



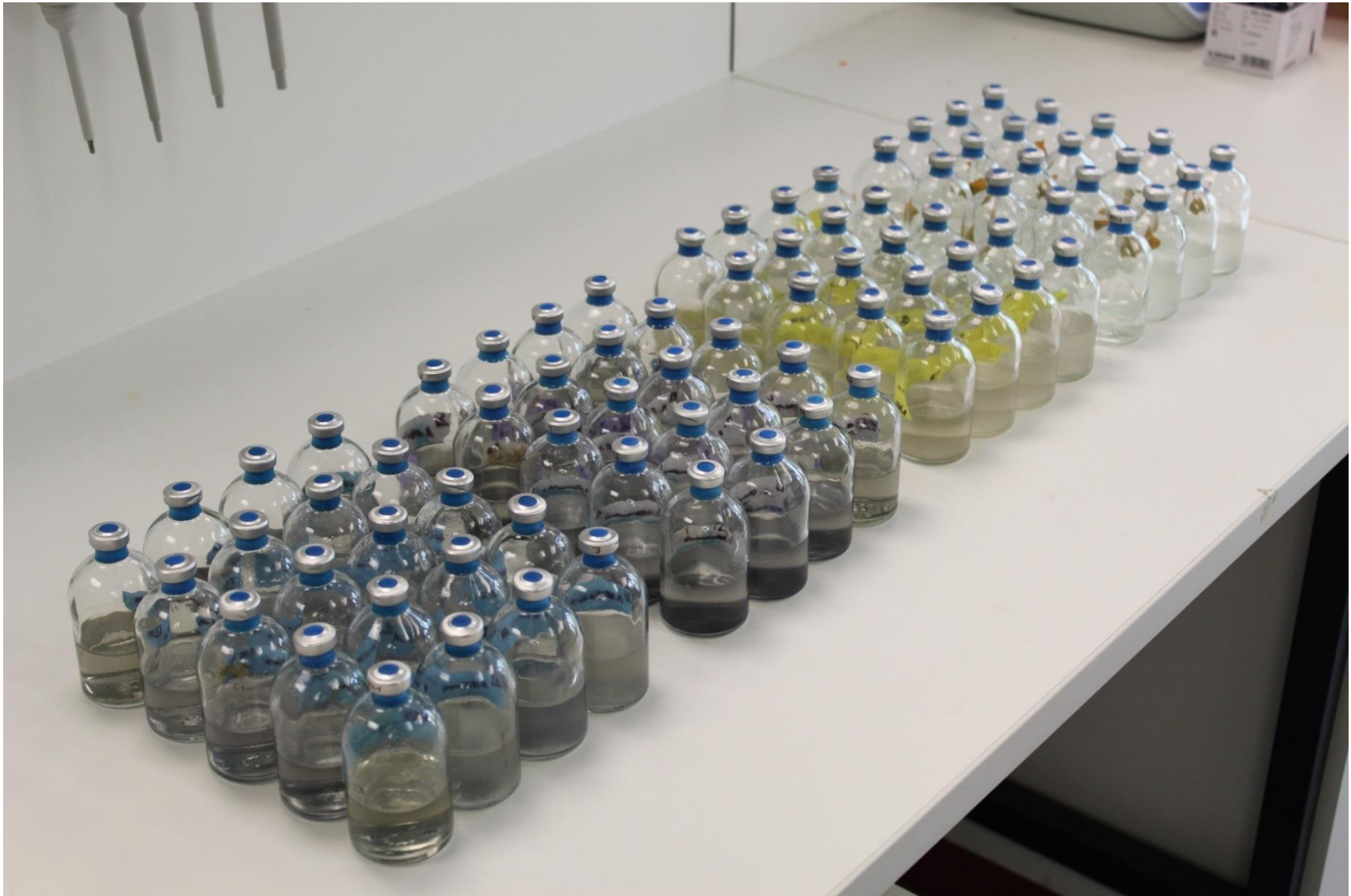
# **Cultivation and Bioprocessing Techniques & Design of Experiments (DoE)**

**Dr. Simon K.-M. R. Rittmann**

# Cultivation & Bioprocessing Techniques

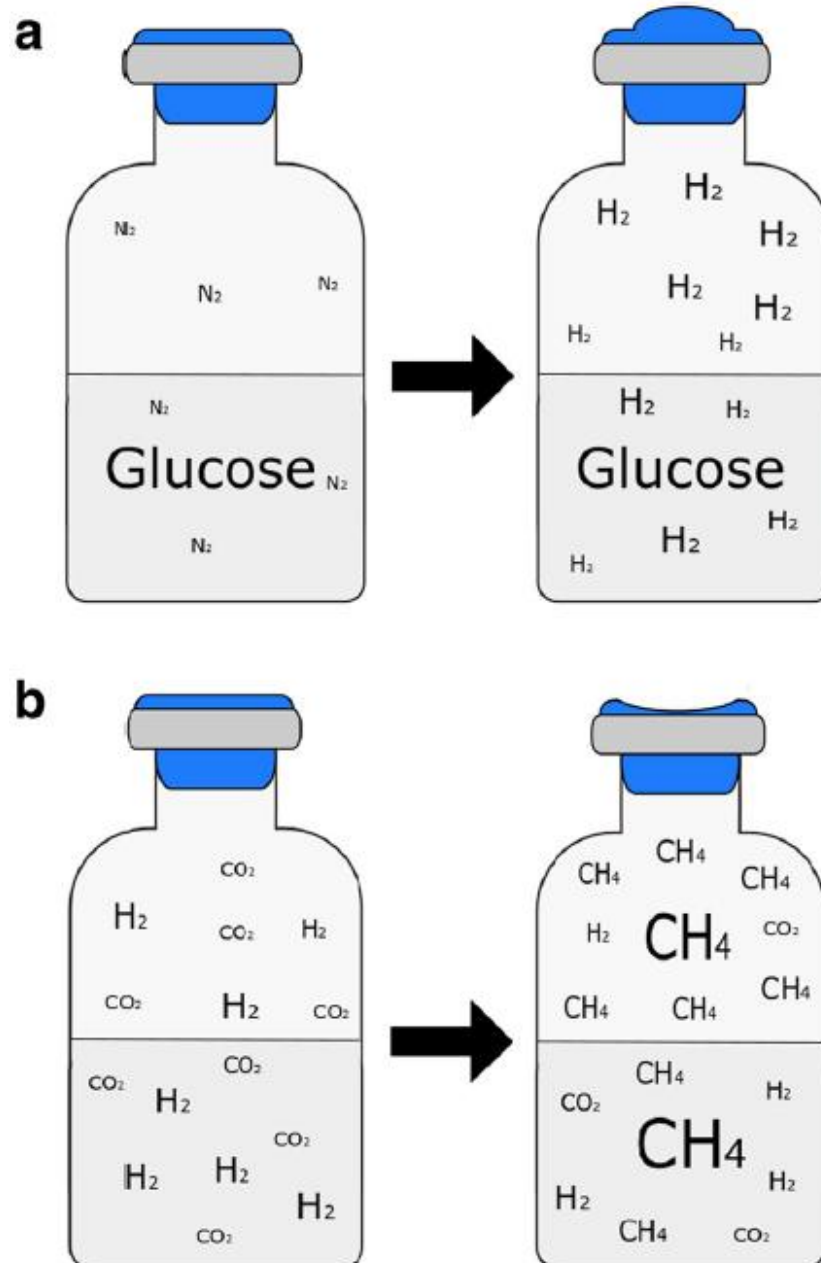
- 1. Closed batch (serum bottles, usually anaerobic)**
- 2. Batch (e.g. Erlenmeyer flask, uncontrolled conditions)**
- 3. Batch (bioreactor, (un)controlled conditions)**
- 4. Fed-batch (bioreactor, controlled conditions)**
- 5. Continuous culture (bioreactor, controlled conditions)**

# Closed batch



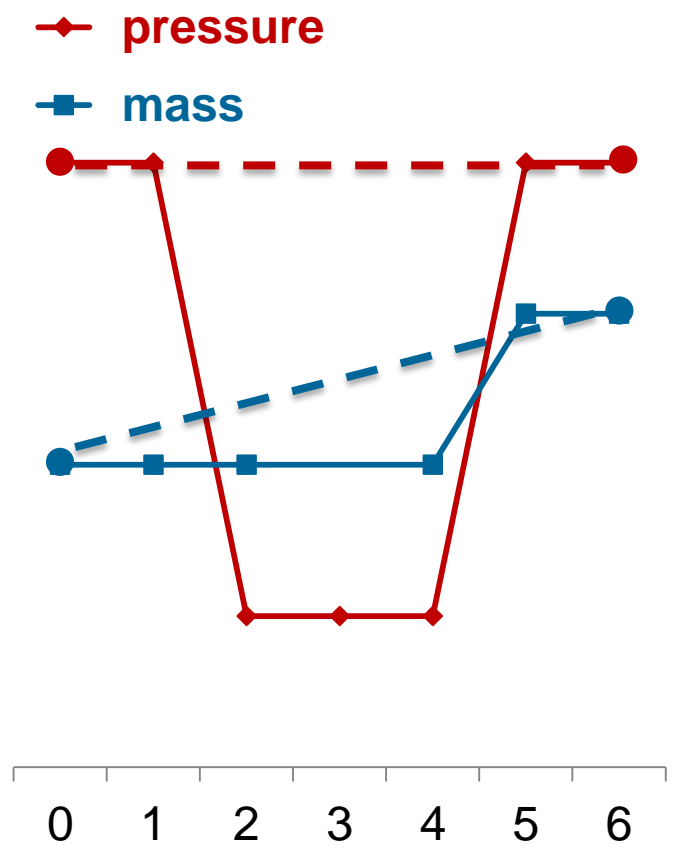
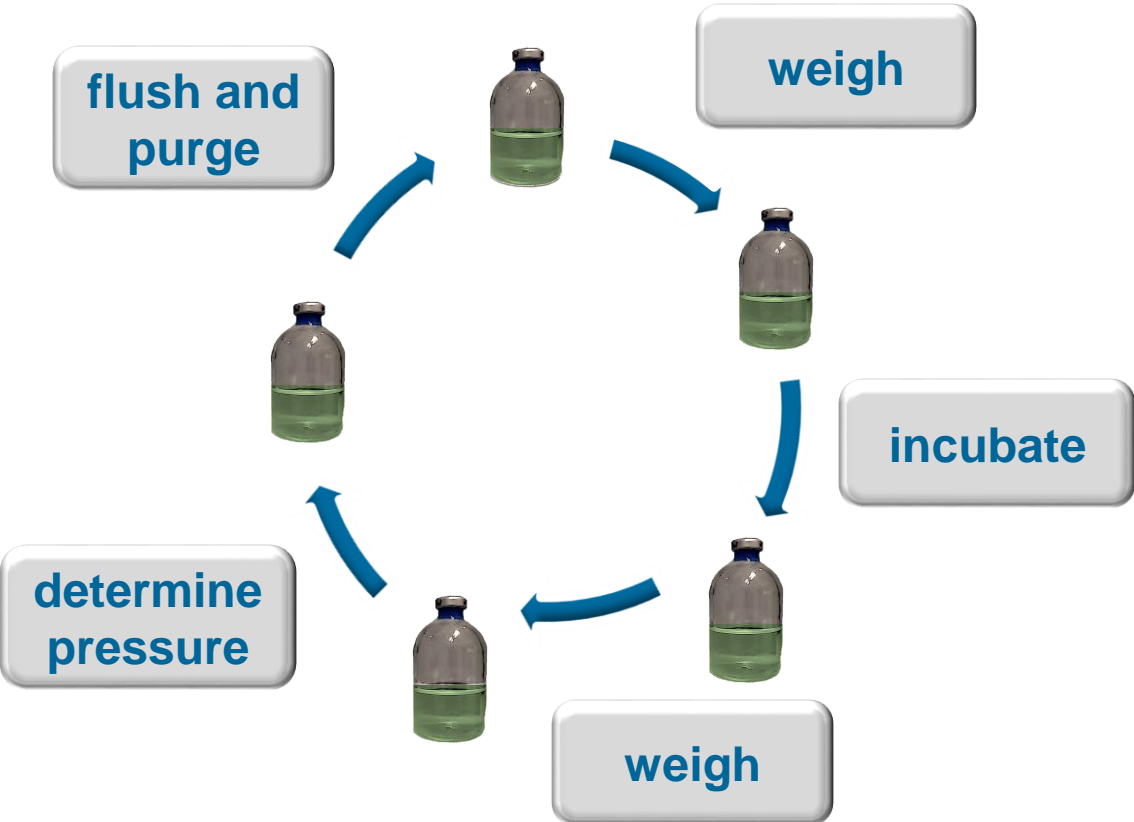
Closed batch cultivation of *Methanothermobacter marburgensis*, *Methanothermococcus okinawensis*, *Methanocaldococcus villosus* and *Methanosarcina soligelidi* in 120 mL serum bottles.

