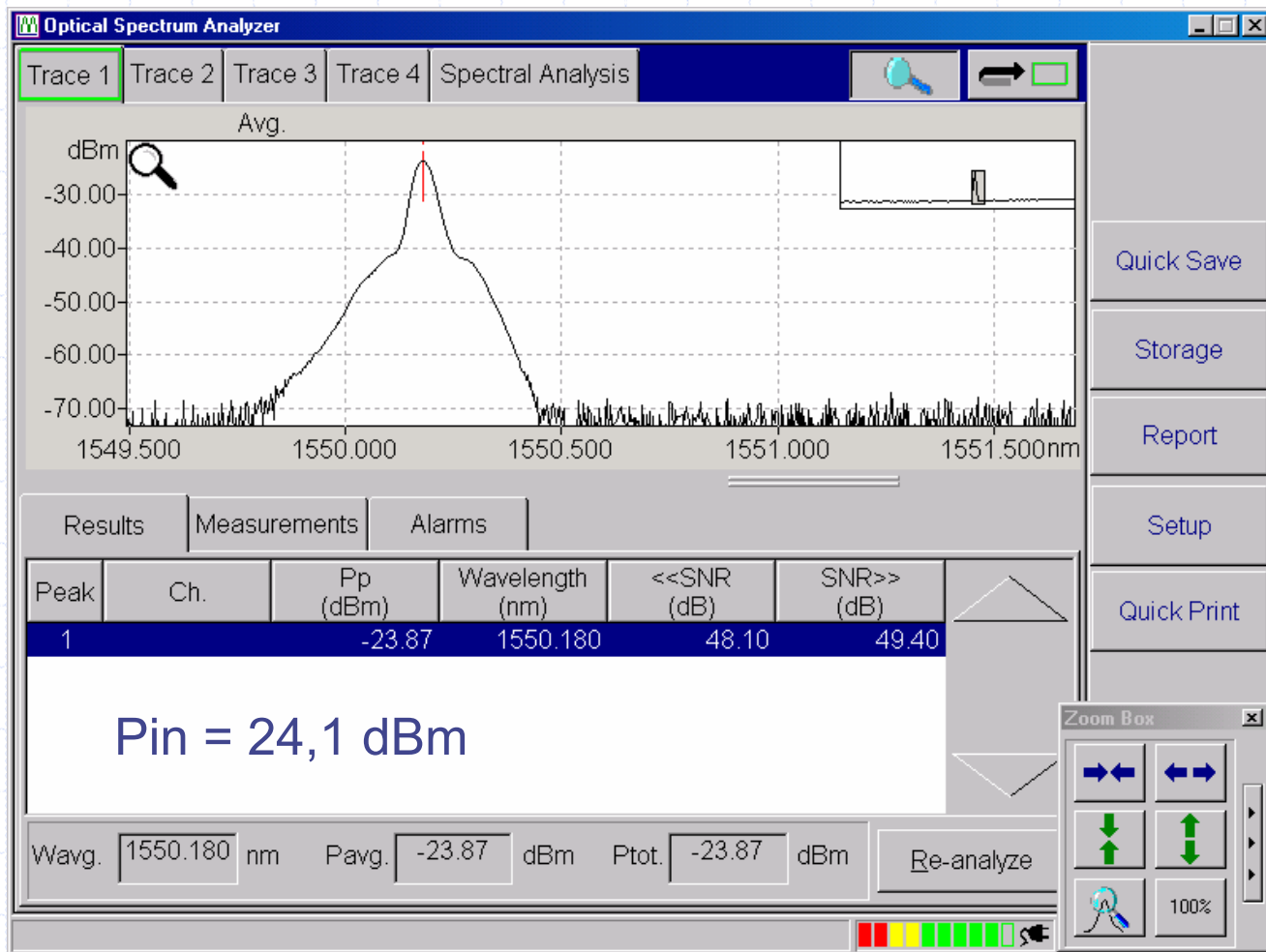
Nonlinear Optical Effects (SPM3)



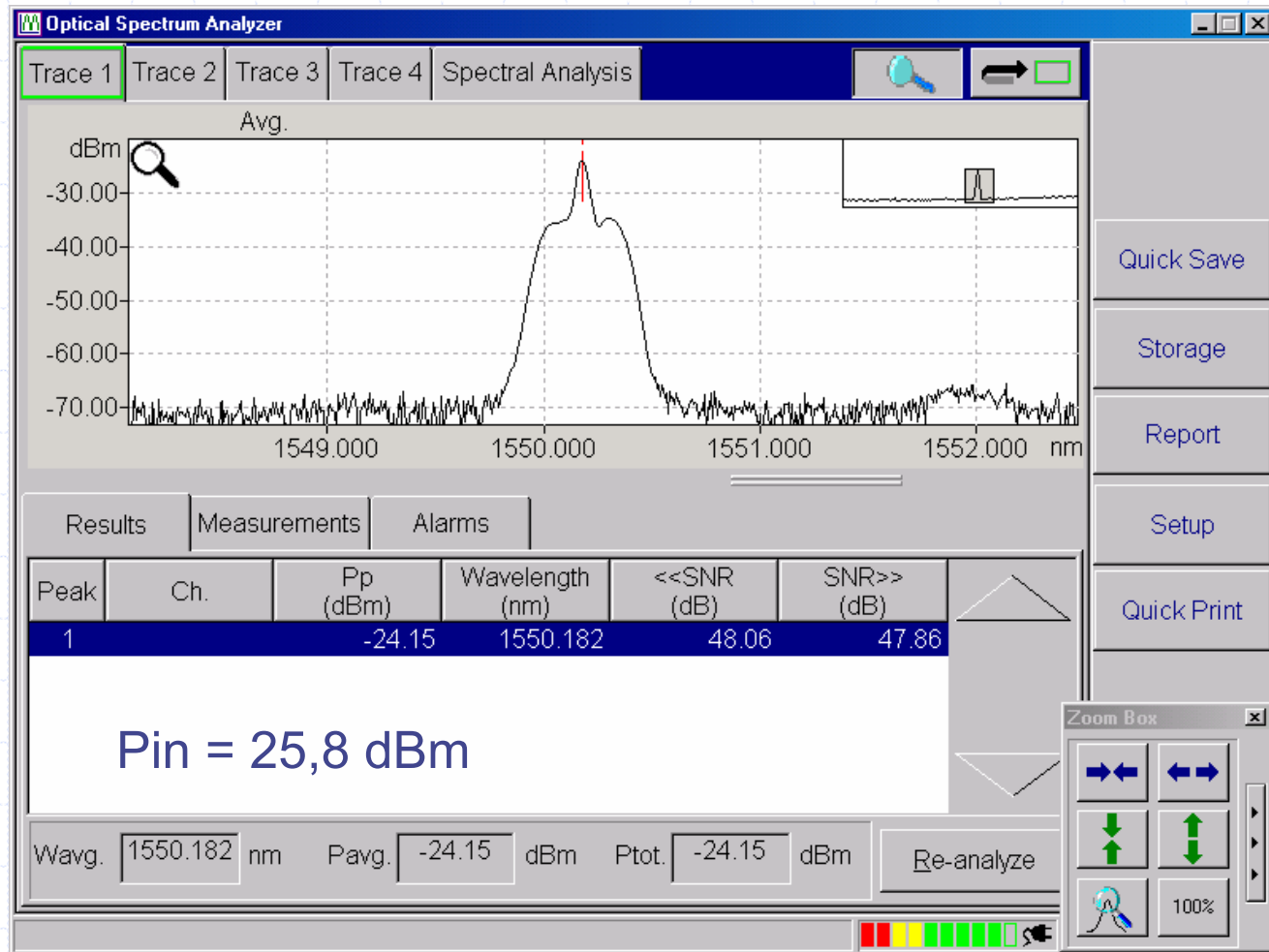
Nonlinear Optical Effects (SPM4)



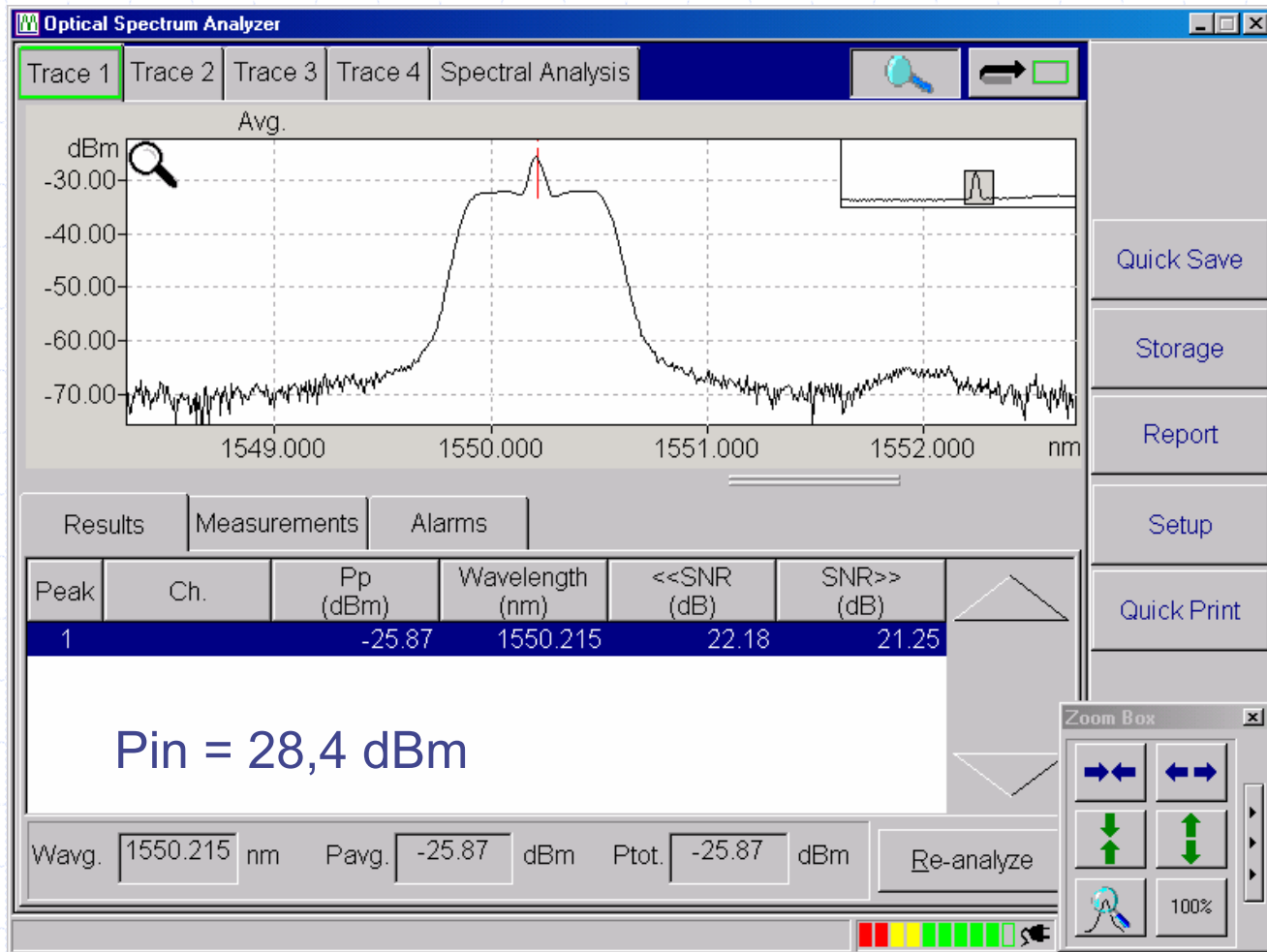
Nonlinear Optical Effects (SPM5)