# Closed batch

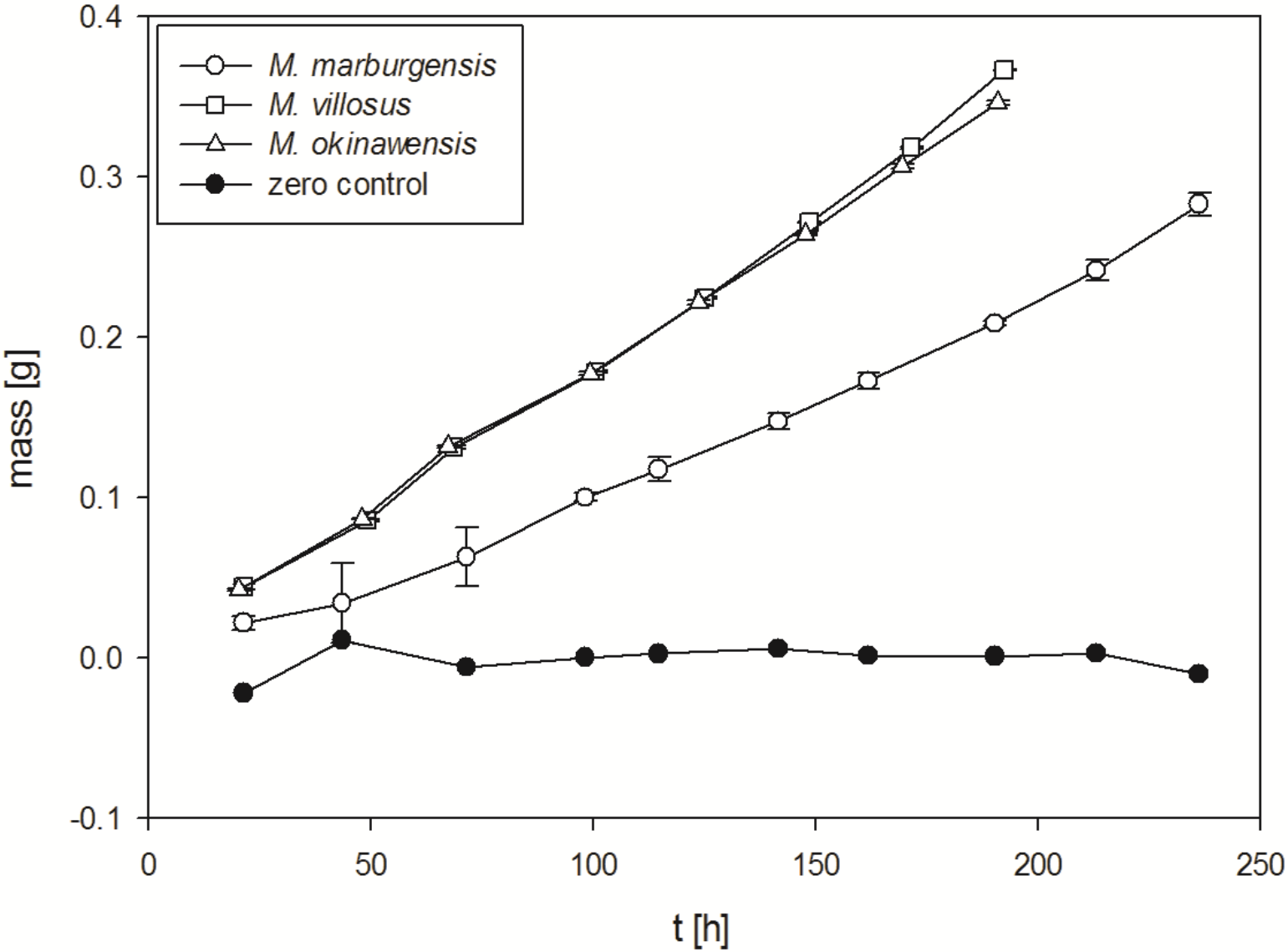


**Fig. 4** Anaerobic closed batch cultivation set-up (serum bottle) supplemented with (a) a liquid substrate, glucose, and (b) a gaseous substrate,  $H_2/CO_2$ . **a** Cultivation of a  $H_2$ -producing microorganism:  $H_2$  production from glucose leads to a pressure increase in the serum bottle. **b** Cultivation of a methanogenic archaeon: closed batch cultivation with discontinuous  $H_2/CO_2$  gassing. The conversion of  $H_2/CO_2$  to  $CH_4$  leads to a pressure drop in the cultivation device due to the following stoichiometric formula ( $4H_2 + CO_2 \rightarrow CH_4 + 2H_2O$ )

# Closed batch

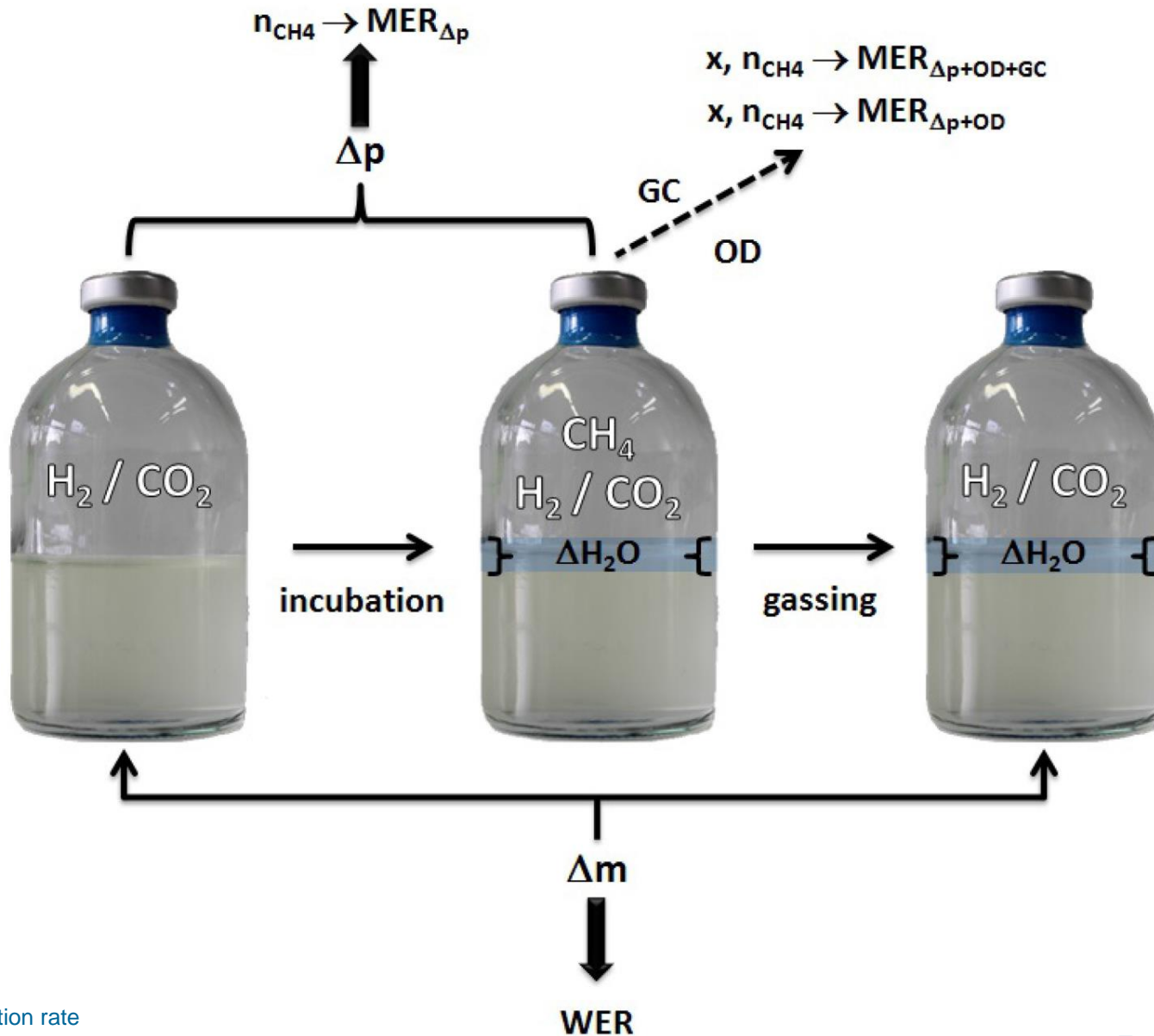


# Closed batch



Cummulative H<sub>2</sub>O production of *M. marburgensis*, *M. villosus* and *M. okinawensis* in 120 mL serum bottles. Growth conditions: T = 65, 80 and 60°C, respectively, V = 50 mL, n = 9, 3 and 3, respectively.

# Closed batch



## General mass balance

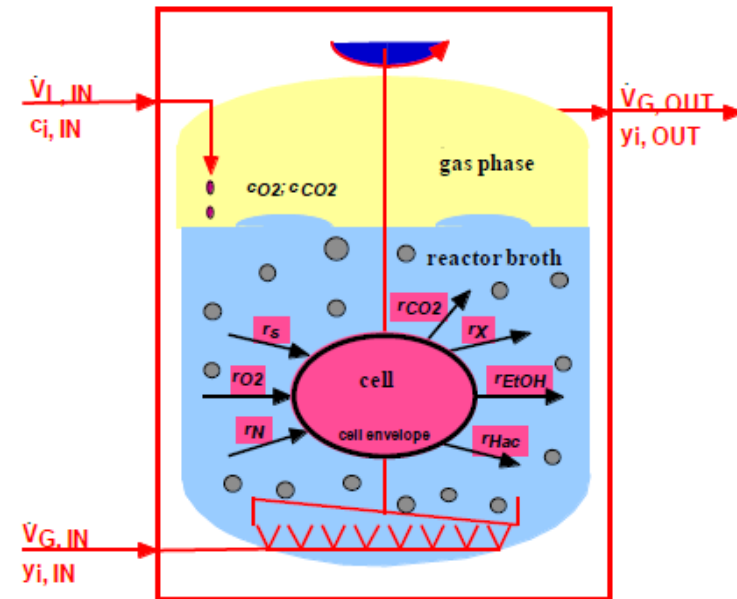
$$\dot{V}_{In} c_{i,In} - \dot{V}_{Out} c_{i,out} + V_R r_i = V_R \frac{\partial c_i}{\partial t} + c_i \frac{\partial V_R}{\partial t}$$

$c_i$  = concentration of component i

$V_R$  = reactor volume

$\dot{V}$  = volumetric flowrate

$r_i$  = reaction rate of component i = production – uptake

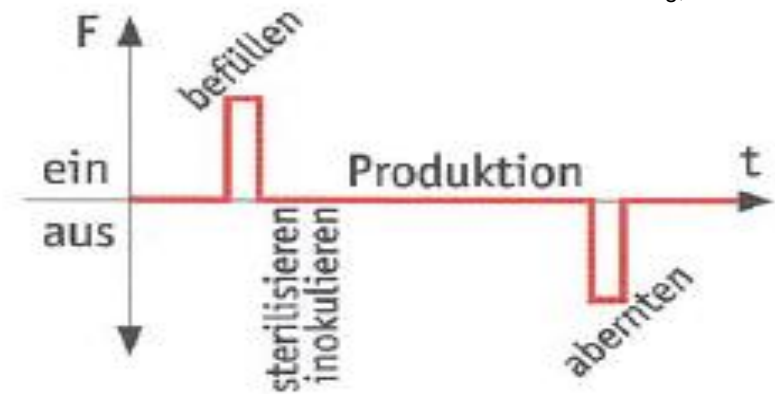
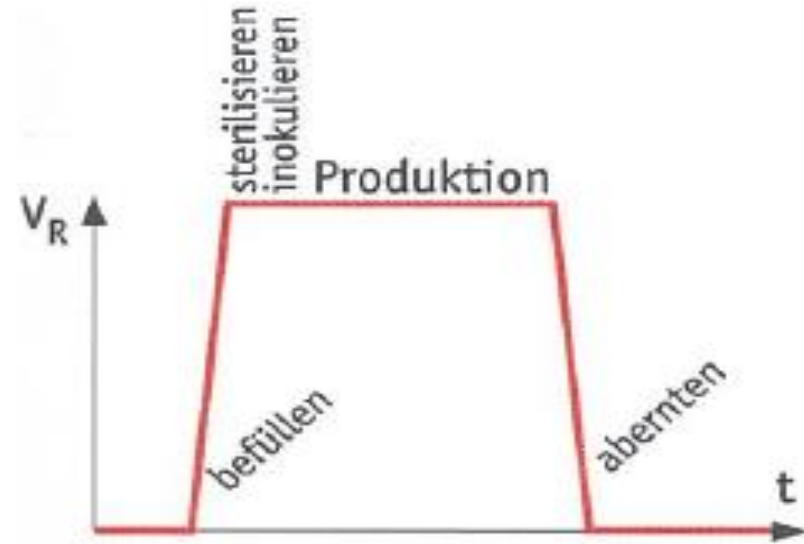




# Batch & Fed-batch



## Satzverfahren (batch)

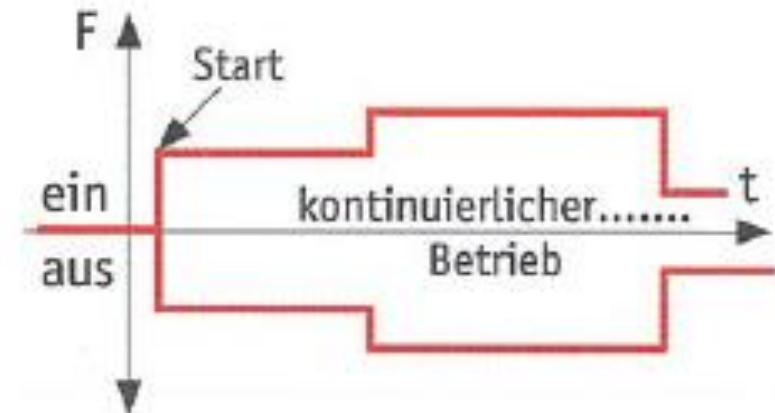


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Spektrum  
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Verlag, 2006

## Kontinuierliche Kultur (continuous culture)



## Mass balance for batch and fed-batch

- Batch

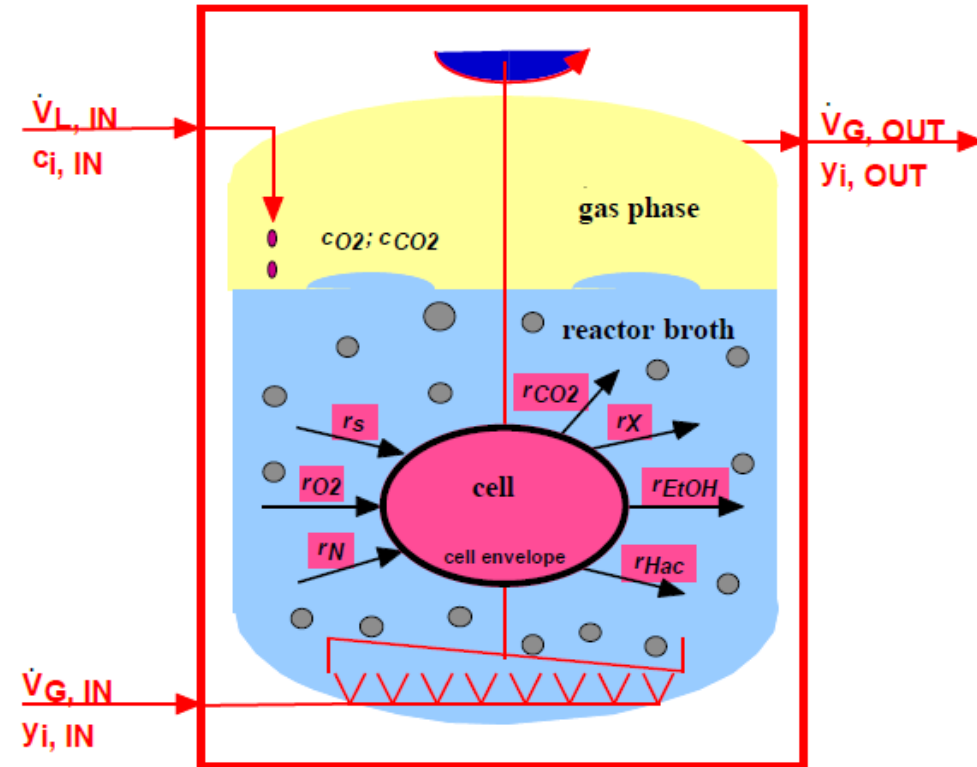
- $i$  = liquid component!

$$V_R r_i = V_R \frac{\partial c_i}{\partial t}$$

- Fed-Batch

- $i$  = limiting added component!