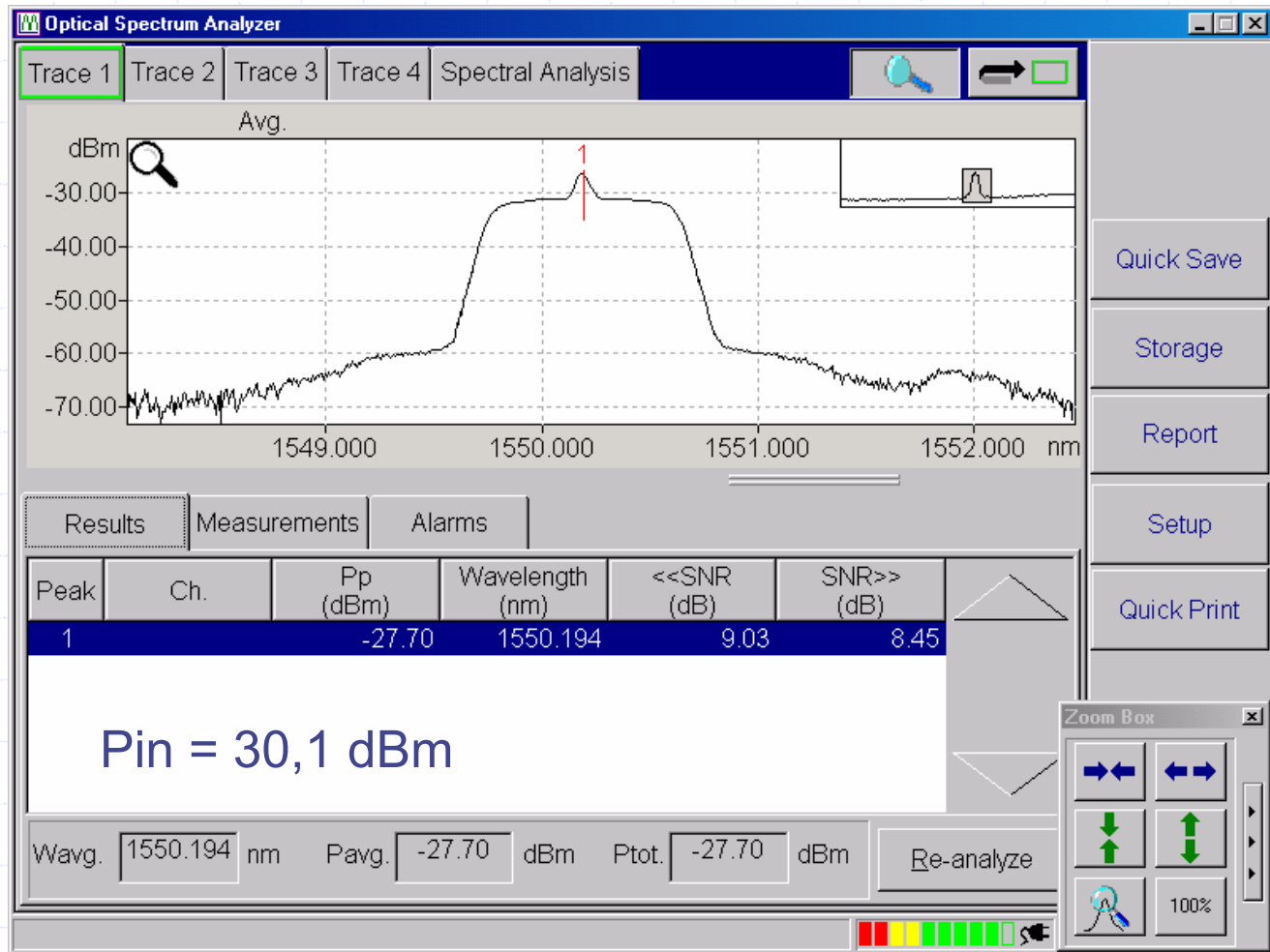
Nonlinear Optical Effects (SPM6)



Nonlinear Optical Effects (SPM7)



Nonlinear Optical Effects (SPM8)



Nonlinear Optical Effects

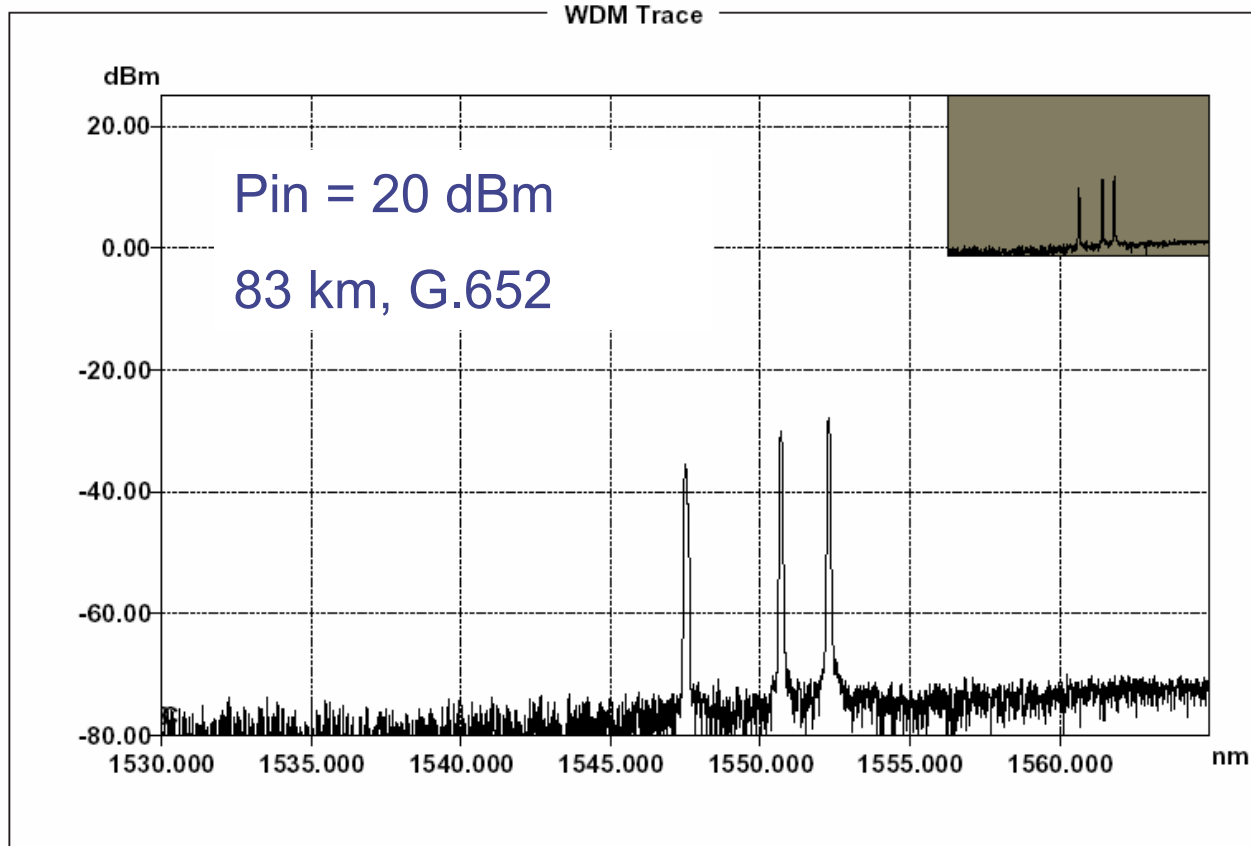
- ◆ Cross-Phase Modulation (CPM)
- ◆ A signal modulates the phases of adjacent channels

Nonlinear Optical Effects

- ◆ Four Wave Mixing (FWM)
- ◆ New „ghost“ signals appear in the transmission spectral range
- ◆ Depends on several factors like launched powers, the CD, the refractive index, the fibre length
- ◆ Severe limitations for G.653 fibres and DWDM transmissions in the 1550 nm window (C band)
- ◆ Solution to this problem is to deploy L band DWDM systems (1565 nm – 1625 nm), where CD is high enough

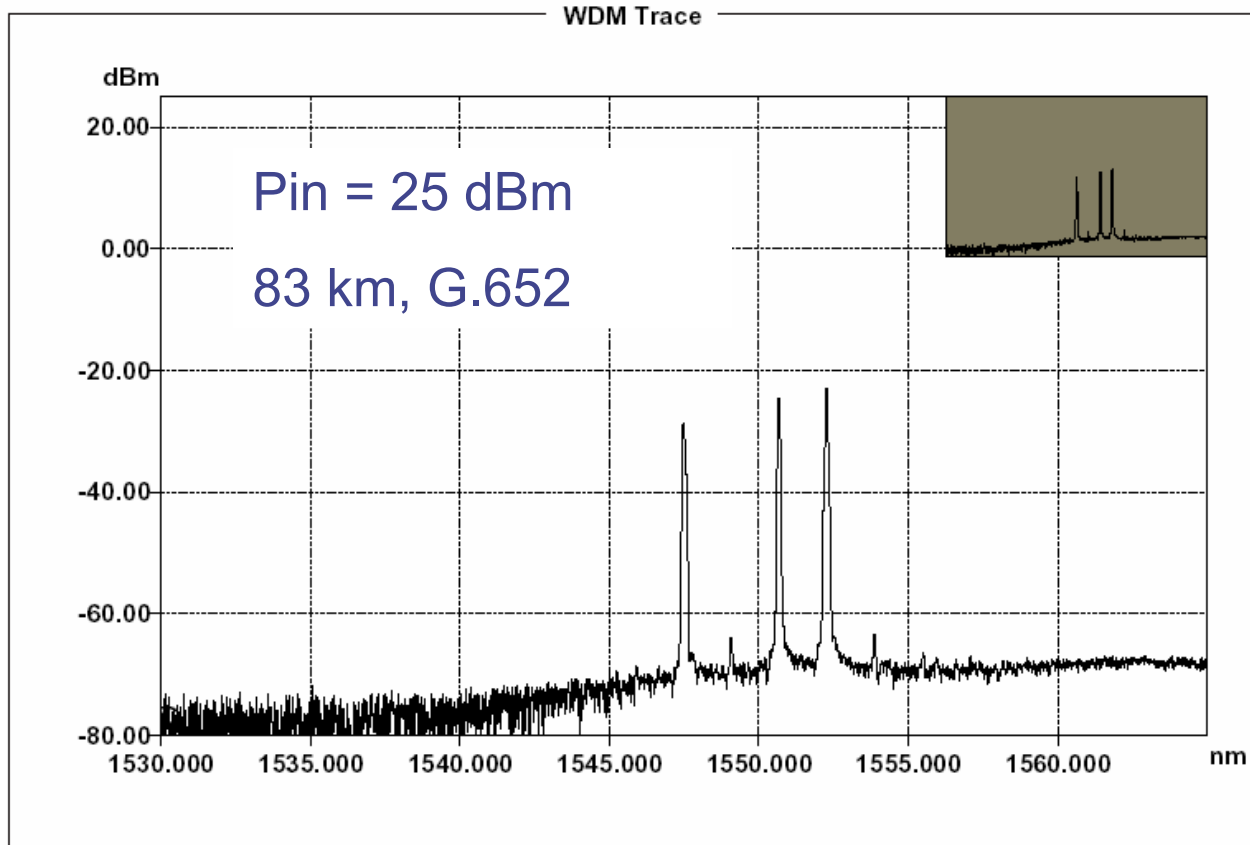
Nonlinear Optical Effects (FWM1)

OSA Report



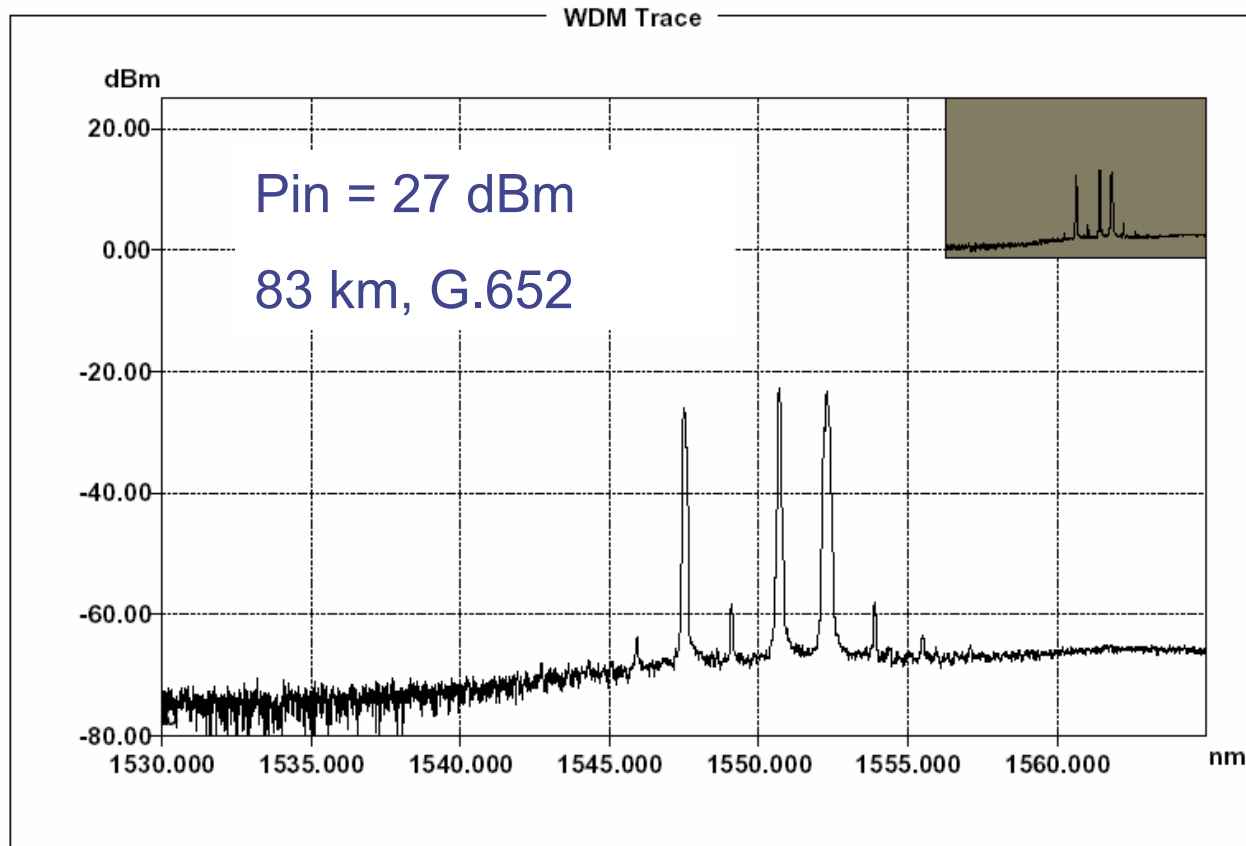
Nonlinear Optical Effects (FWM2)

OSA Report

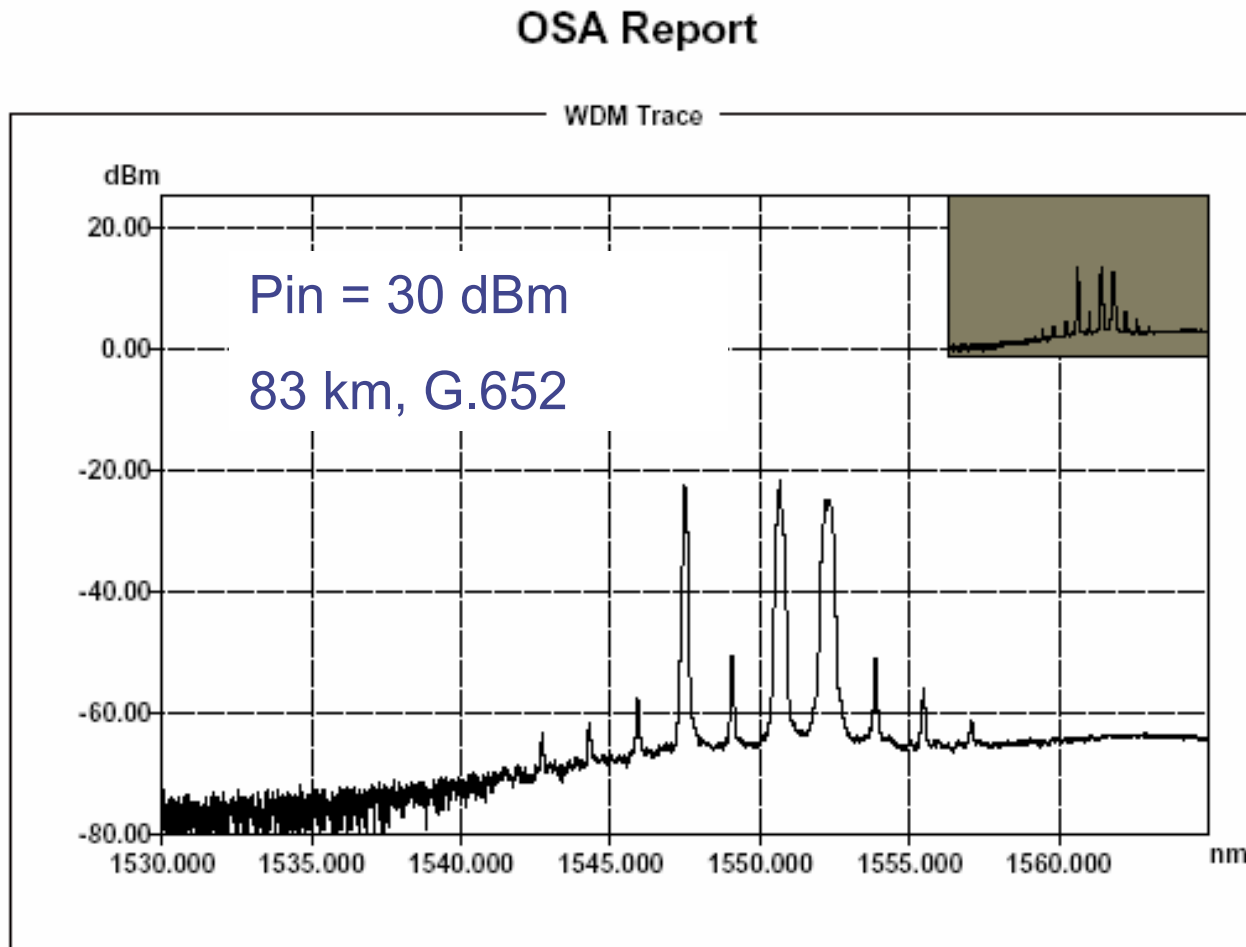


Nonlinear Optical Effects (FWM3)

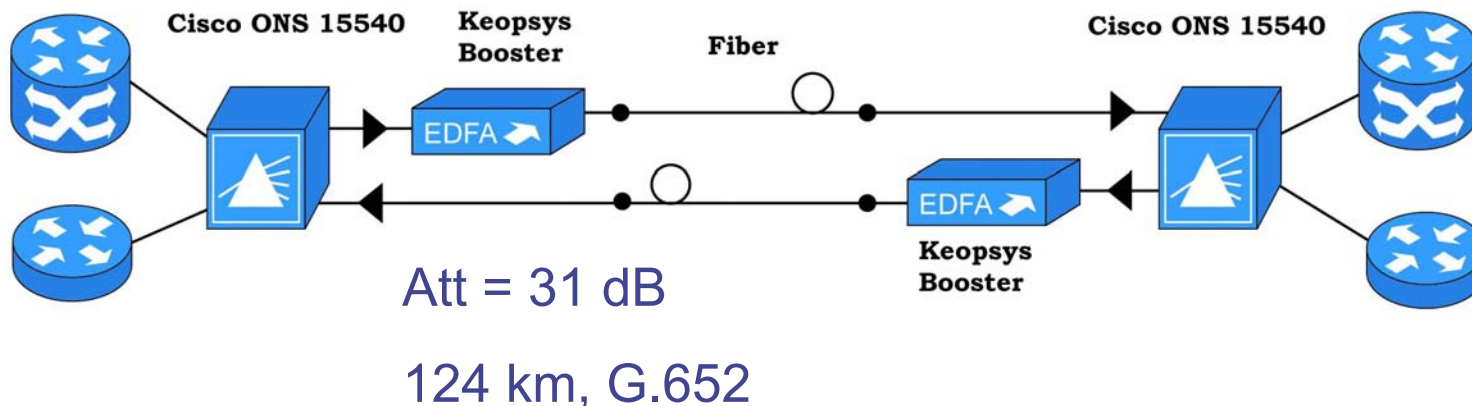
OSA Report



Nonlinear Optical Effects (FWM4)