$$\dot{V}_{In} c_{i,In} + V_R r_i = V_R \frac{\partial c_i}{\partial t} + c_i \frac{\partial V_R}{\partial t}$$



Exponentieller Feed

$$\dot{V}_{In} = \dot{V}_0 \exp(\mu t)$$

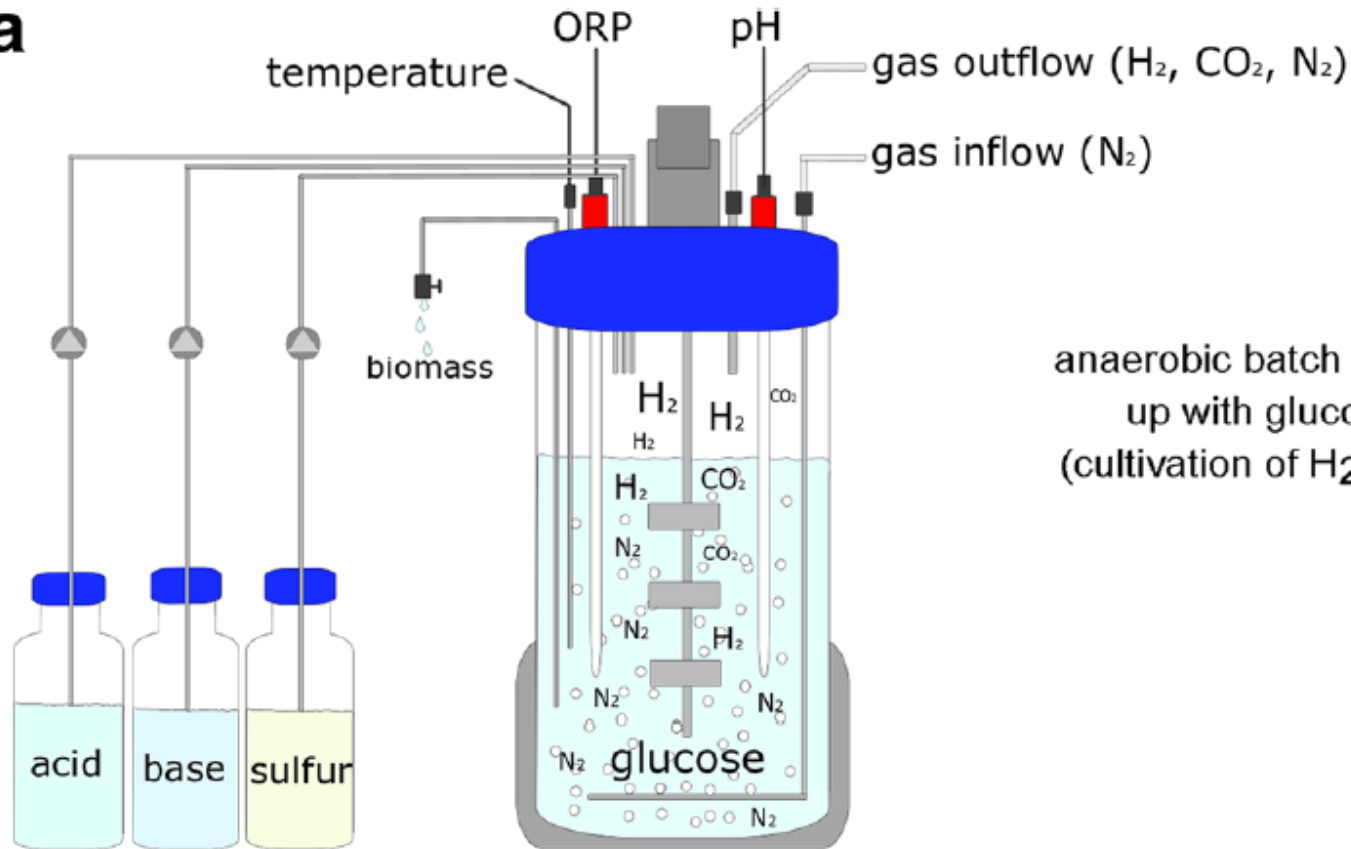
Beschleunigter Feed (Accelerostat)

$$\dot{V} = \dot{V}_0 \exp((\mu + \alpha t)t)$$

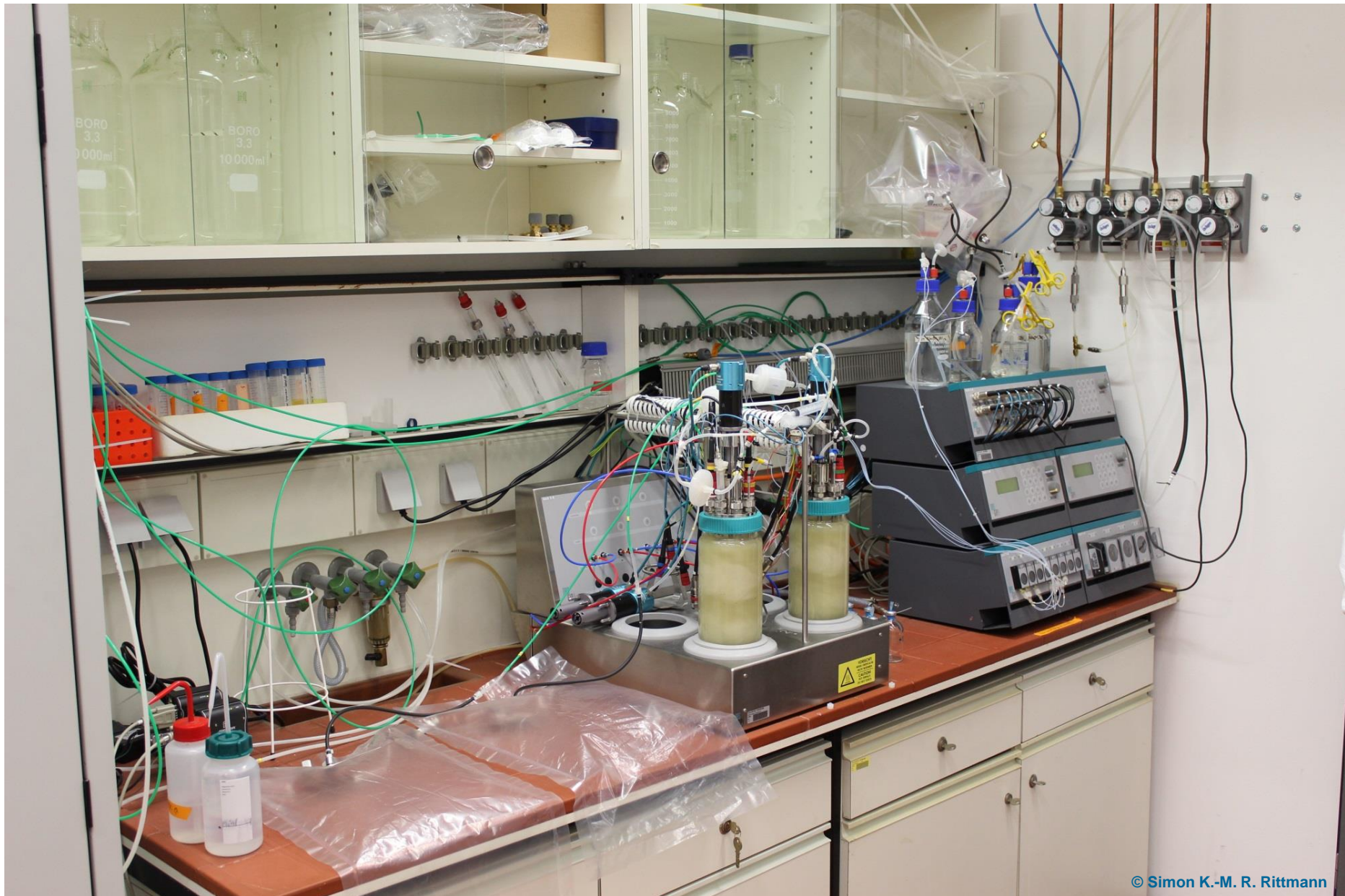
Konstanter Feed

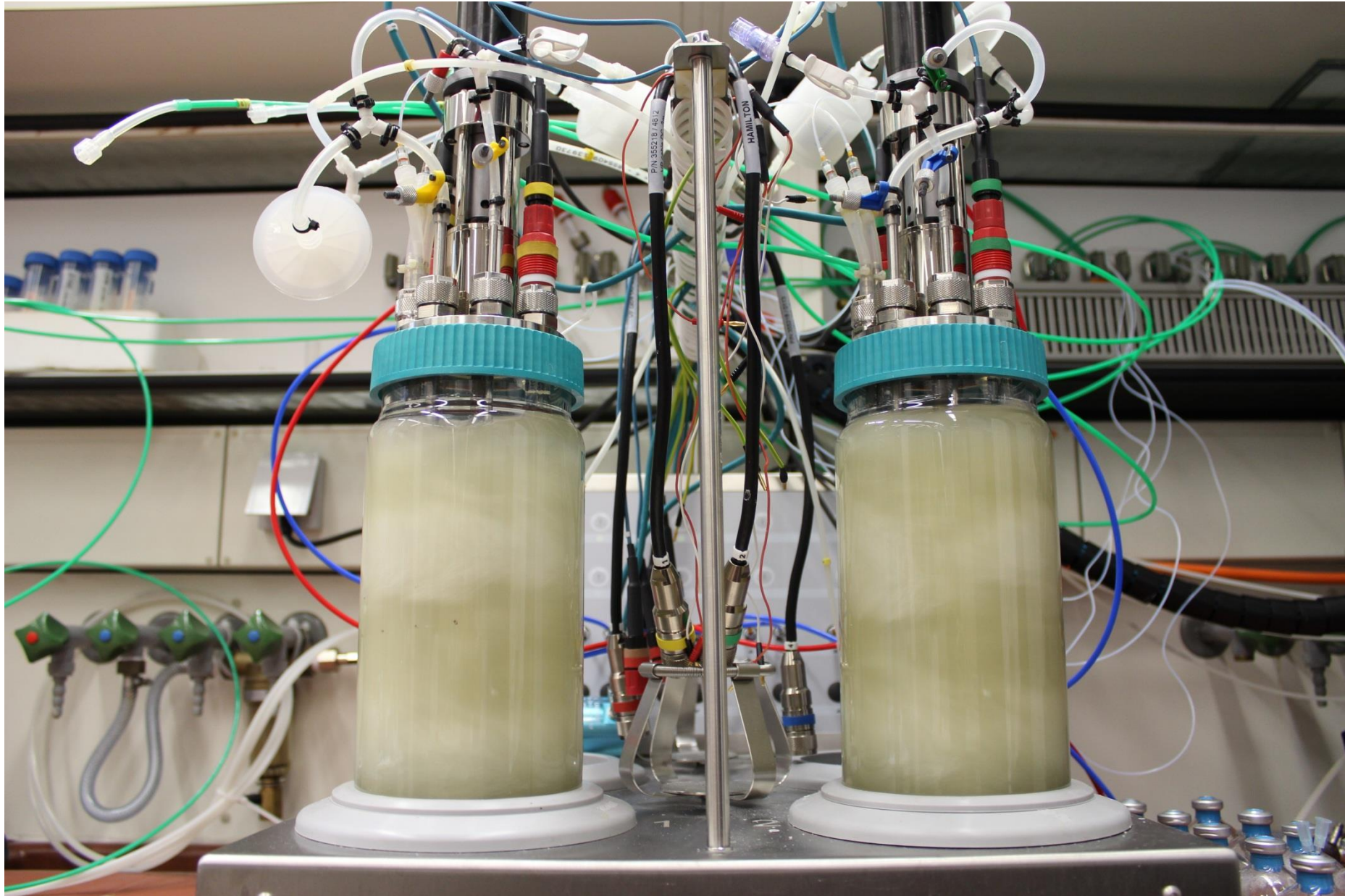
$$V_R(t) = V_{R,0} + \dot{V}_{In} t \text{ und } \dot{V}_{In} = \frac{\partial V_R}{\partial t} = const.$$

**a**



anaerobic batch fermentation bioreactor set-up with glucose as a liquid substrate (cultivation of  $H_2$ -producing microorganism)

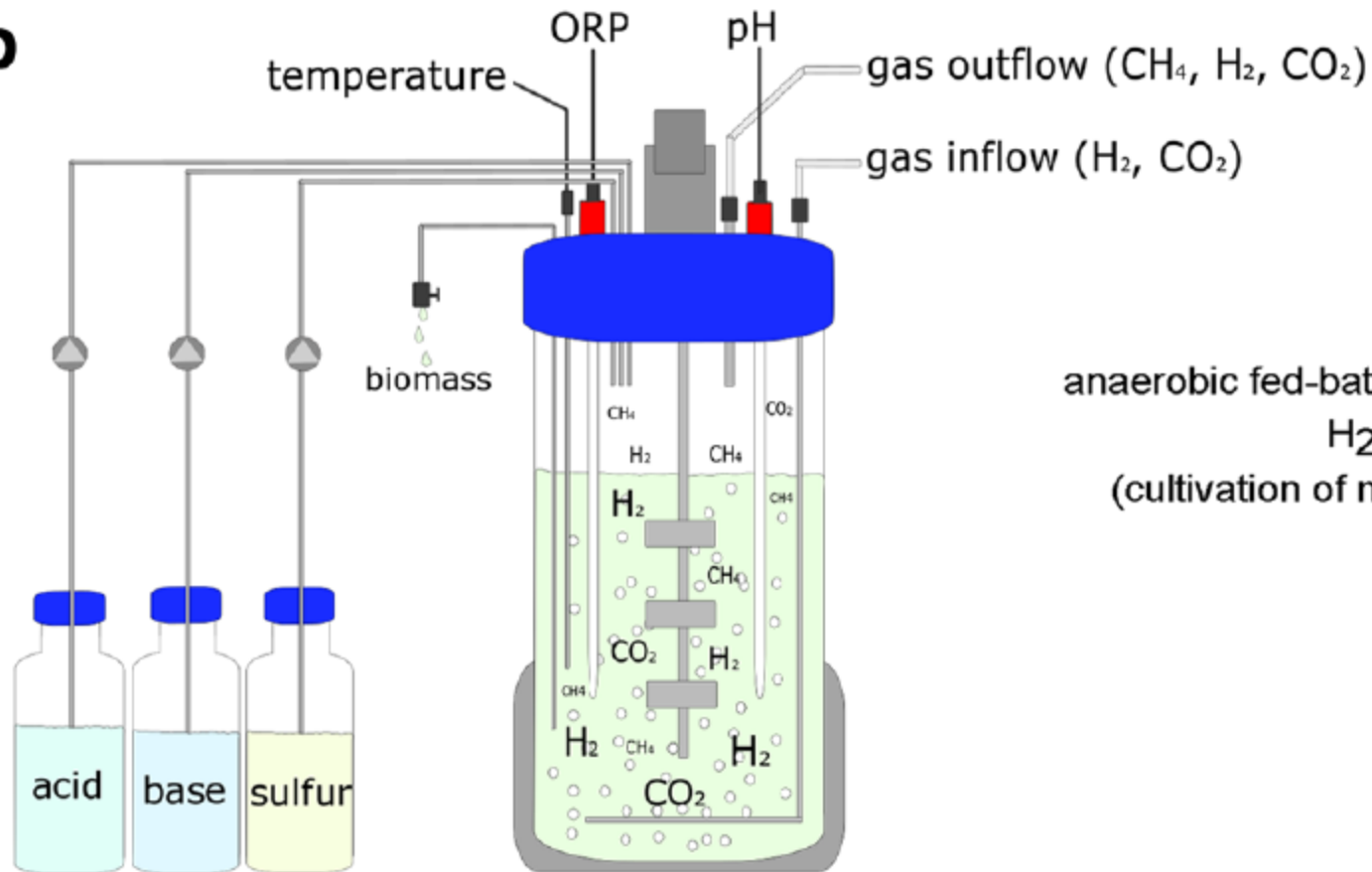




Fed-batch fermentation of *Methanothermobacter marburgensis* in the Eppendorf bioreactor system.