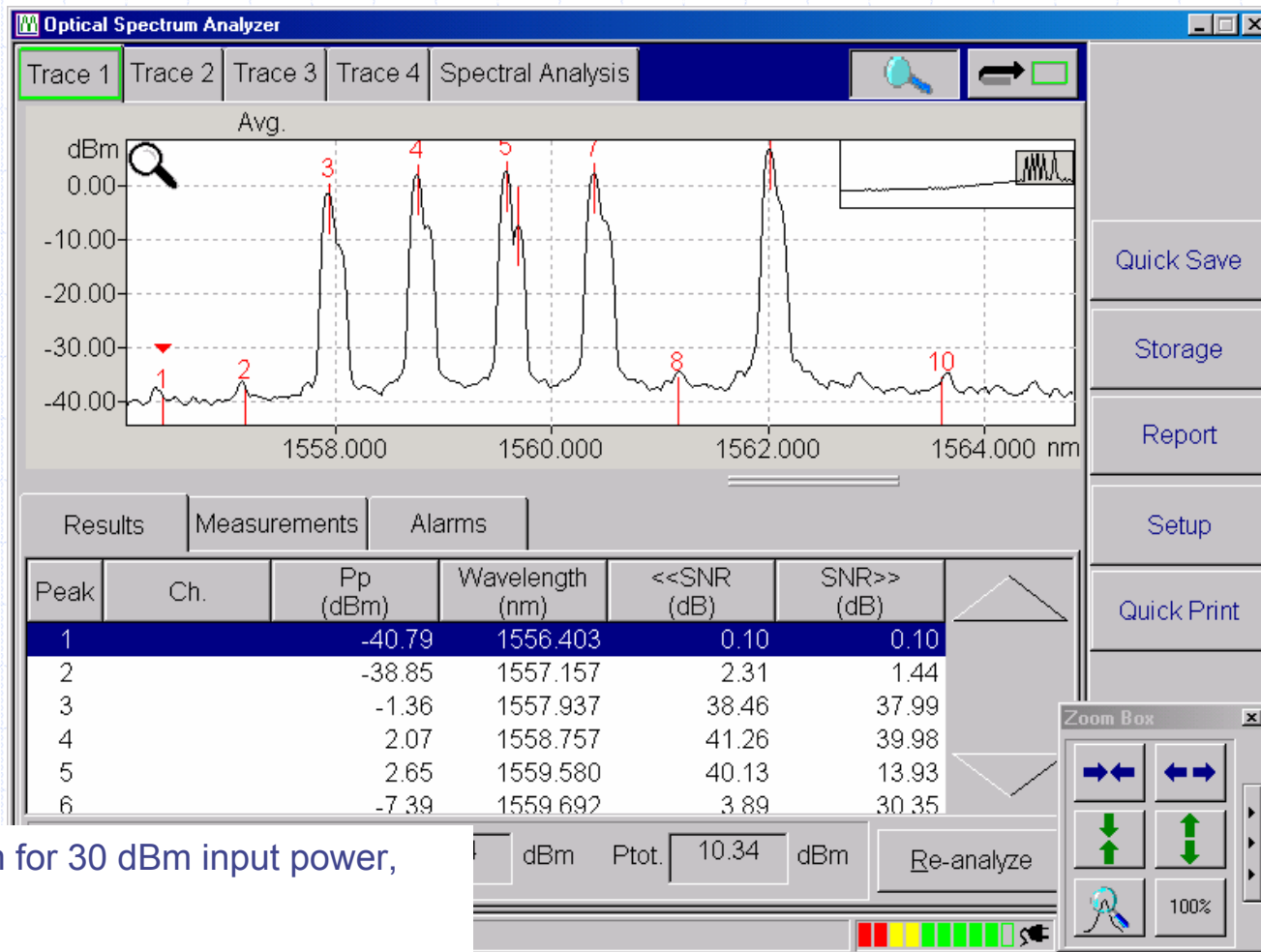


Nonlinear Optical Effects (FWM5), TNC03



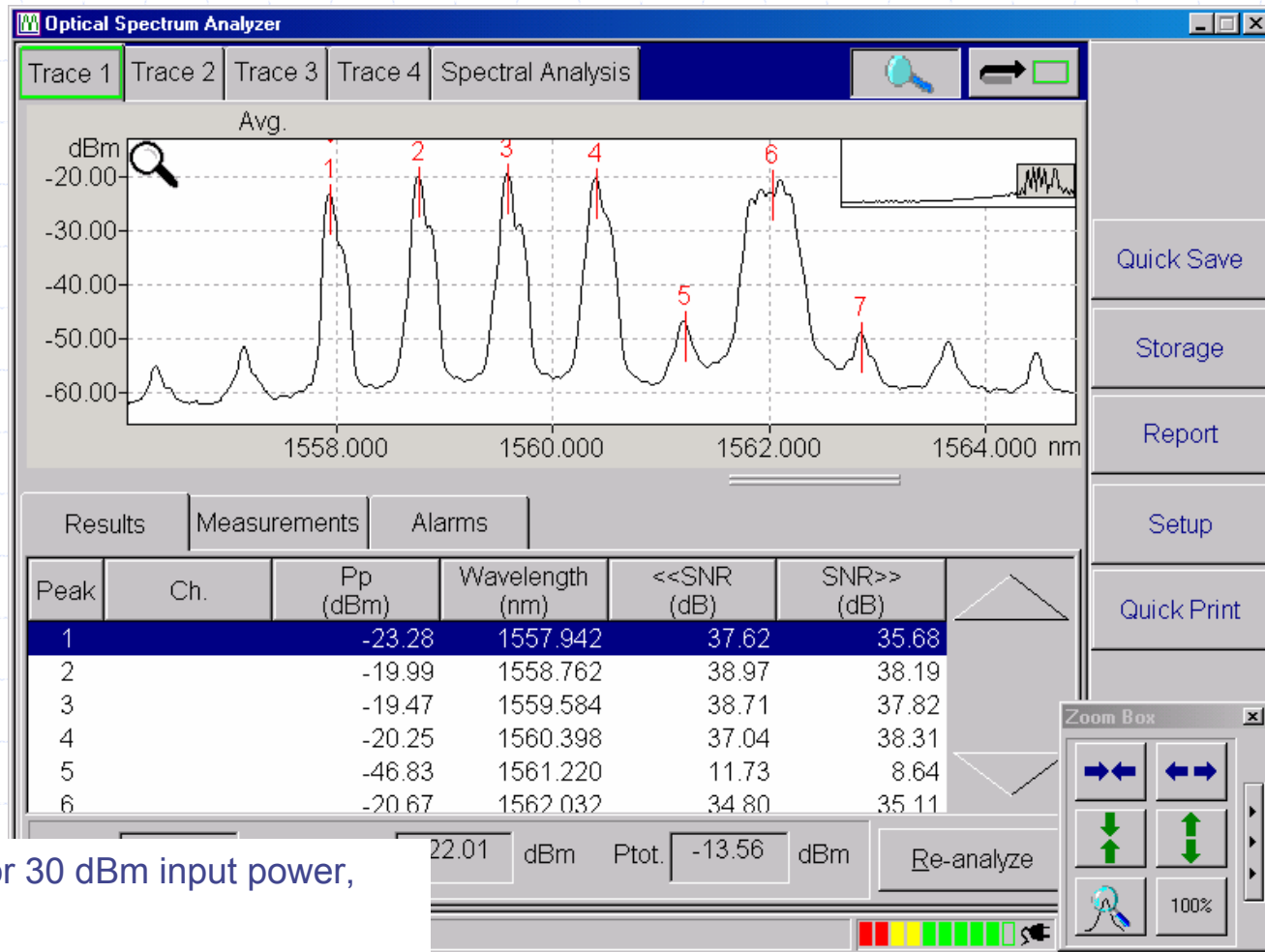
- ◆ Strong effects of SPM, CPM and FWM
- ◆ OSC mostly affected
- ◆ Single-channel EDFAs are OK for 5 channels
- ◆ For 16/32 channels you need really powerful booster (17 dBm for 1 channel corresponds to 2 dBm for 32 channels)

Nonlinear Optical Effects (FWM6)



Spectral diagram for 30 dBm input power, after EDFA.

Nonlinear Optical Effects (FWM7)



Spectral diagram for 30 dBm input power, before receiver.

Transmitters

- ◆ Laser and modulator
- ◆ Conversion of electrical signals into optical streams
- ◆ Laser: LED, Fabry-Perot (FP), Distributed Feedback (DFB)
- ◆ Direct or external (10 Gb/s) modulation
- ◆ Output powers: 0 dBm – 5 dBm
- ◆ Pluggable, DWDM ITU wavelengths (193,1 THz)
- ◆ GBIC (1 Gb/s), SFP (1 Gb/s – 2,5 Gb/s)
- ◆ Xenpak, XFP, Xpak, X2 (10 Gb/s)

Transmitters

- ◆ Price comparison
- ◆ GBIC 1550 nm: USD 6 000 (2002) from big vendors
- ◆ SFP DWDM: USD 2 000 (2005)
- ◆ Xenpak 1550 nm: USD 12 000 (2005)
- ◆ Xenpak DWDM: USD 31 000 (2005) from big vendors
- ◆ Xenpak DWDM: USD 5 500 (2005) from manufacturers
- ◆ XFP 1550 nm: USD 2 500 (2005)
- ◆ XFP DWDM: USD 4500 (2006)

Transmitters



Transmitters – Modulations 1

- ◆ Different modulation formats, signal formats
- ◆ How to convert an electrical signal into an optical stream?
- ◆ On-Off Keying (OOK)
- ◆ A simple digital modulation scheme, easy to implement
- ◆ Intensity modulation with direct detection (IM/DD)
- ◆ Incoherent (the intensity only, no phase coherence)
- ◆ Two basic choices for the signal formats – return-to-zero (RZ) and nonreturn-to-zero (NRZ)
- ◆ Carrier suppressed (CS), Single side band (SSB), Vestigial sideband (VSB), Chirped (C) both for RZ and NRZ (CS-RZ, C-RZ,...)

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Transmitters – Modulations 2

- ◆ Coherent - well known from radio and microwave systems and literature
- ◆ Improvement of receiver sensitivity (up to 20 dB) when compared to IM/DD systems [Agrawal]
- ◆ More efficient use of bandwidth by increasing the spectral efficiency (higher tolerance to nonlinear effects, chromatic dispersion CD, polarization mode dispersion PMD)
- ◆ More complicated and more expensive

Advanced Modulation Formats

- ◆ Amplitude-shift keying (ASK)
- ◆ Phase-shift keying (PSK)
- ◆ Frequency-shift keying (FSK)
- ◆ Differential phase-shift keying (DPSK)
- ◆ Differential quadrature phase-shift keying (DQPSK) –
Wi-Fi
- ◆ Optical Duo Binary ODB (also known as phase shaped
binary modulation)

Advanced Modulation Formats

- ◆ Signal formats can be RZ, NRZ, CS-, etc. again
- ◆ DQPSK, ODB are *multilevel* modulations
- ◆ Multilevel – more amplitude levels (to achieve spectral efficiency better than 1 bit/s/Hz), 40 Gb/s is 10 Gbaud for a 16 level modulation
- ◆ DQPSK (information is encoded in the 4 differential optical phase between successive bits)
- ◆ ODB (in simplest scheme - two consecutive bits are summed -> a three level code is created, AM-PSK)
- ◆ RZ-DPSK, NRZ-DPSK, CS-RZ OOK, RZ-ODB have been studied extensively (better tolerance to different impairments)

Receivers

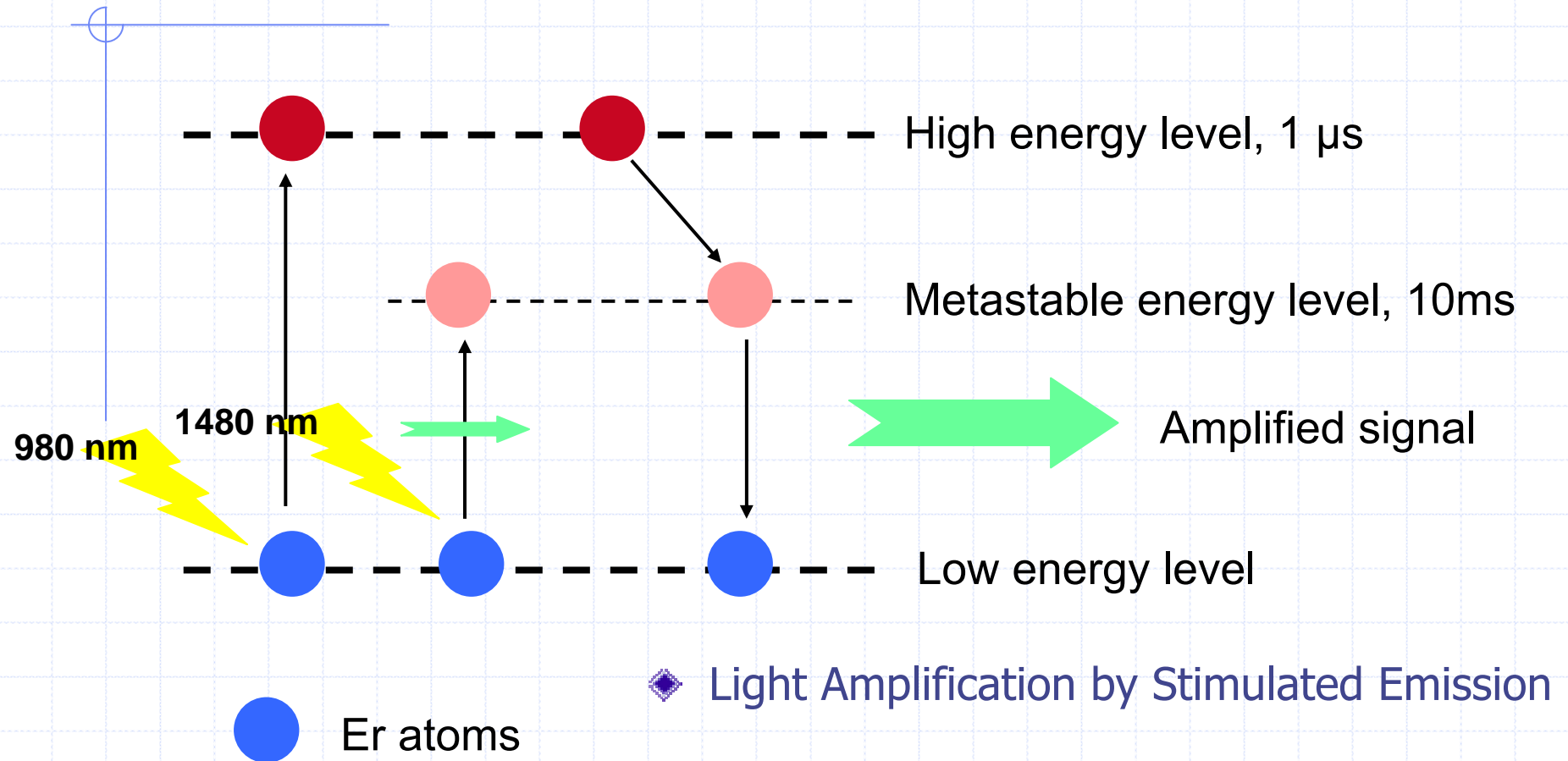
- ◆ Photodetector and demodulator
- ◆ PIN
- ◆ APD (better performance)
- ◆ Receiver sensitivity for certain BER
- ◆ 1 GE: - 34 dBm
- ◆ 10 GE: - 15 dBm/- 24 dBm
- ◆ BER: 10^{-9} , 10^{-12} , 10^{-15}
- ◆ Coherent (transmitted signal plus local oscillator) and incoherent (OOK) receivers

Optical Amplifiers

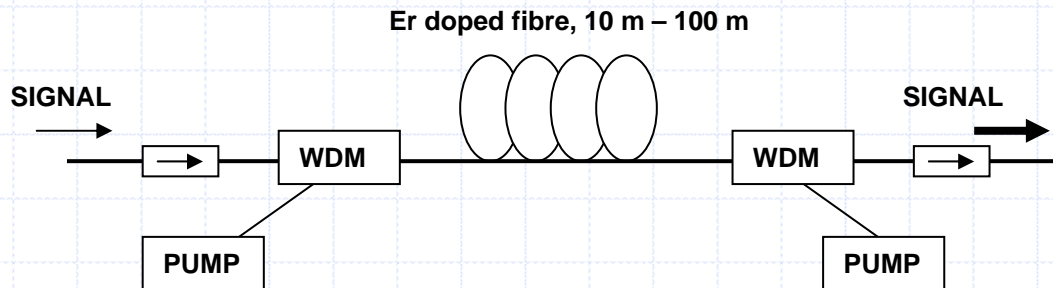
- ◆ Fibre, Semiconductor (SOA), Raman
- ◆ Erbium Doped Fibre Amplifiers (EDFA)
- ◆ Really began a revolution in the telecommunications industry
- ◆ Late 1980s, Payne and Kaming (University of Southampton)
- ◆ OAs can directly amplify many optical signals
- ◆ Protocol, bit-rate transparent
- ◆ EDFAs working in the 1550 nm window (C band and later L band)

Optical networks and equipment

Optical Amplifiers EDFA



Optical Amplifiers EDFA

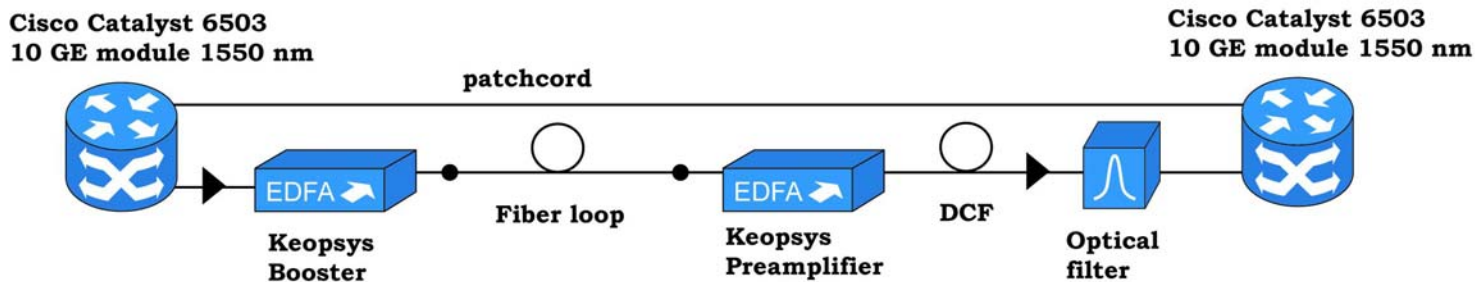
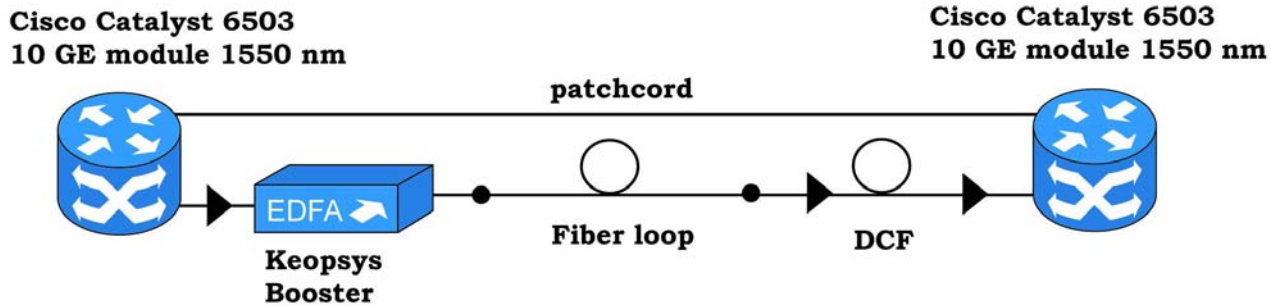


- ◆ Forward, backward pumping
- ◆ Forward: lowest noise
- ◆ Backward: highest output power
- ◆ 980 nm: low noise
- ◆ 1480 nm: stronger pump sources (req. longer Er fibres)
- ◆ 1480 nm & backward; 980 nm & forward
- ◆ Single or dual stage (for DCF)

Optical Amplifiers EDFA

- ◆ Output powers (5 Watts or more)
- ◆ Gain (30 dB), is not uniform across C (L) band
- ◆ Input power (- 35 dBm)
- ◆ Noise Figure (NF): theoretical minimum 3 dB
- ◆ ASE
- ◆ For L band: long Er fibres (> 100 m)
- ◆ Booster, in-line, preamplifiers

Optical Amplifiers



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Other Optical Fibre Amplifiers

- ◆ Praseodymium Doped Fluoride Fibre Amplifier (PDFFA)
 - 1310 nm, not as energy efficient compared to EDFA
 - Problems with fluoride fibres, not very widespread
- ◆ Thulium DFFA (TDFFA)
 - 1460 nm, 1650 nm
 - the lifetime problems
- ◆ Neodymium DFA
 - 1310 nm, fluoride fibre

Semiconductor Optical Amplifiers

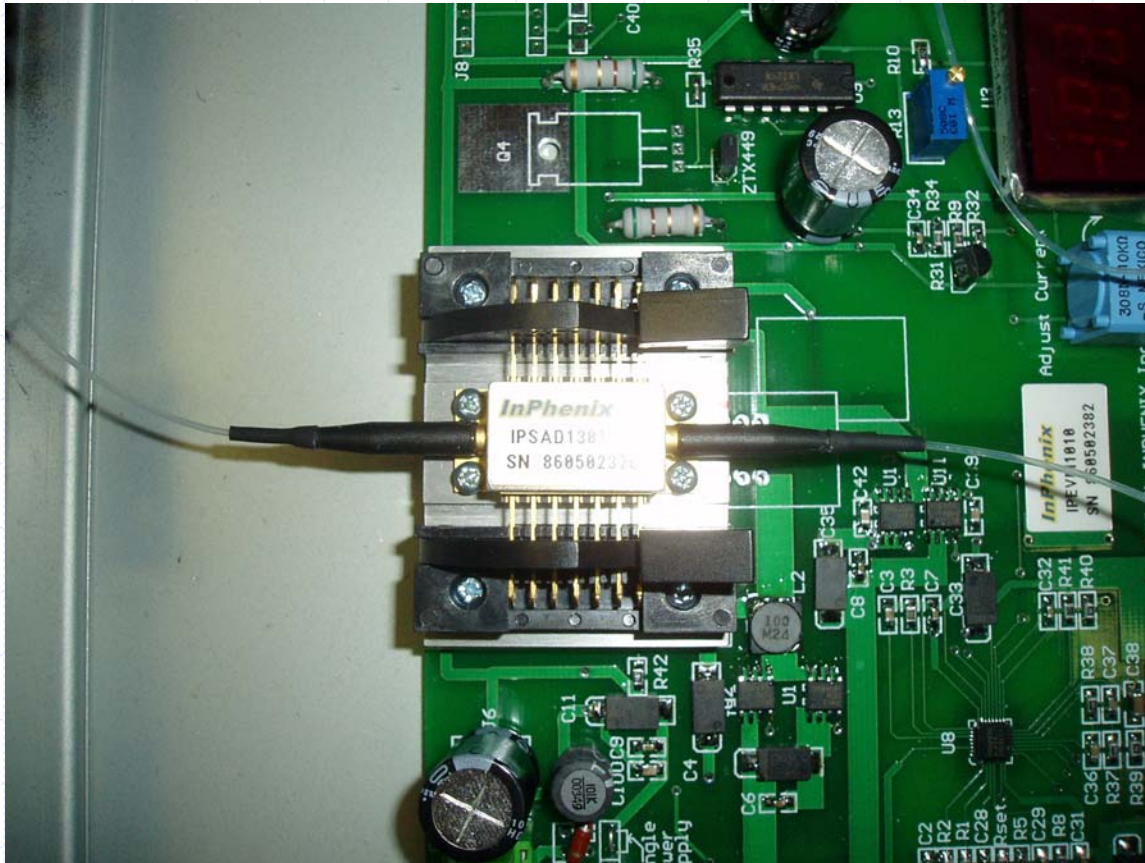
- ◆ Cost effective solutions, especially for 1310 nm window
- ◆ Based on conventional laser principles
- ◆ Active medium (waveguide) between N and P regions
- ◆ High gain (up to 25 dB)
- ◆ Low output powers (15 dBm)
- ◆ Wide bandwidth
- ◆ High noise figure (8 dBm)
- ◆ InGaAsP – small and compact components

Semiconductor Optical Amplifiers

- ◆ Can be used as wavelength convertors, regenerators, time demultiplexors (OTDM), clock recovery devices
- ◆ EDFAs are more powerful and less noisy (but more expensive)
- ◆ But PDFAs are not so widespread and common, optical parameters (output powers and noise figures are not comparable with EDFAs) – SOAs can present an interesting solution
- ◆ 10 GE line cards for PC (PCI-X, PCI-E) S2io (Neterion), Chelsio, Intel with fixed 1310 nm transceivers only
- ◆ The only way to extend a reach is to deploy amplifiers (10 km is not enough, even for MANs in the Czech Republic) or use wavelength convertors (OEO – L2 Ethernet switches)

Optical networks and equipment

Semiconductor Optical Amplifiers



SOAs versus FOAs



Raman Amplification

- ◆ Not a discrete amplifier
- ◆ Stimulated Raman scattering effect
- ◆ Distributed amplification, a communication fibre itself is a gain medium
- ◆ Can add 40 km to increase a maximum transmitter-receiver distance
- ◆ Upgrading of existing links to add more channels
- ◆ A quite weak effect in silica fibre – very high powers have to be used
- ◆ Safety problems (automatic laser shutdown - ALS)