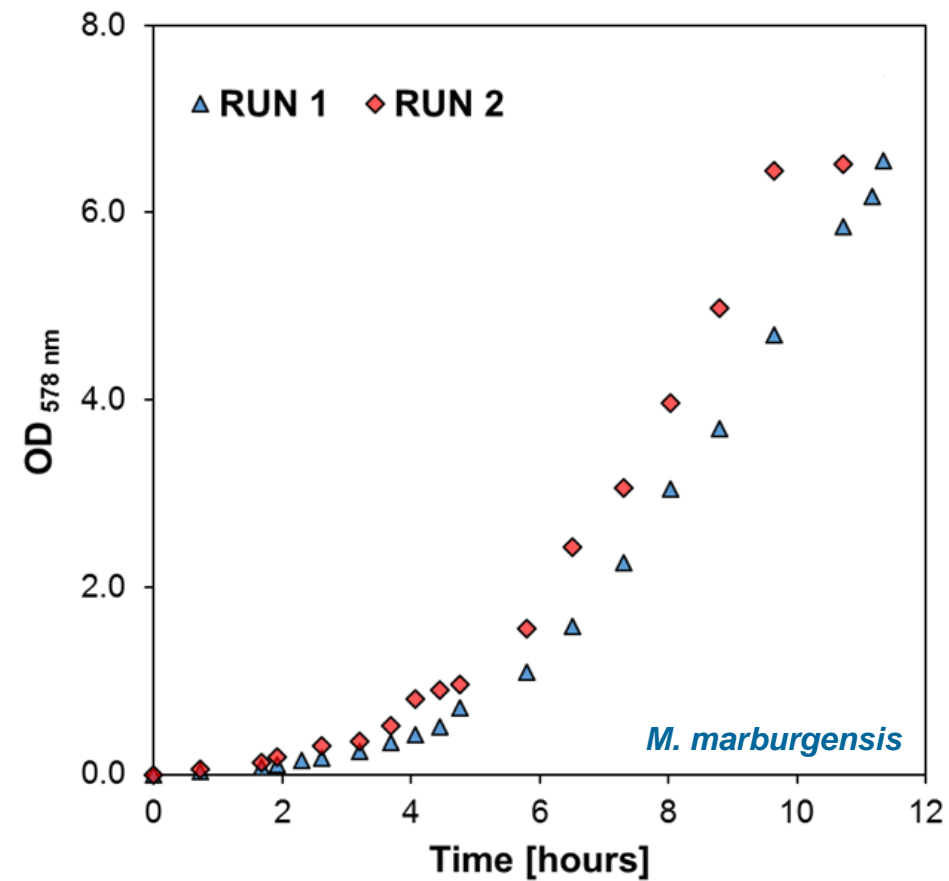
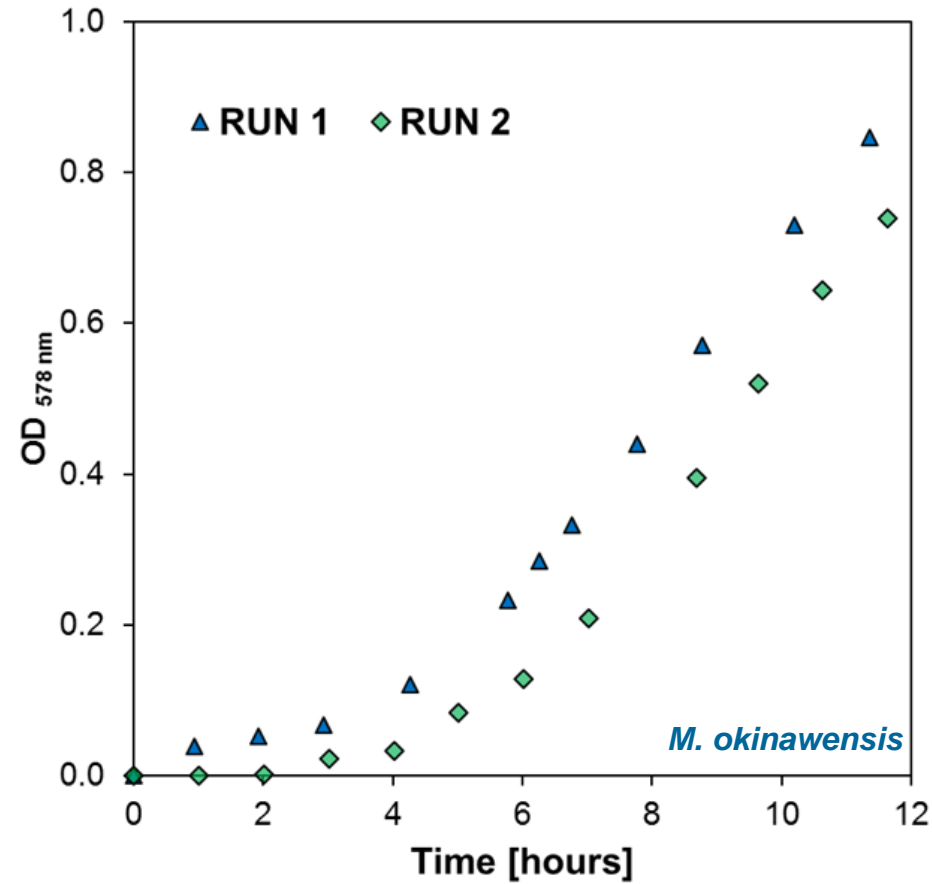
# Fed-batch

**b**



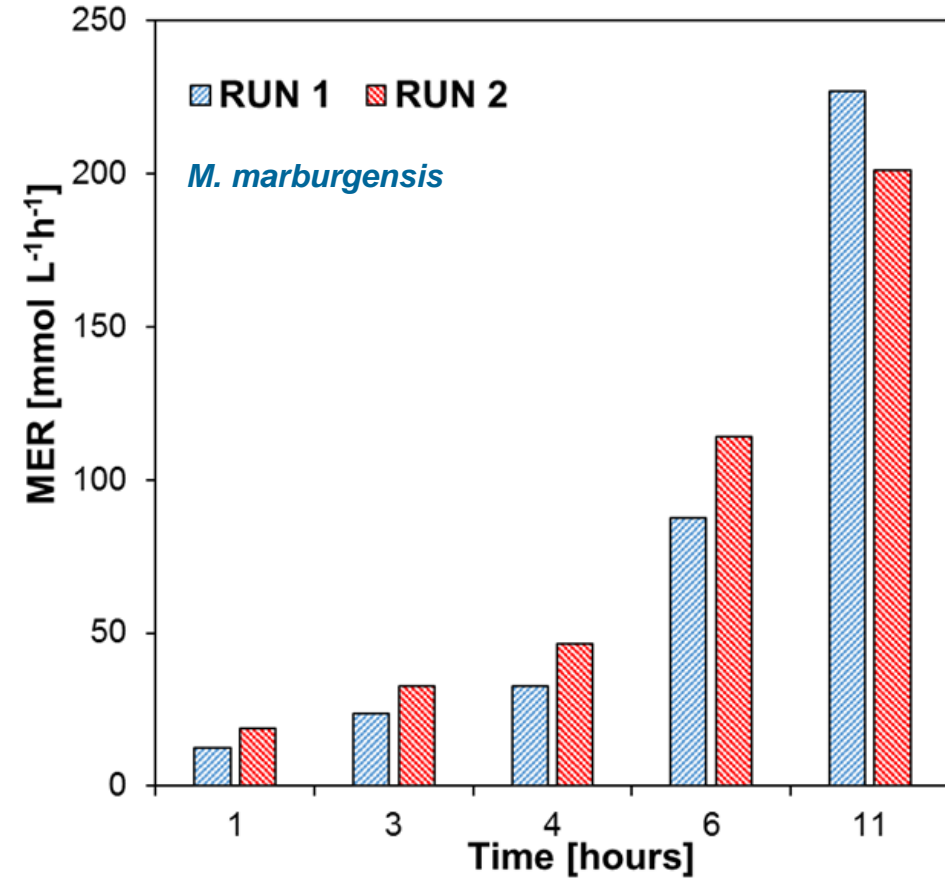
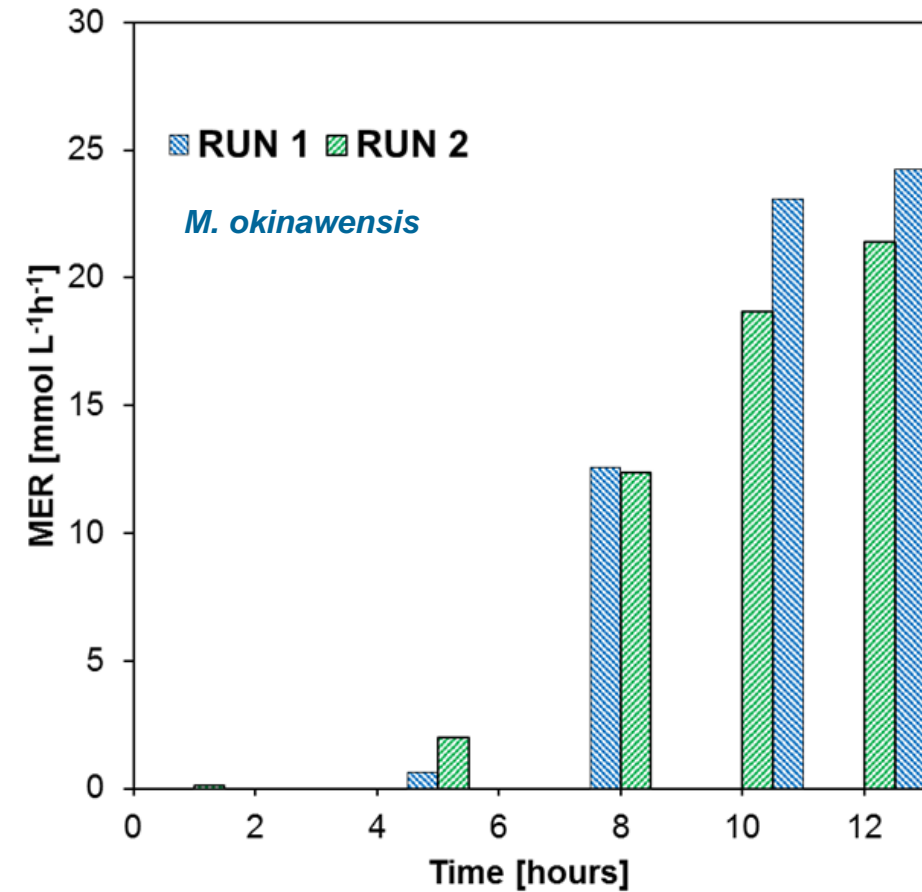
anaerobic fed-batch bioreactor system with  
H<sub>2</sub>/CO<sub>2</sub> feed  
(cultivation of methanogenic archaea)

# Fed-batch



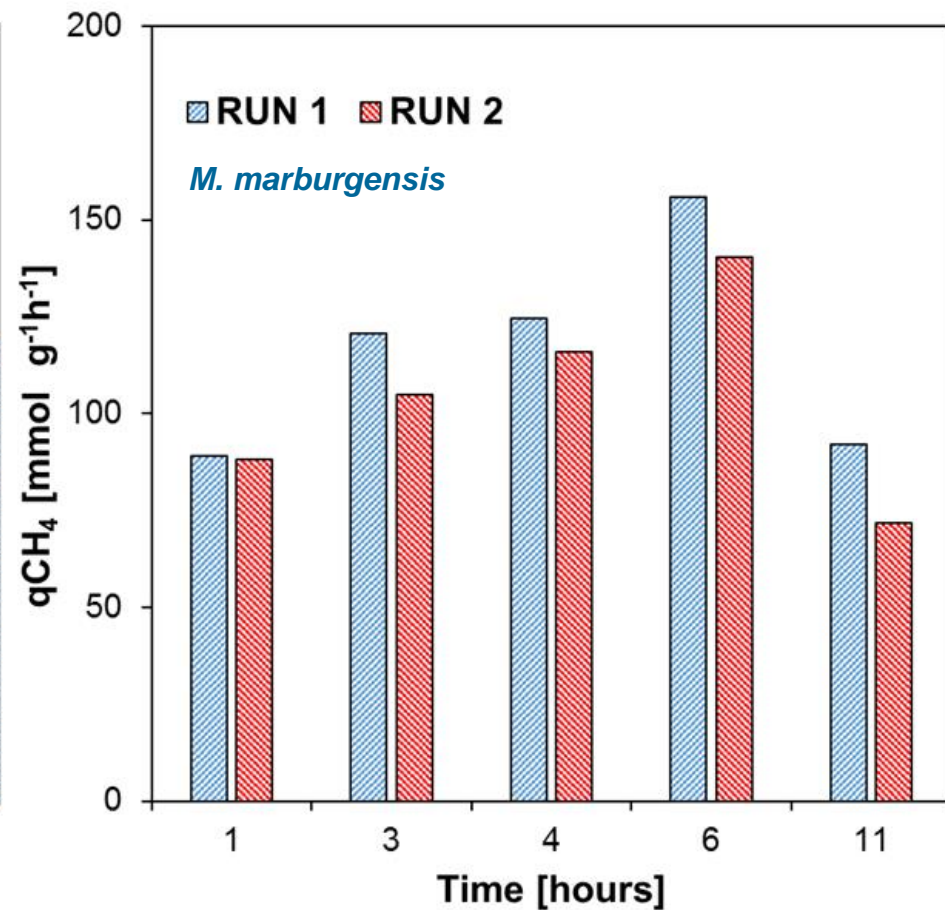
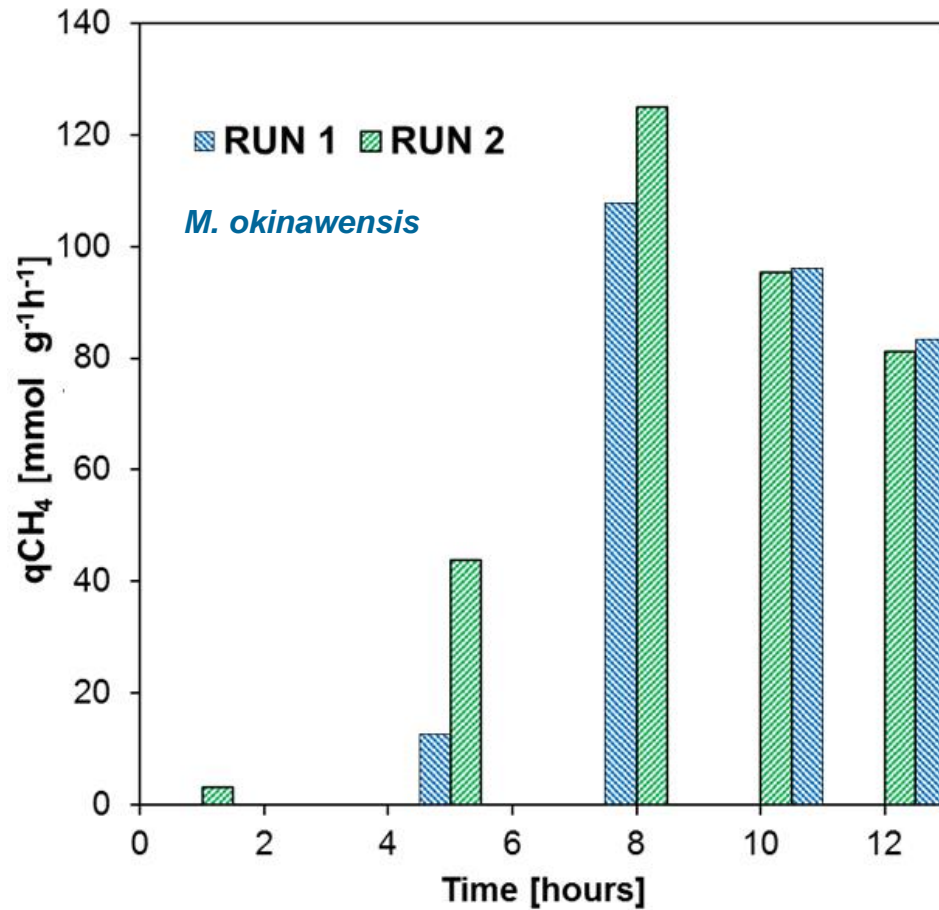
Growth (OD<sub>578nm</sub>) of *M. okinawensis* (left) and *M. marburgensis* (right) in fed-batch cultivation mode. Run 1 and run 2 are replicates.

# Fed-batch



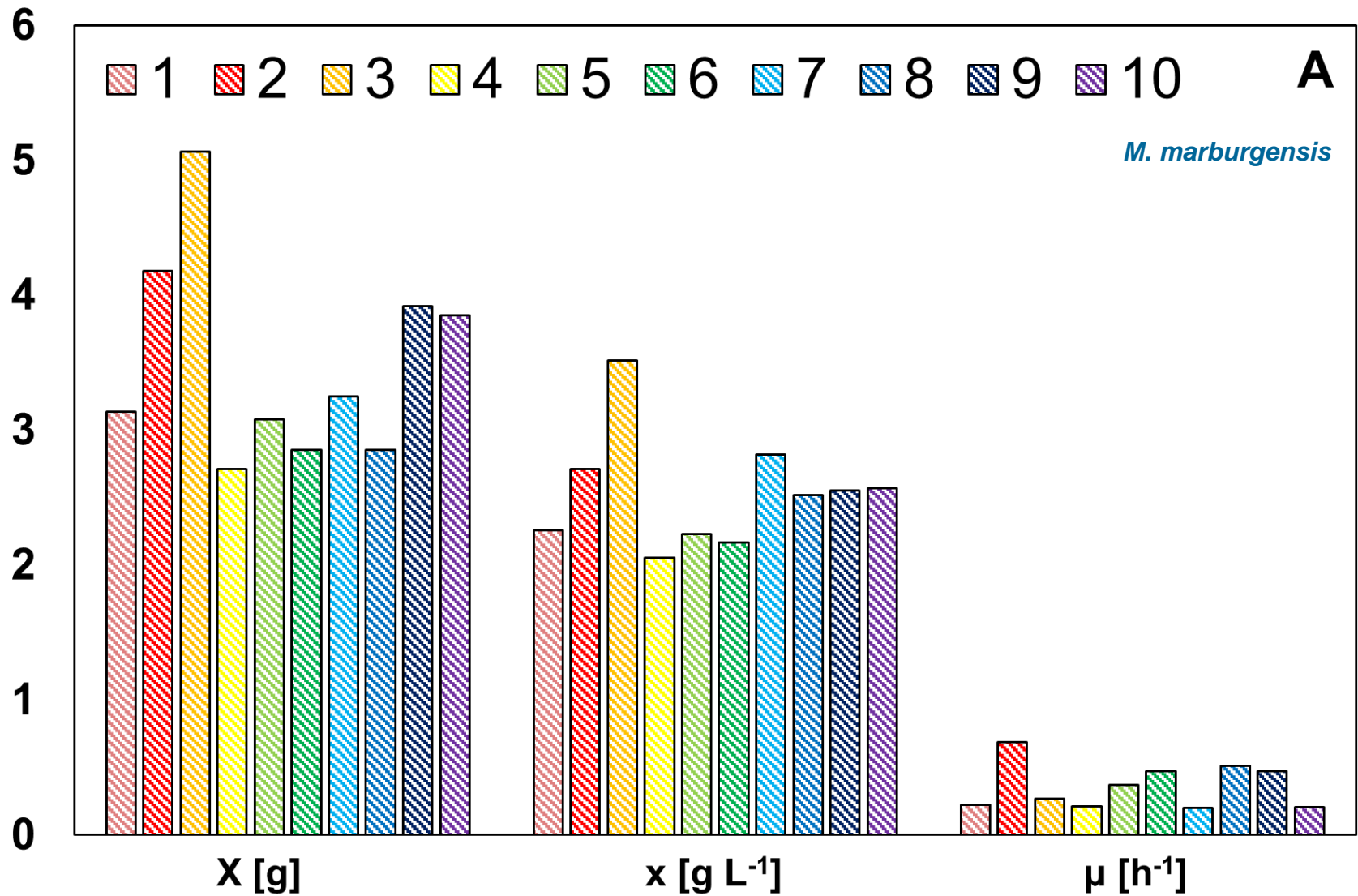
Methane evolution rate (MER) of *M. okinawensis* (left) and *M. marburgensis* (right) in fed-batch cultivation mode. Run 1 and run 2 are replicates.





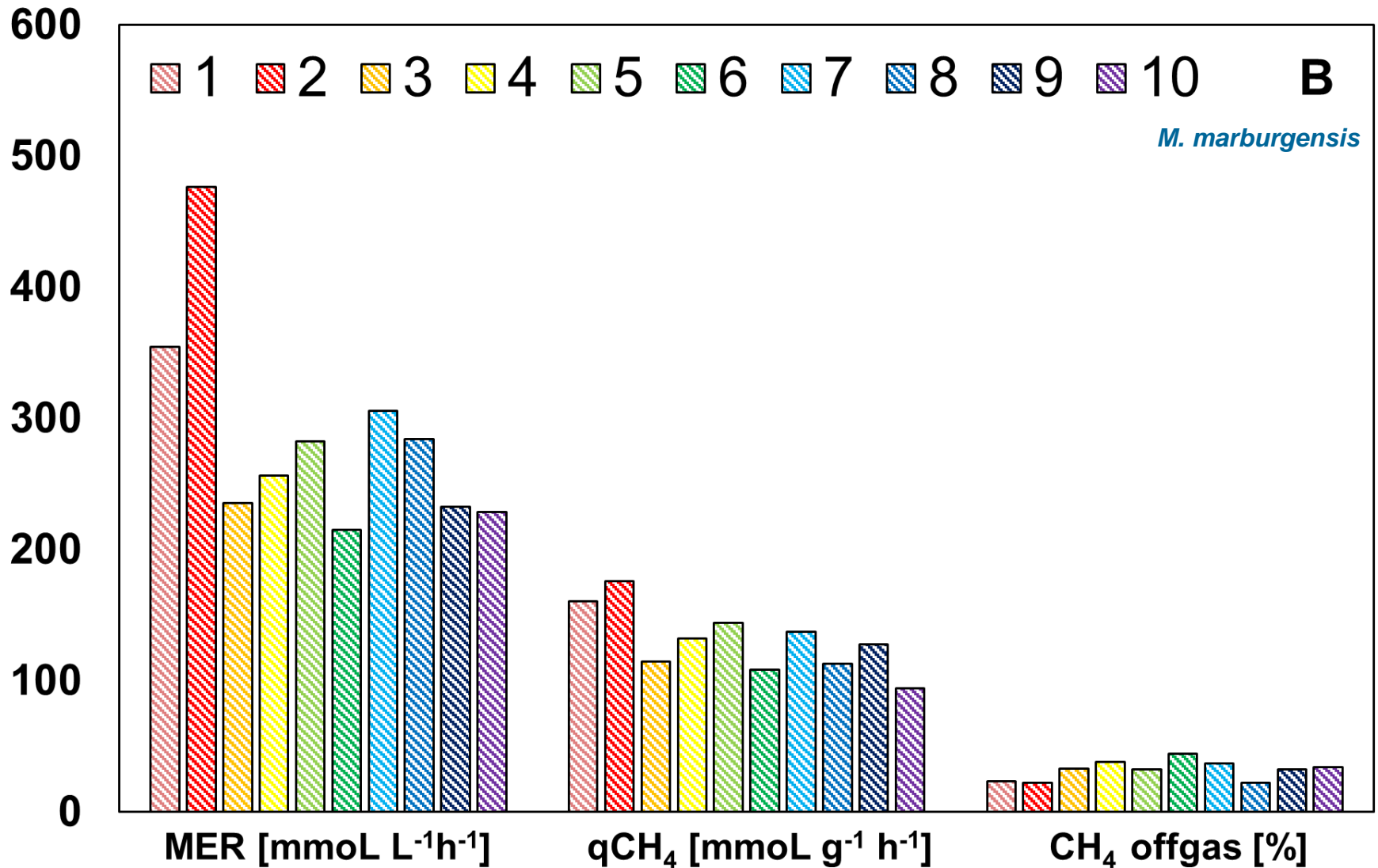
Specific methane evolution rate ( $q_{CH_4}$ ) of *M. okinawensis* (left) and *M. marburgensis* (right) in fed-batch cultivation mode. Run 1 and run 2 are replicates.

# Exponential fed-batch



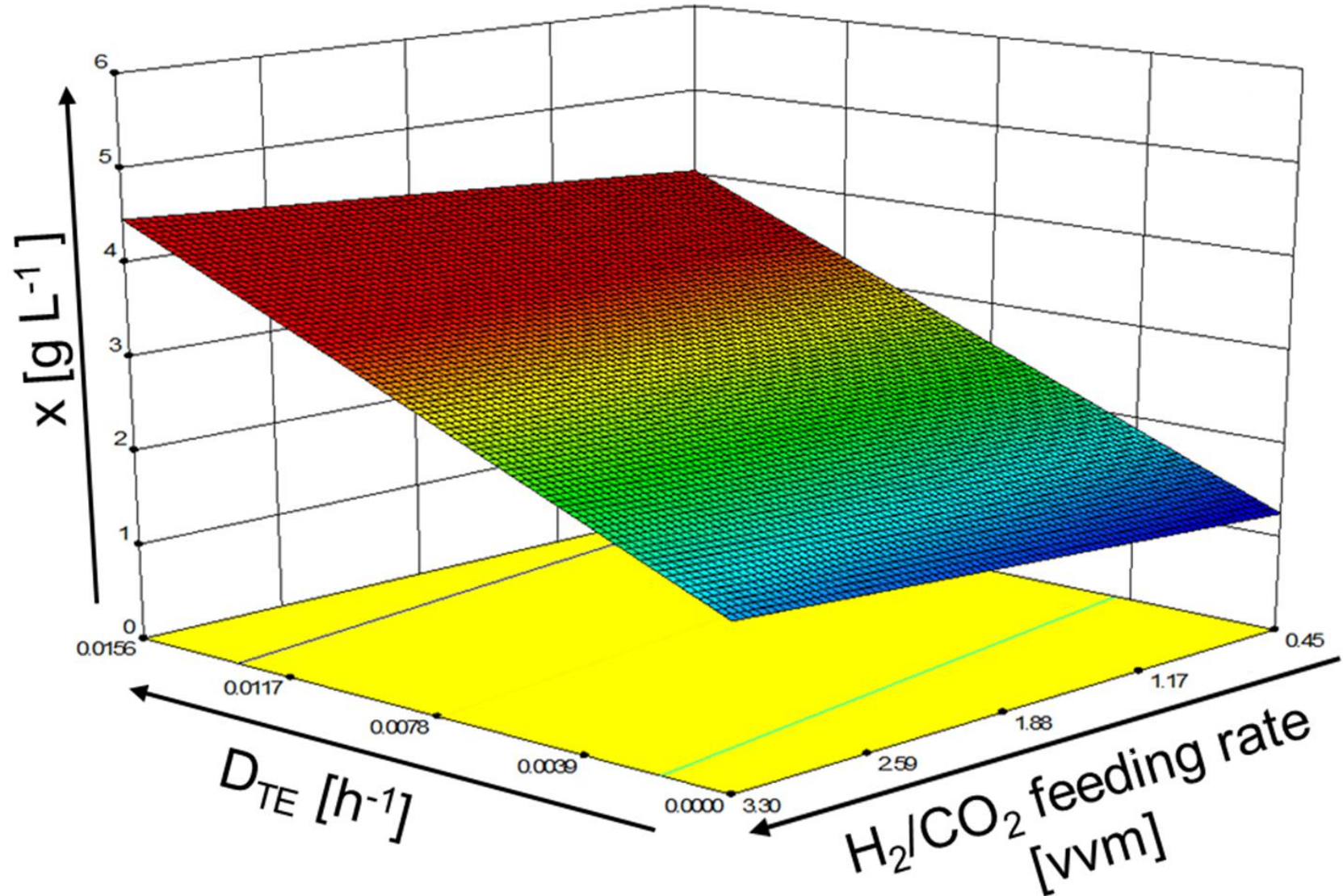
Results from the exponential fed-batch cultivation using *M. marburgensis*. For each run (colour legend) are presented the values of X, x, μ on the x-axis. Run 3 (orange bar) had the highest biomass (X [g]) and biomass concentration (x [g L<sup>-1</sup>]).