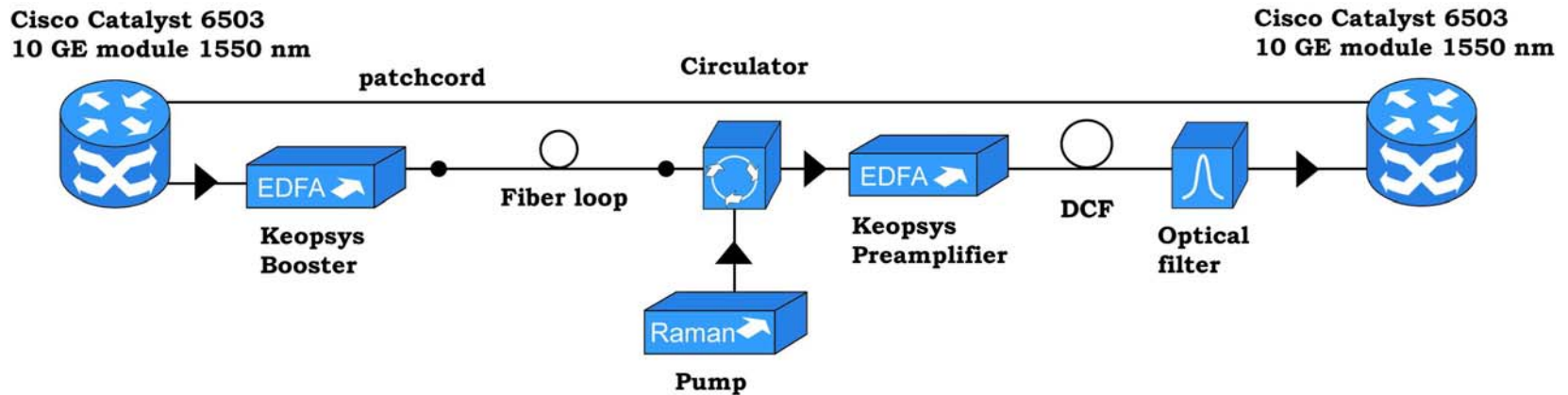
Raman Amplification

- ◆ Double Rayleigh scattering (DRS)
- ◆ Fibre acts like mirrors ie limits launch powers



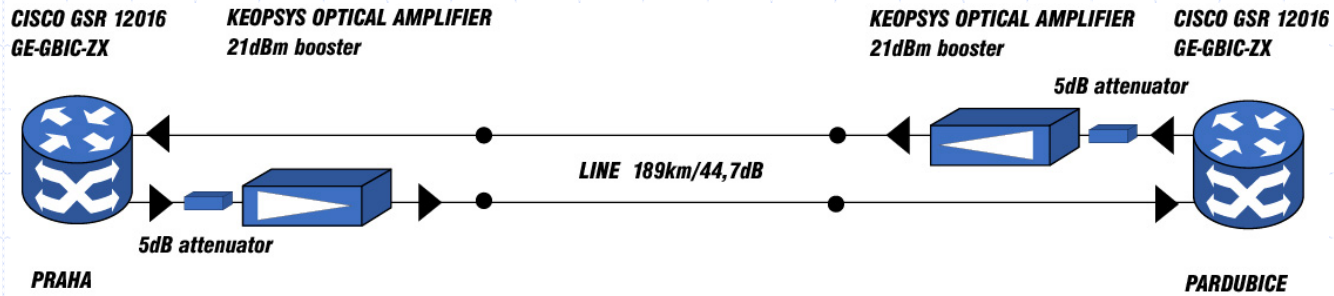
Raman Amplification

- ◆ Counter-directionally pumping schemes

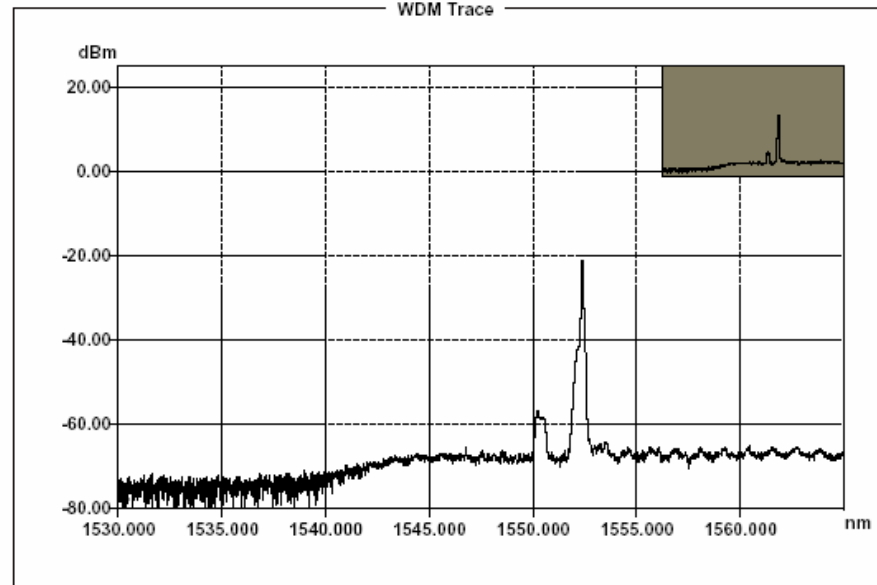


Optical networks and equipment

OAs and Practical Deployment



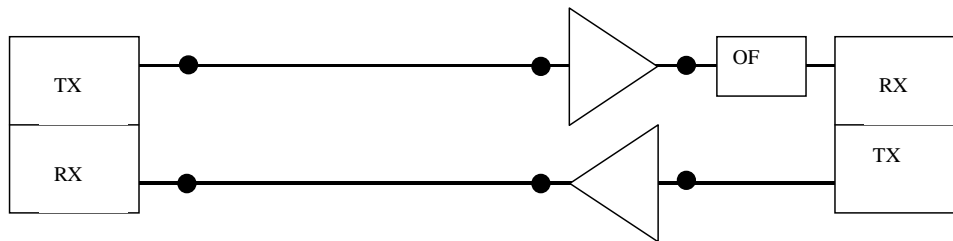
OSA Report



Praha - Pardubice
 Since May 17, 2002

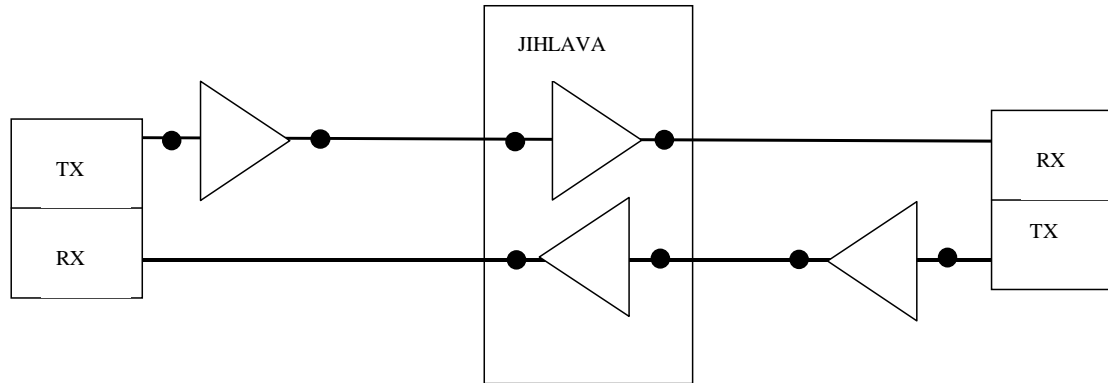
OAs and Practical Deployment

- ◆ Praha – Pardubice, 189 km, 44 dB, 1 GE
- ◆ Praha – Plzeň (One Side Amplification), 123 km, 34 dB, 1 GE



OAs and Practical Deployment

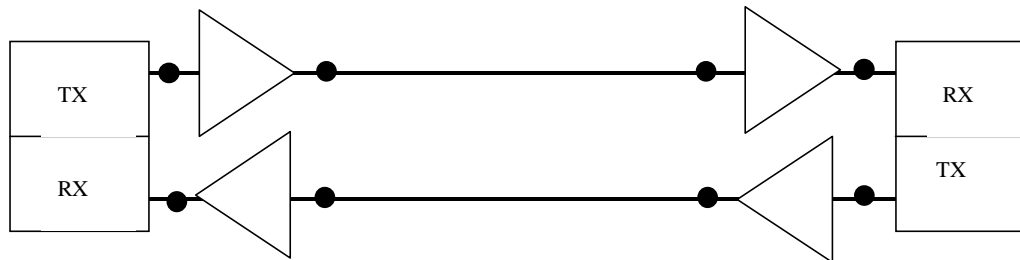
- ◆ Brno – České Budějovice, 308 km, 70 dB, 2,5 Gb/s, PoS, without optical filters



Optical networks and equipment

OAs and Practical Deployment

- ◆ Brno – Ostrava, 235 km, 51 dB, 1 GE (tested for 2,5 G PoS), without optical filters



PDFAs/SOAs and Ramans for 1310 nm

- ◆ Development of high-speed customer empowered fibre networks and availability of 10 GE LAN cards with 1310 nm transceivers stimulates the need for interconnection of stand-alone or hardware accelerated PCs at 10 Gbit/s rate
- ◆ Advantage – zero chromatic dispersion of standard single mode fibres (SSMF) at 1310 nm in, the 1310 nm transceivers are much cheaper than the 1550 nm ones
- ◆ Disadvantage – loss of SSMF at 1310 nm is almost twice as high as at 1550 nm

PDFAs/SOAs and Ramans for 1310 nm

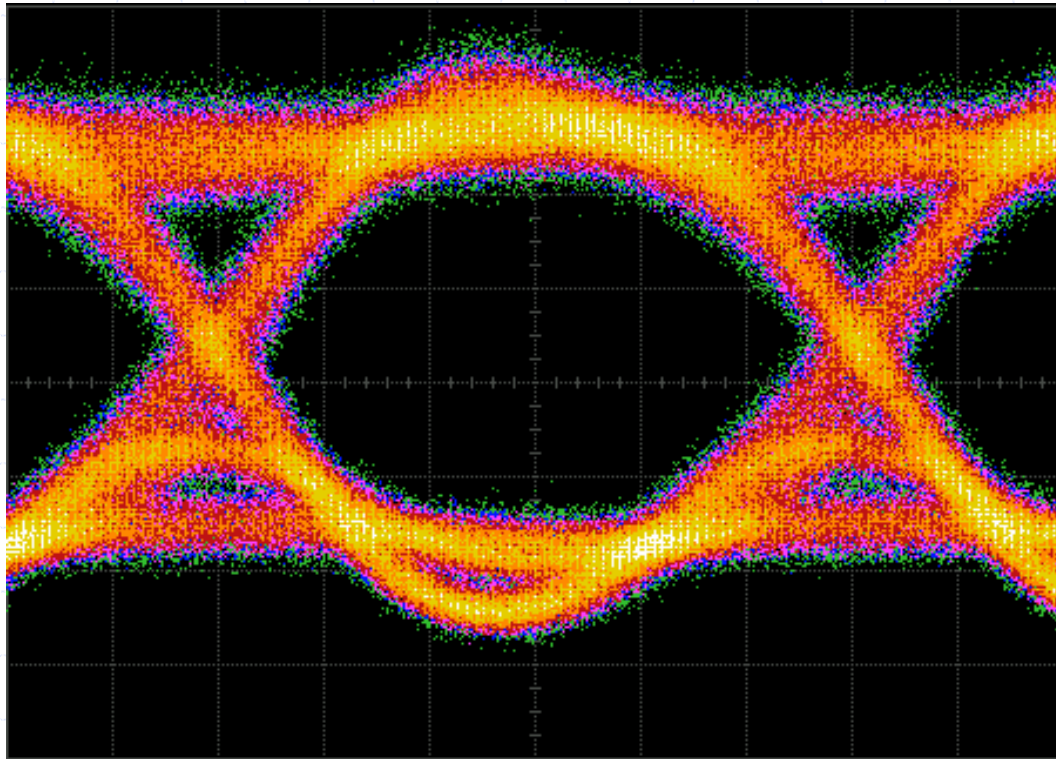
- ◆ Praseodymium-doped fluoride fibre amplifiers (limited number of manufacturers, low saturated output power in comparison with EDFA, FiberLabs, FL8610-OB, $P_{\text{sat}}=16\text{dBm}$, $\text{NF}=5.5\text{dB}$)
- ◆ Distributed amplification in the transmission fibre utilizing stimulated Raman scattering (Raman fibre amplifier (RFA), no pump LDs at 1250 nm, Raman fibre laser, IPG, $P_{\text{outmax}} = 2\text{ W}$ at 1250nm)
- ◆ Semiconductor optical amplifiers (InPhenix, IPSAD1301, $P_{\text{sat}}=10\text{dBm}$, $\text{NF}=7.5\text{dB}$)
- ◆ Experiments with 10 GE