# Exponential fed-batch



Results from the exponential fed-batch cultivation using *M. marburgensis*. For each run the values MER, qCH<sub>4</sub>, CH<sub>4</sub> offgas are presented on the x-axis. Run 2 (red bar) showed the highest MER and qCH<sub>4</sub>. During run 6 the highest CH<sub>4</sub> off-gas concentration was obtained.

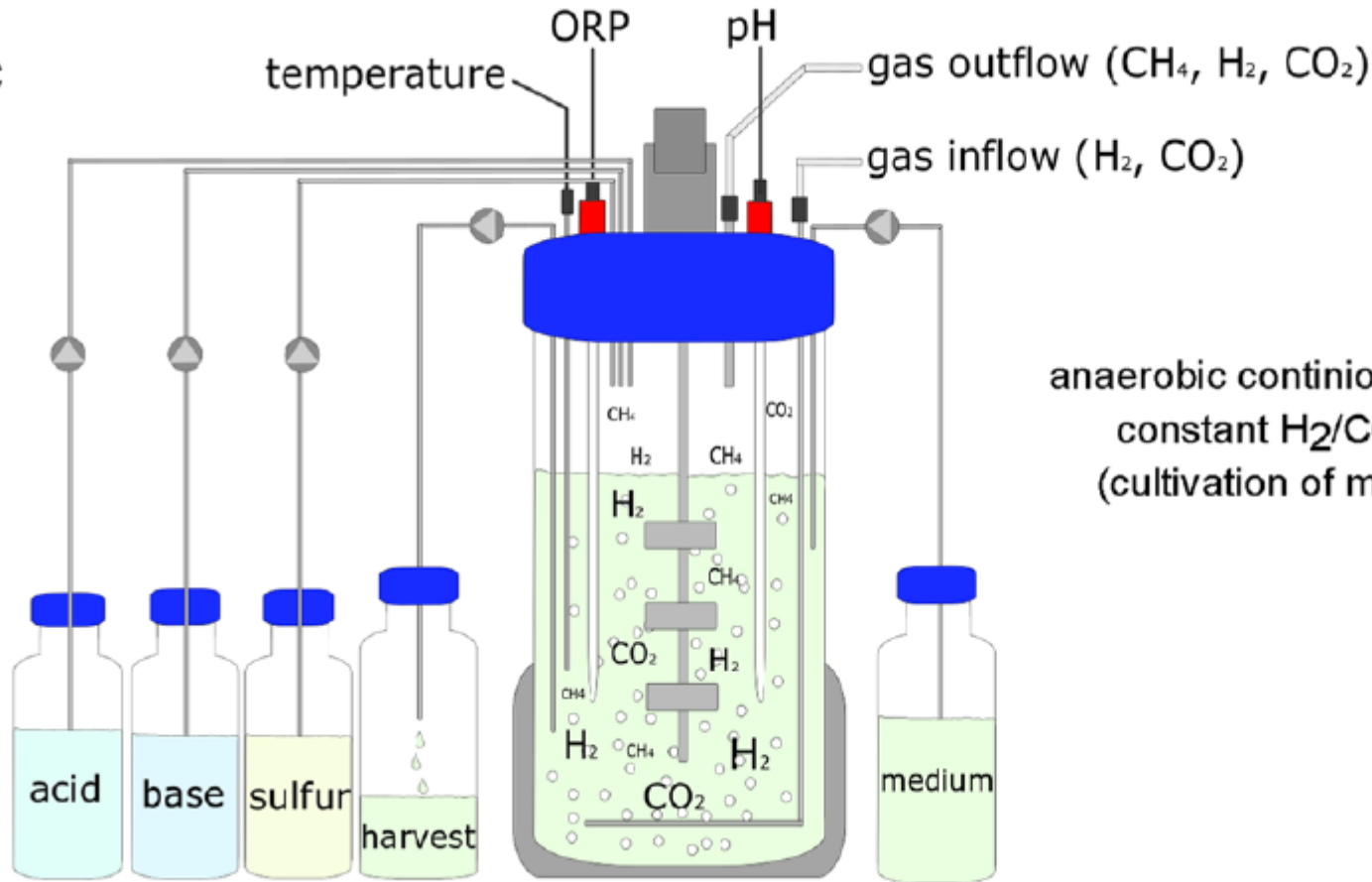
# Exponential fed-batch



Model for biomass concentration ( $x$ ) calculated from the exponential fed-batch data of *M. marburgensis*.

# Continuous culture

**C**



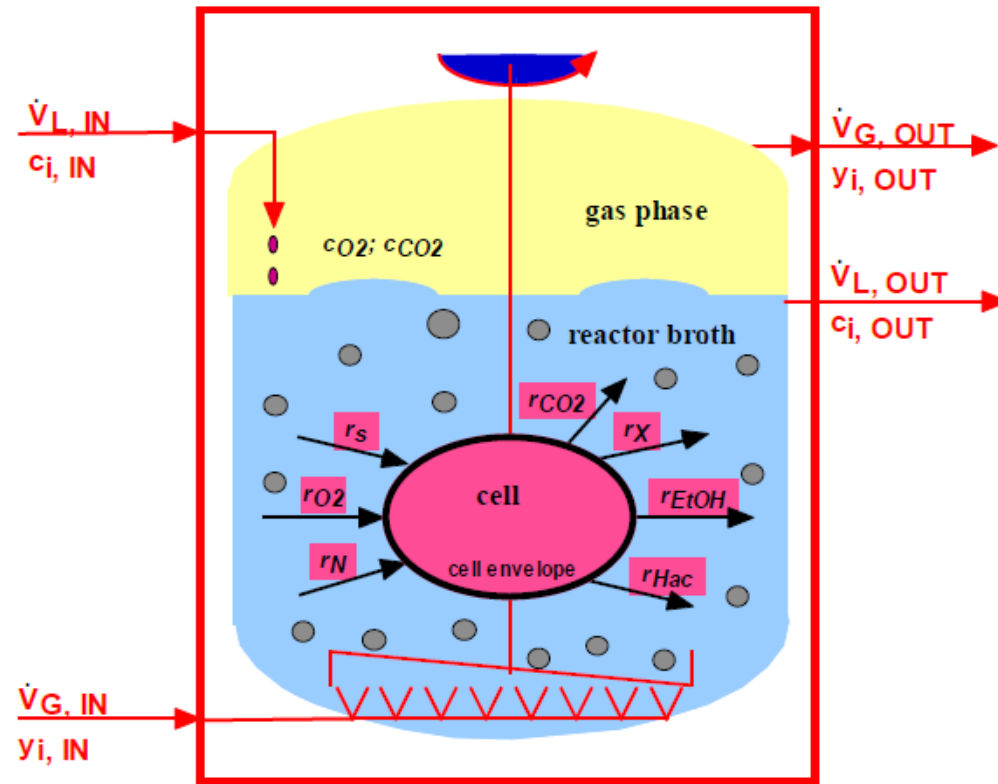
anaerobic continuous bioreactor set-up with  
constant H<sub>2</sub>/CO<sub>2</sub> and medium feed  
(cultivation of methanogenic archaea)

## Mass balance for continuous culture

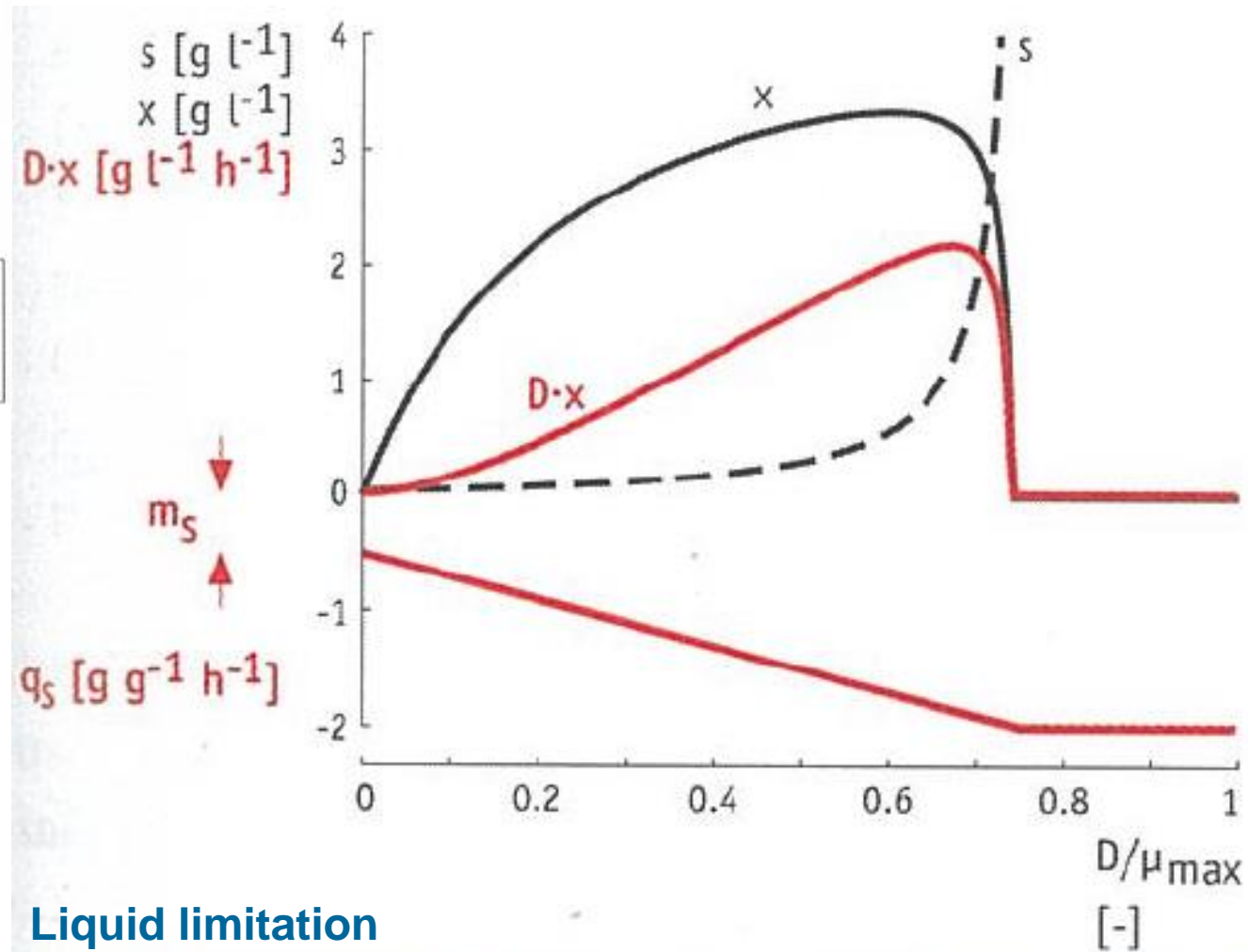
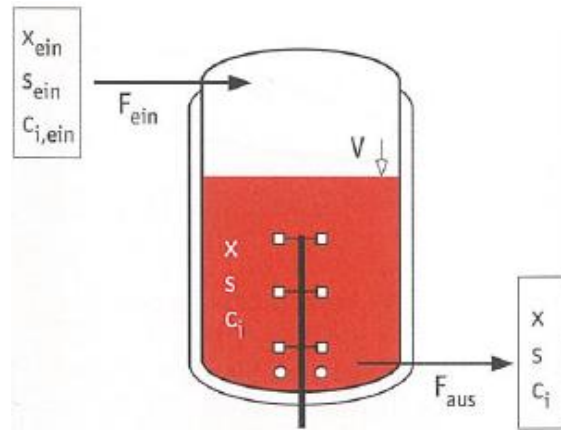
$$D = \mu = \frac{\dot{V}}{V_R} = \left[ \frac{1}{h} \right]$$

$$\dot{V}_{In} c_{i,In} - \dot{V}_{Out} c_{i,out} + V_R r_i = 0$$

$$r_i = -D(c_{i,In} - c_{i,out})$$



# Continuous culture



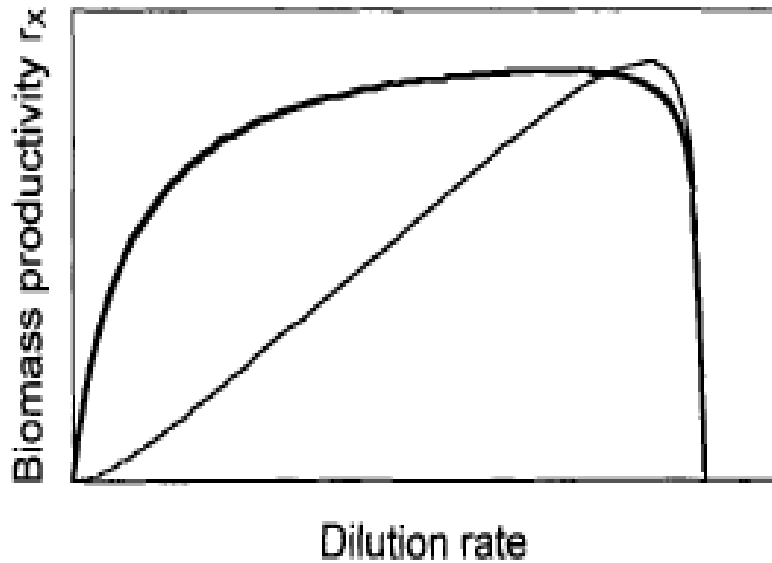
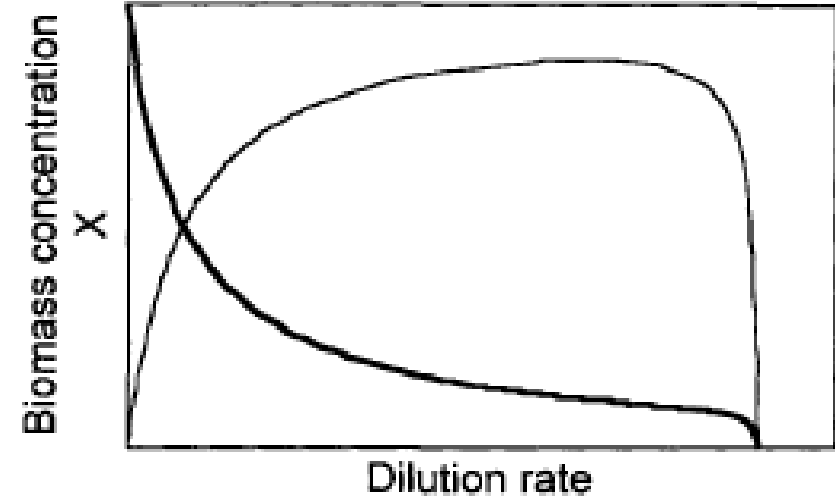
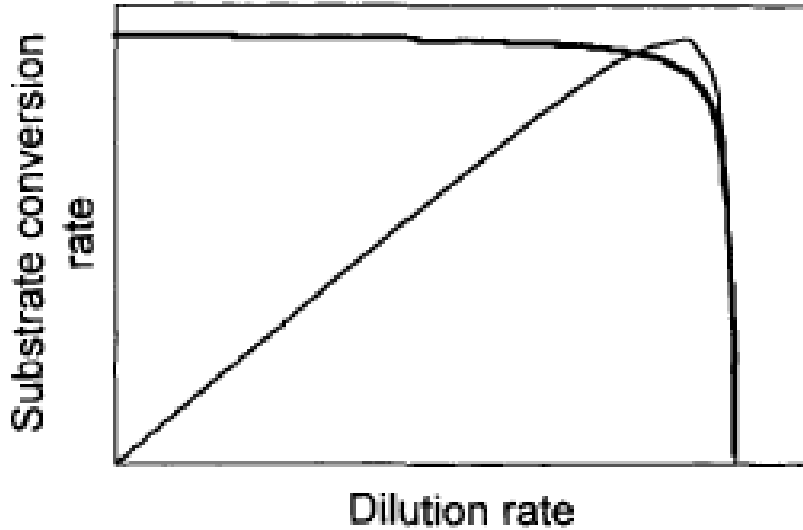
Liquid limitation