PDFAs/SOAs and Ramans for 1310 nm

- ◆ Similar configuration as for EDFAs plus Ramans
- ◆ Booster or preamplifier only
- ◆ Booster and preamplifier
- ◆ Booster and in-line amplifier
- ◆ Booster, preamp and Raman amplifier
- ◆ Dual booster (to increase the output power) and Raman
- ◆ Booster, inline and Raman

Optical networks and equipment

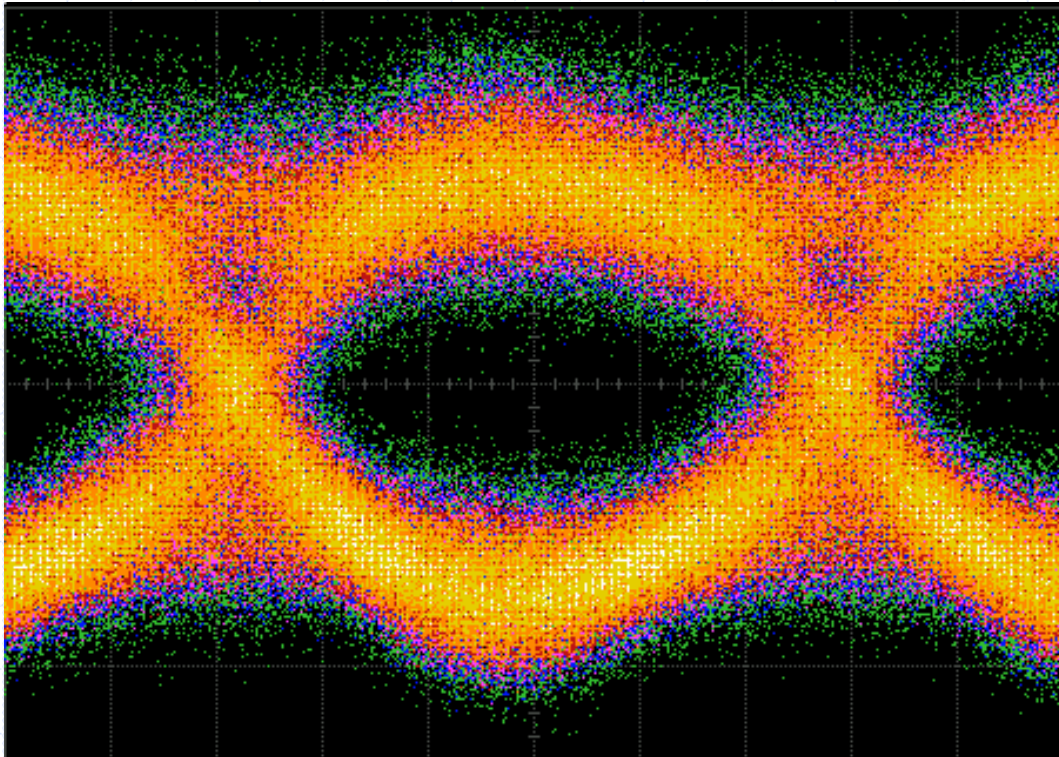
PDFAs/SOAs and Ramans for 1310 nm



Eye diagram after preamp, $l = 100$ km

Optical networks and equipment

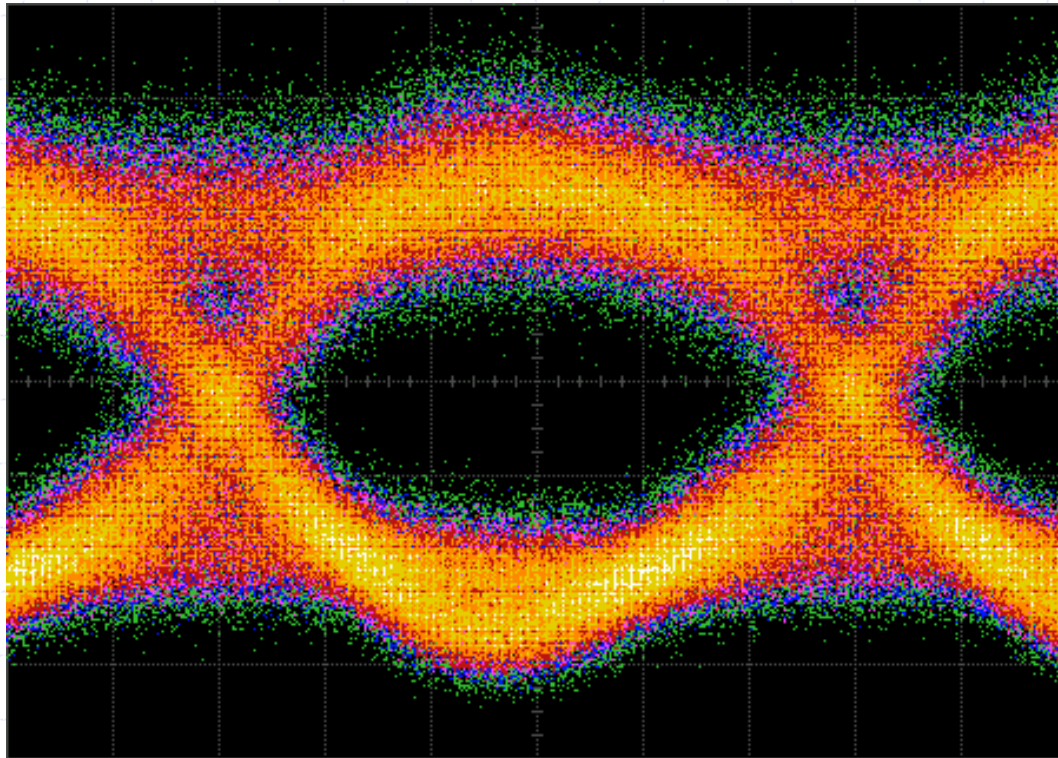
PDFAs/SOAs and Ramans for 1310 nm



Eye diagram after preamp, $l = 120$ km

Optical networks and equipment

PDFAs/SOAs and Ramans for 1310 nm



Eye diagram after preamp and optical filter, $l = 120$ km

Optical networks and equipment

PDFAs/SOAs and Ramans for 1310 nm

Configuration	Reach (km)
Guaranteed	10
In lab, no amps	30
Booster	85
Booster and preamp	120
Dual booster and Raman	135

CzechLight Amplifiers

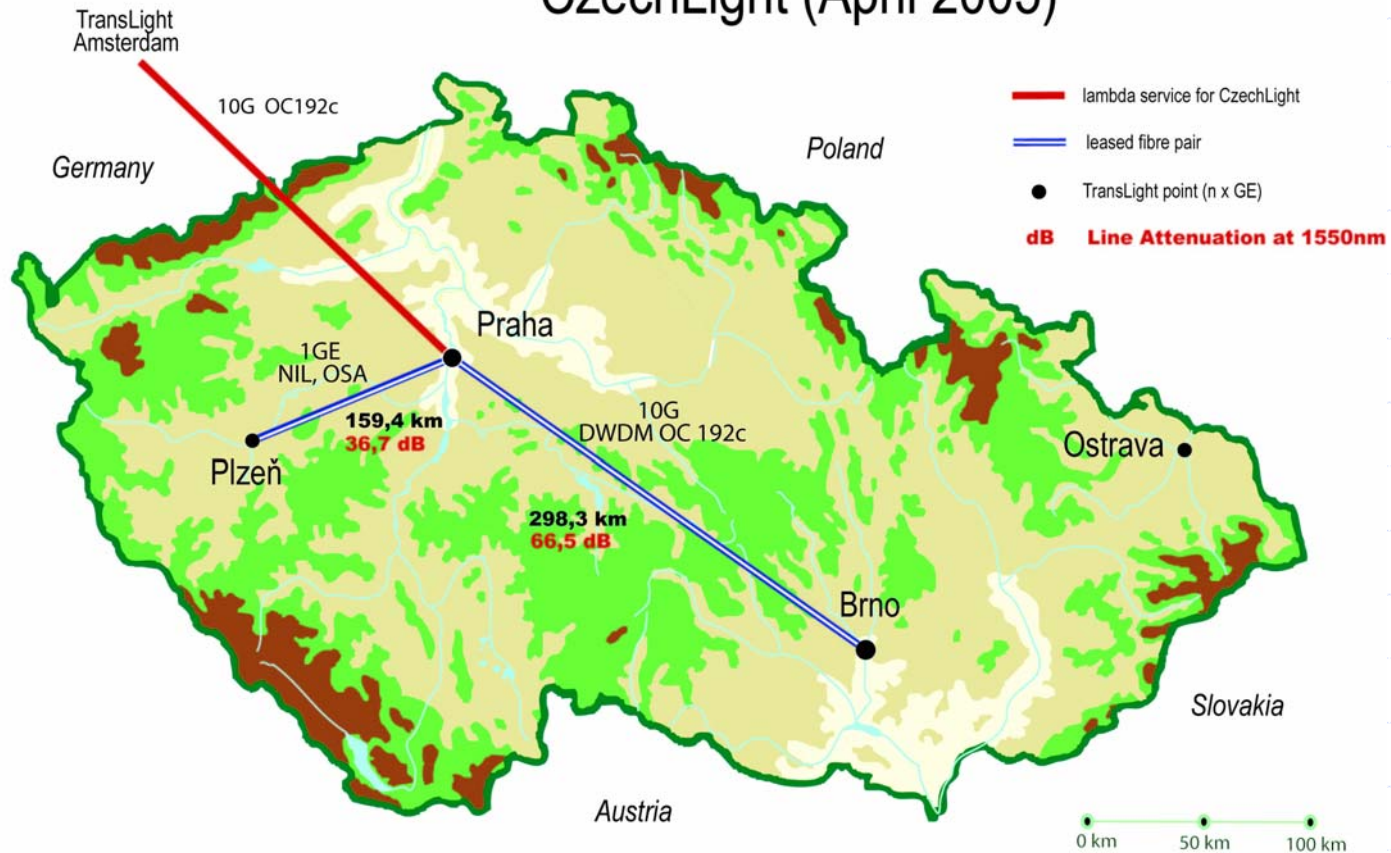
- ◆ An optical kit composed from commercially available elements
- ◆ Cost effectivity & reliability
- ◆ Possibilities of future development
- ◆ Customer based OFA modules – EDFA for 1550 nm, PDFFA for 1310 nm (*10 GE line cards for PC*), Raman modules
- ◆ High power boosters, low-noise preamps, in-line amps...
- ◆ The result is: CzechLight amplifiers (CLAs)
- ◆ Why? What is CzechLight?