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Verlag, 2006

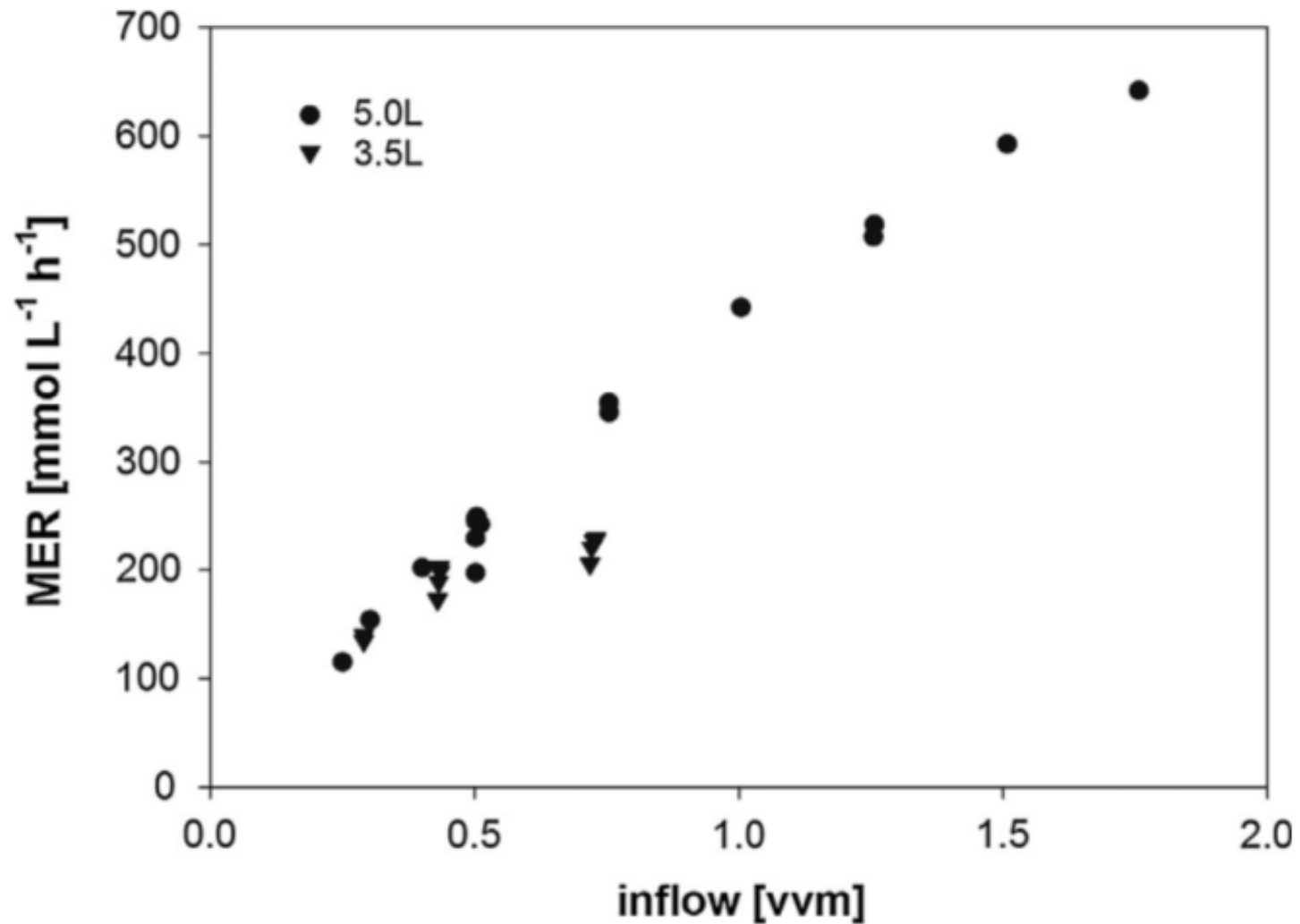
# Continuous culture



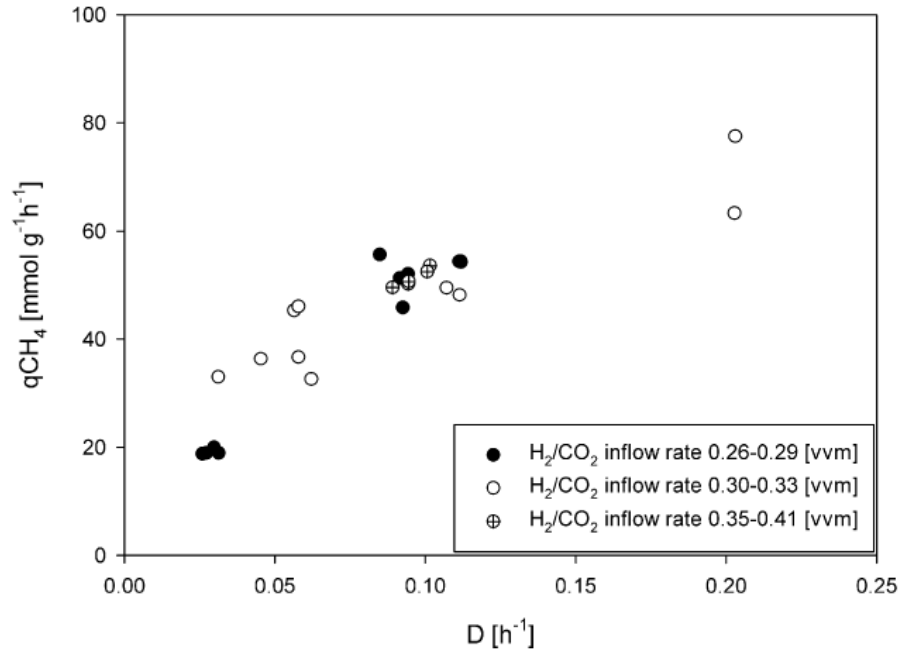
## Principles of continuous culture bioprocessing

- Liquid limitation: thin line
- Gas limitation: bold line

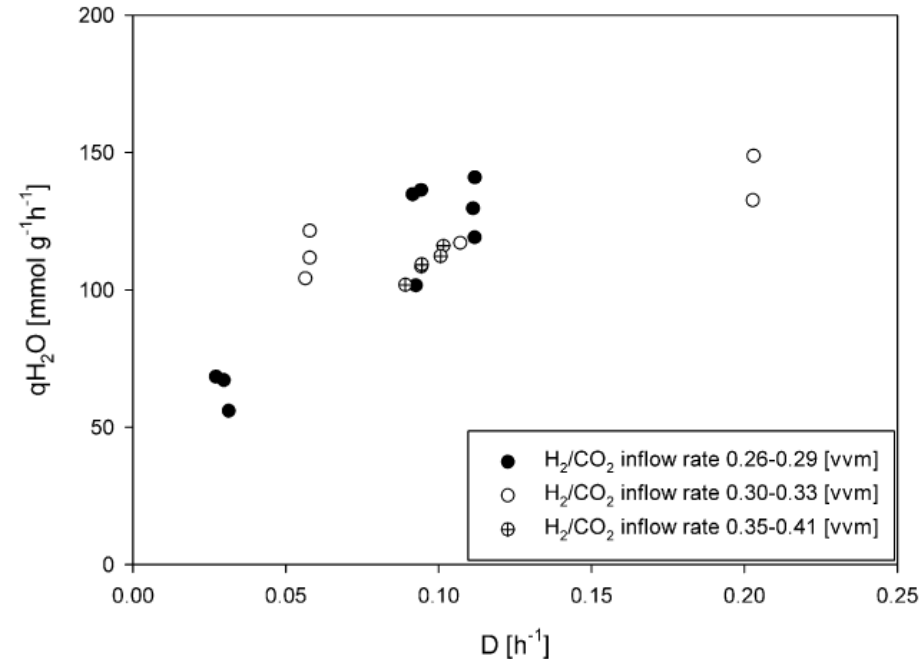




**Fig. 6.** Increase of MER with increased gasflow at 3.5 L and 5 L culture volume.

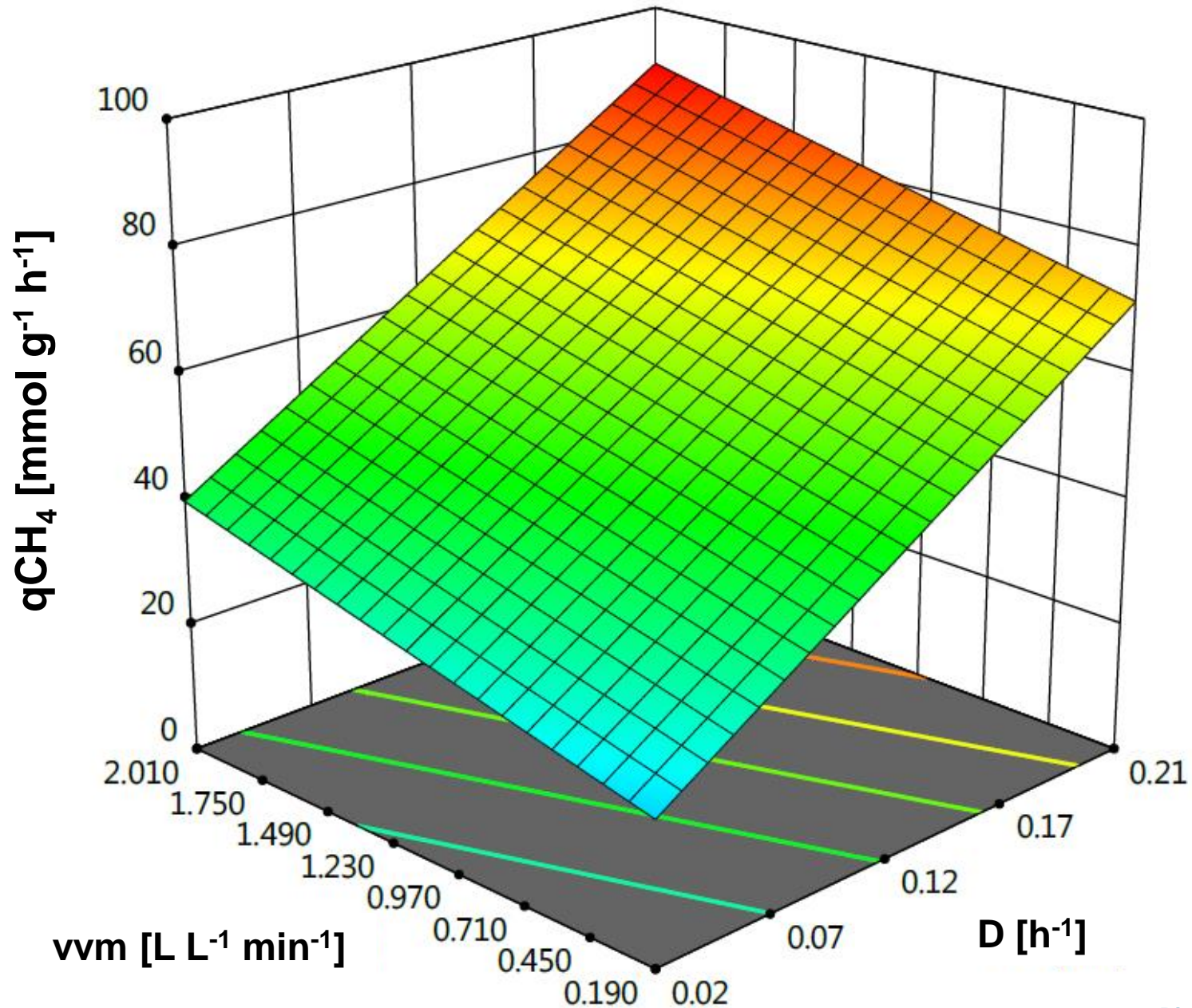


**Fig. 2 – Specific methane productivity is shown as a function of the liquid dilution rate. By increasing the liquid dilution rate the specific methane productivity increased. An elevated  $H_2/CO_2$  gassing rate ambiguously influenced  $q_{CH_4}$ .**