CzechLight

- ◆ An experimental and breakable optical network, testbed
- ◆ 10 G lambda to NetherLight (Amsterdam), a part of GLIF
- ◆ Started as 2, G G lambda, back in January 2003
- ◆ To test new components before deployment (lab -> CzechLight -> CESNET2)
- ◆ Experimental traffic for Institute of Physics and other researchers
- ◆ Praha – FermiLab (1 GE)
- ◆ Praha – Taipei (1 GE)
- ◆ For high speed experiments like iGrid2005, SC2005 (full 10 G)
- ◆ <http://www.ces.net/doc/press/2005/pr051219.html>

CzechLight

CzechLight (April 2005)



CzechLight Amplifiers Features

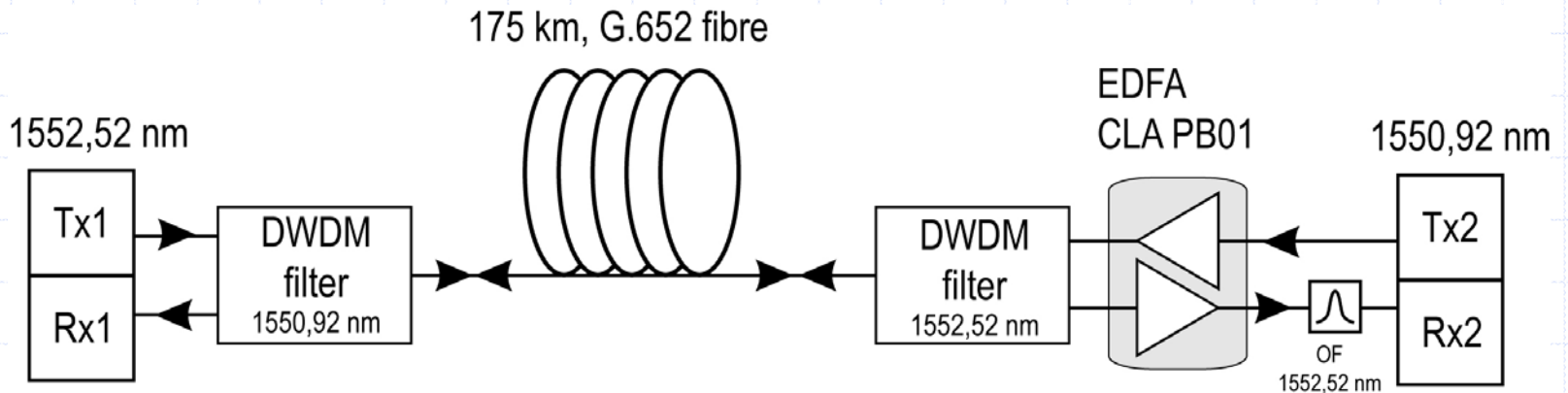
- ◆ Redundant PSUs from industry leading vendor
- ◆ DC voltages, fan speeds, temperatures are monitored
- ◆ Runs on flash disc (no vibration sensitive rotational parts), Linux based
- ◆ Interfaces: RS232, FastEthernet, USB, I²C
- ◆ Extensive management capabilities – console, LAN, GSM/GPRS, Wi-Fi, BlueTooth, SSH, SNMP

CzechLight Amplifiers

- ◆ CLA PB01 – preamplifier and booster, applicable as: DF link terminating OAs, inline OAs with CD compensation and for one side amplified (OSA) DF links
- ◆ OSA – all components are located at one place, star topologies
- ◆ CLA DI01 - dual inline OA, used during iGrid2005 and SC2005 experiments
- ◆ Now looking for manufacturers/partners

CzechLight Amplifiers

- OSA (One Side Amplification) – all components are located at one place, for star topologies



Optical networks and equipment

CzechLight Compensators

- ◆ To eliminate effects of Chromatic Dispersion
- ◆ A big issue for 10 G speeds (and beyond) in 1550 nm
- ◆ Dispersion compensation fibres – lossy, bulky and expensive
- ◆ Fibre Bragg gratings – a relatively new element, DWDM laser is a must (narrow band), today FBGs can compensate for 51 DWDM channels
 - Signal filtering, spectrum shaping
- ◆ Cost effective solution
- ◆ Tuneable FBGs, not possible with DCFs (for e2e lightpaths, lambdas on demand)
- ◆ CLCs (an FBG plus management capabilities)

Optical networks and equipment

CzechLight OOO switches

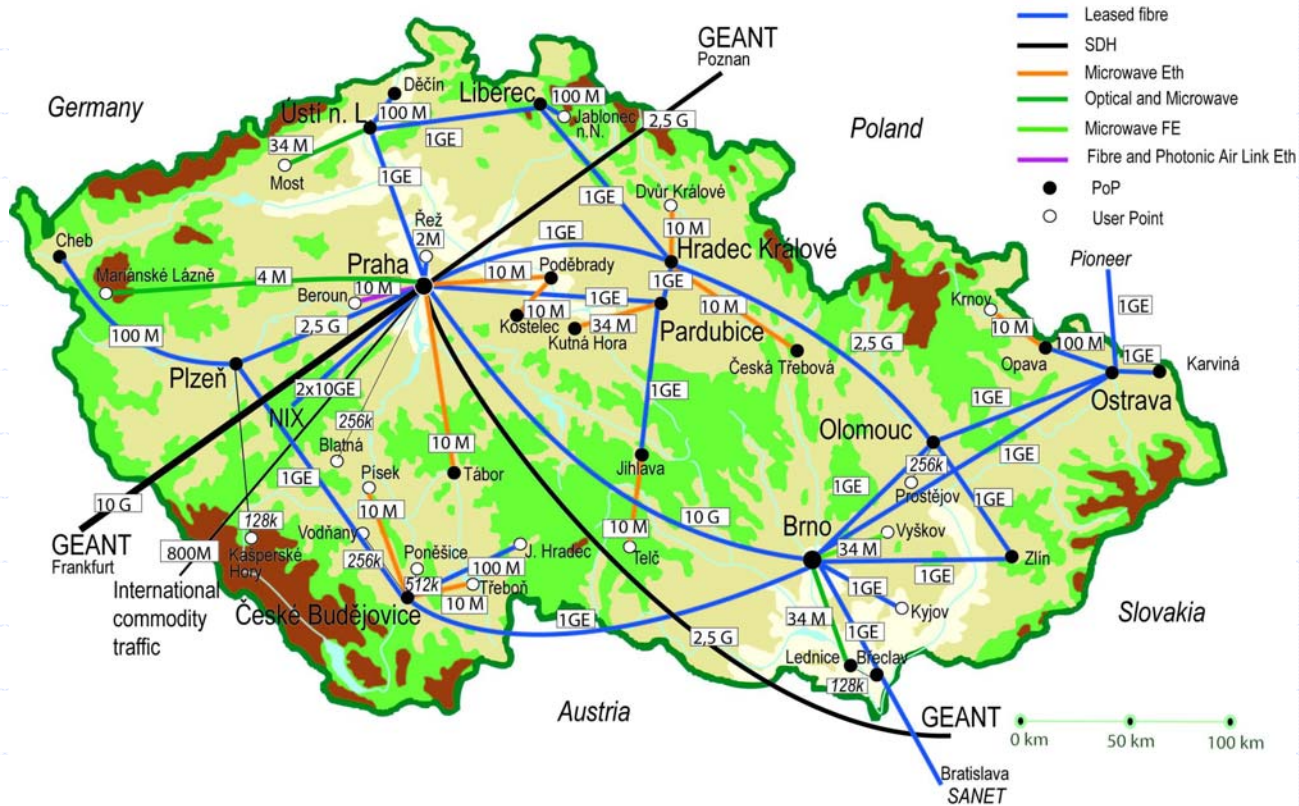
- ◆ The last component for a transparent optical network
- ◆ ROADM vs. OOO switches
- ◆ 8 x 8 switching nonblocking matrix (16 x 16 in future)
- ◆ RS232 for configuring
- ◆ Management dtto CLAs

CLAs Deployment

- ◆ Both in CESNET2 (production) and CzechLight (experimental and breakable) networks
- ◆ Praha – Hradec Králové (CESNET2)
 - 150.4 km of G.652, 35.7 dB@1550nm
 - NIL, OSA (one side amplification) w/ CLA, 1 GE
 - From Dec 2004 till Dec 2005, working without any problem
 - CLA now moved to other edge link
- ◆ New 10 G Cross Border Fibre links to Poland and Austria are being prepared
- ◆ 10 G CBF to Slovakia operational (4 x 10 Gb/s)

CESNET2

CESNET2 Topology (December 2005)



CLAs Deployment

- ◆ Praha – Brno (CzechLight)
 - 298 km, mixture of G.652/G.655+/G.655-, 67 dB@1550nm
 - Not NIL solution, without Ramans but with one inline CzechLight amplifier (DI01)
 - Today 1 channel, 10 G SONET, DWDM transceivers, ready for up to 8 (16 with high power boosters and inline amps) 10 G DWDM SONET/SDH/Ethernet channels
 - Deployment of (tuneable) FBGs and ROADMs/OOO switches is already planned

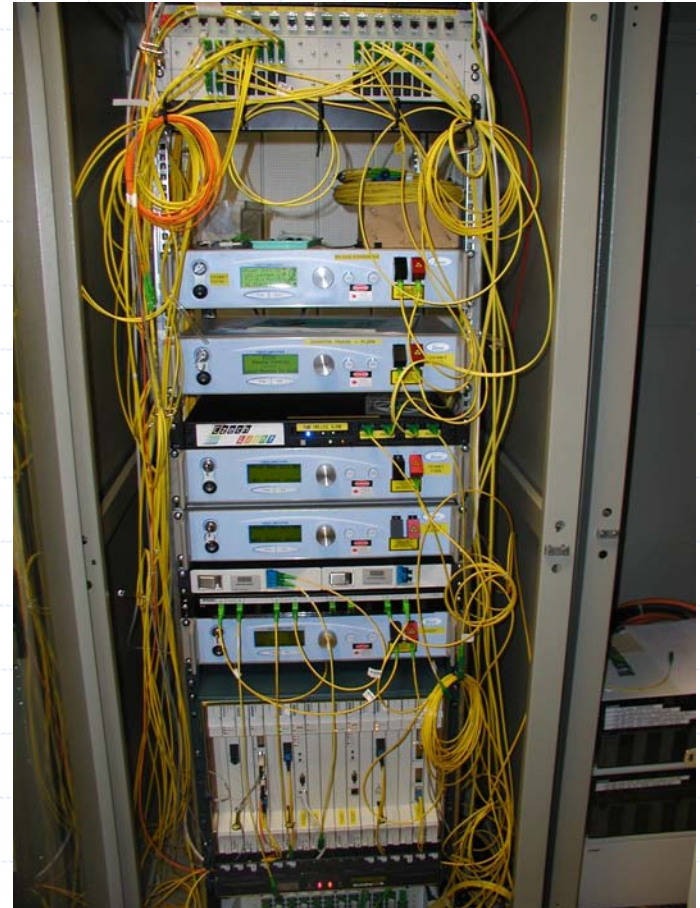
CLAs Deployment

◆ A bit of History :-)

- Started with 302 km of mixture of G.652/G.655+ fibre spools, EDFAs and Ramans, 65 dB@1550nm - working fine
- 297 km testing fibre loops, in the ground, mixture of G.652/G.655+/G.655-, 66 dB@1550nm - working fine
- The „true“ 298 km/67 dB line Praha – Brno was (and still is) sort of bewitched, the BER was too high for our NIL configuration with Ramans :- (

CLAs Deployment

- ◆ Praha – Hradec Králové (CESNET2)
- ◆ The rest of a rack is for CzechLight



CzechLight Equipment and NIL

- ◆ 302 km, 1 x 10 G DWDM channel, in lab on fibre reels
 - With Raman amplifiers and dispersion compensating fibres
- ◆ 250 km, 4 x 10 G DWDM channel, in lab on fibre reels
 - Without Ramans, with Fibre Bragg gratings
- ◆ 135 km, 1 x 10 GE, 1310 nm!, in lab on fibre reels
 - No CD compensation at all, PDFAs and Ramans for 1310 nm
- ◆ One historic footnote from February 2003 (TF - NGN, Rome)
 - 10 Gigabit Ethernet
 - In my opinion, we can go over 40 km :-)
 - Again, our goal is Nothing-In-Line solution
 - The latest result: 252 km, 2 x 10 GE grey 1550 nm channels

Conclusions

- ◆ Development and deployment of new components
- ◆ Especially important (in our opinion) for academic and research community
- ◆ The results will (may) be used in a successor of SEEFIRE, GN2 (Joint Research Activities), Porta Optica
- ◆ Cross Border Fibre solutions
- ◆ Metropolitan Area Networks, Regional Optical Networks

Acknowledgement

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Optical networks and equipment