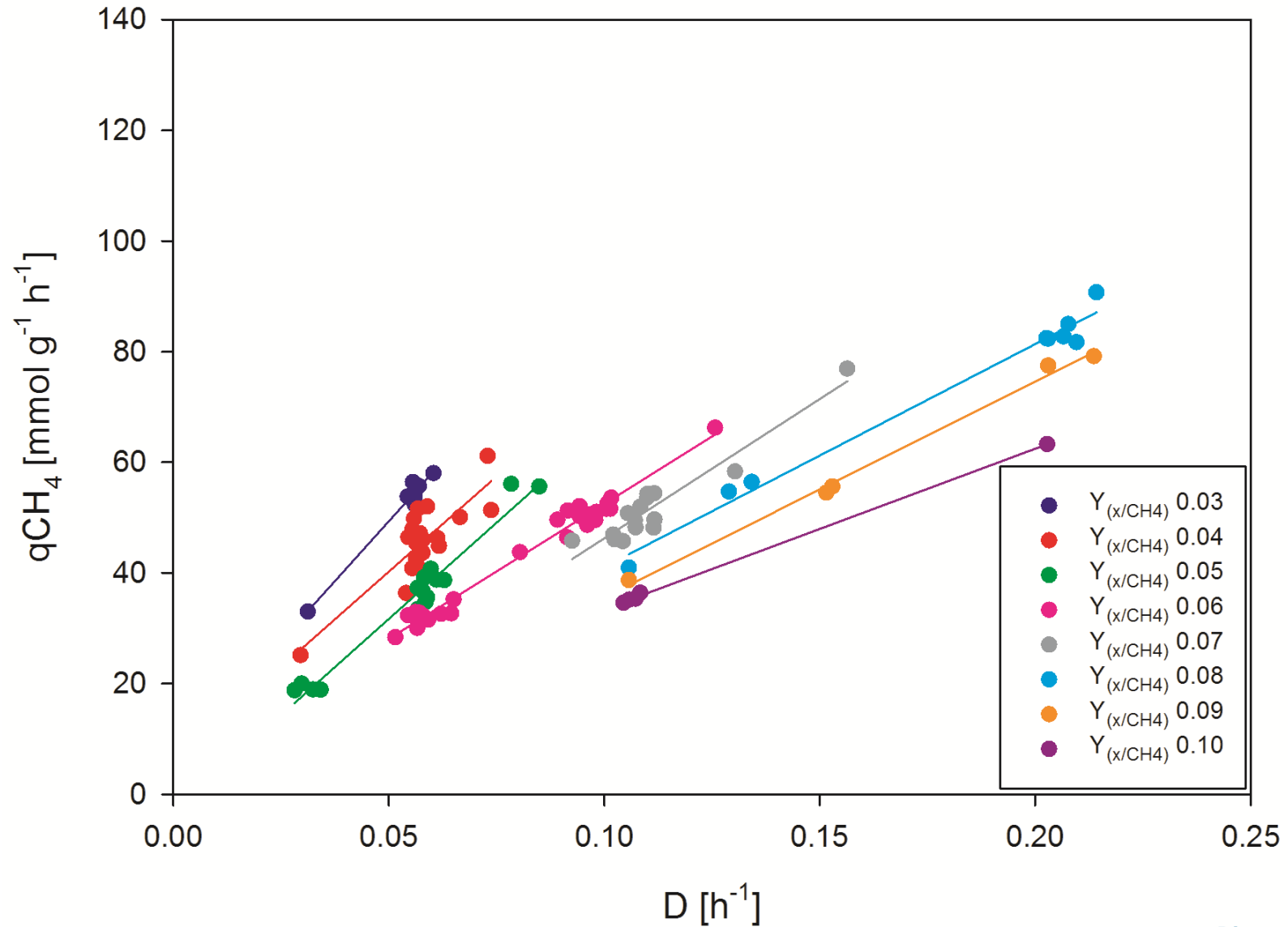


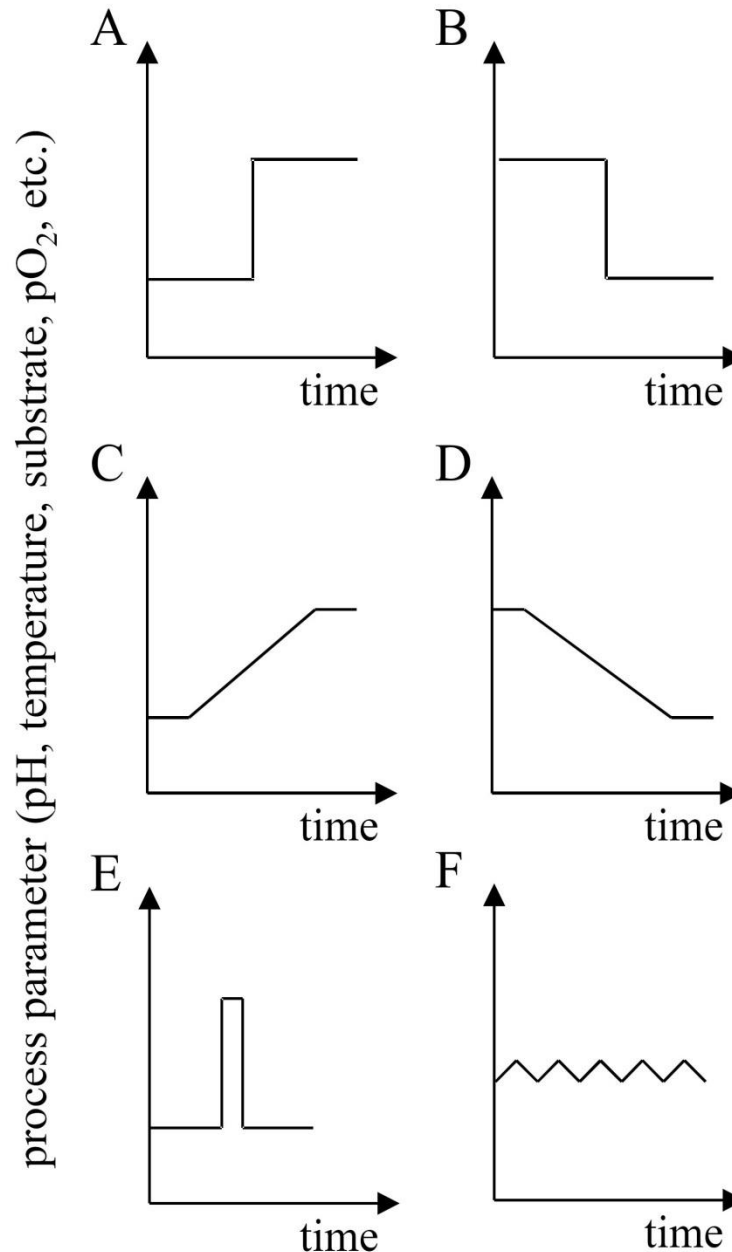
**Fig. 5 – Specific water production of *M. marburgensis* is illustrated as a function of the liquid dilution rate. By increasing the liquid dilution rate the specific water production increased. An elucidation of different  $H_2/CO_2$  gassing rates ambiguously influenced specific water productivity.**

# Continuous culture



# Continuous culture





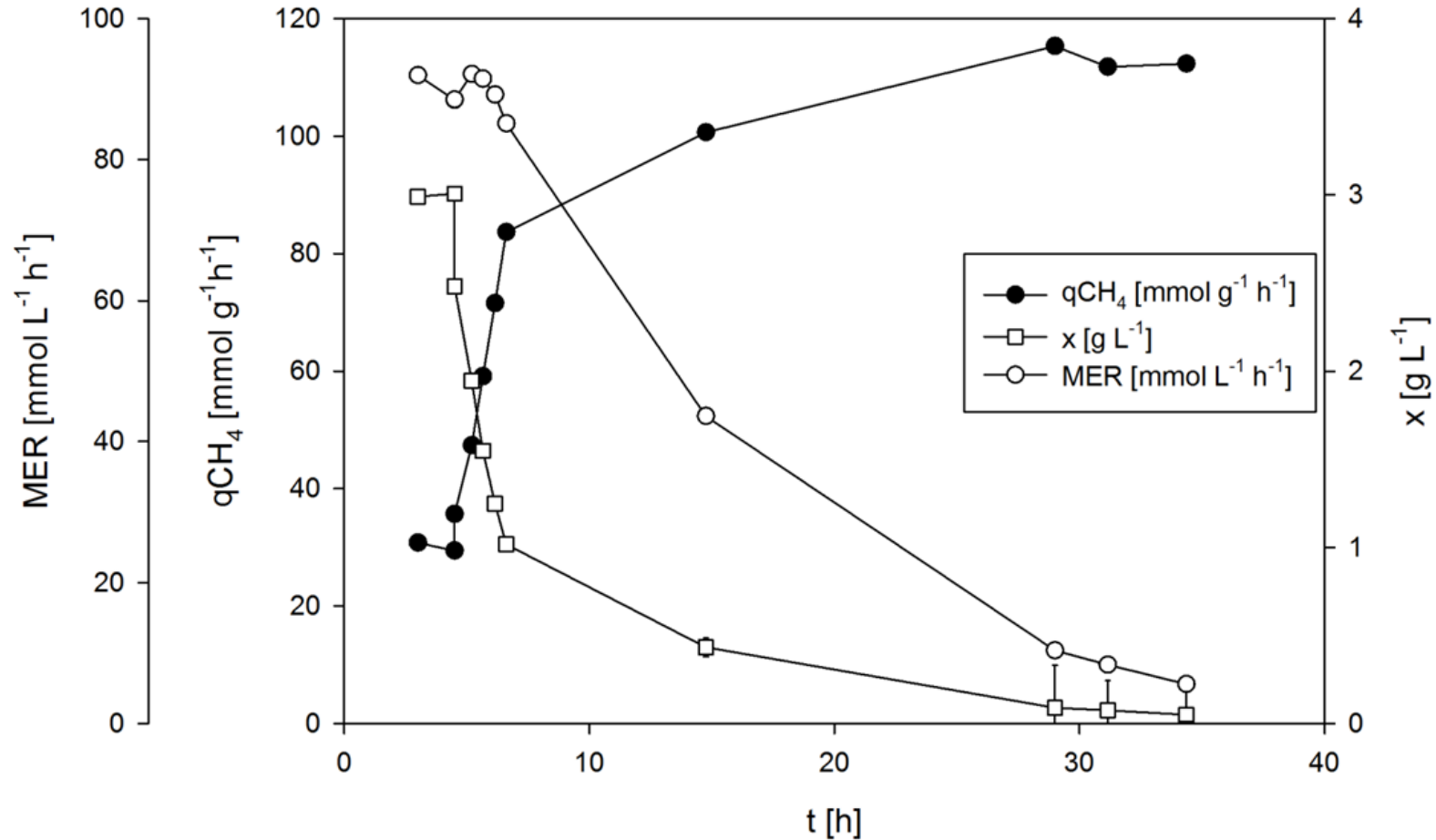
- A: shift-up
- B: shift-down
- C: ramp-up
- D: ramp-down
- E: pulse
- F: oscillation

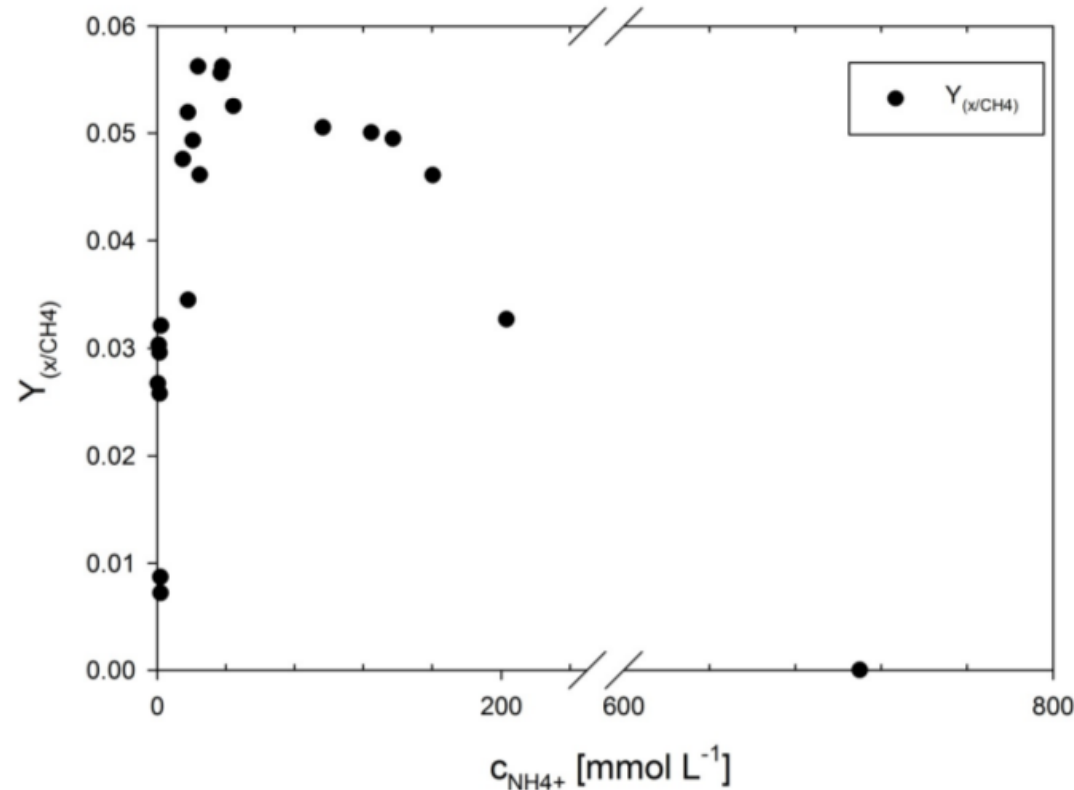
**Figure 1.** An overview of dynamic process conditions which can be used in bioprocess development.

# Dynamic process conditions

Dynamic condition	Modus operandi	Changed condition	Identification/Optimisation of	
<b>Shift</b>	rapid change of parameter(s) followed by stable condition(s)	physical parameters (D, T, rpm, vvm, light intensity, feed profile)	maximum physiological capacity ( $\mu_{\max}$ , $q_{s,\max}$ ) productivity ( $q_{p,\max}$ ) maintenance energy stress response metabolism morphology changes limitations	
	continuous and slow change of parameter(s)		productivity yields growth and production kinetic morphology viability limitations physiological capacity	
	sudden change of parameter(s)		chemical parameters (pH, nutrient concentrations, osmolality)  physiological parameters ( $\mu$ , $q_i$ )	productivity uptake rates yields growth kinetics short time cellular response product and metabolite release unscramble physiological and metabolic changes strain characteristic parameters ( $q_s$ , $q_p$ )
	controlled short up and down ramp(s) in a defined or changing frequency and/or amplitude		productivity growth kinetics metabolic and physiological optimisation heat and stress response quality improvement metabolite formation	

Identification of the maximum specific CH<sub>4</sub> evolution rate ( $q_{CH_4,max}$ ).





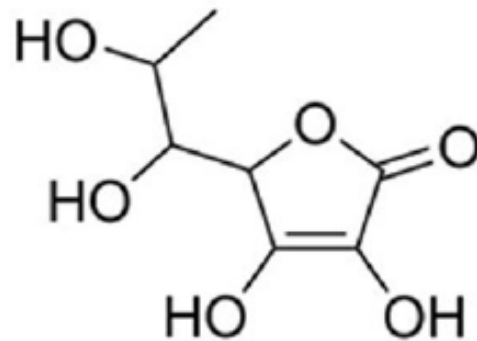
**Figure 5.** Analysis of  $Y_{(x/CH_4)}$  as function of the  $C_{NH_4^+}$  from dynamic experiments and chemostat cultures at fixed DM. The results indicate that a window of operation for a high  $Y_{(x/CH_4)}$  can be achieved if the  $C_{NH_4^+}$  is set to values between 30 and 60  $mmol L^{-1}$ .  $C_{NH_4^+}$  lower than 30  $mmol L^{-1}$  and higher than 60  $mmol L^{-1}$  clearly reduces  $Y_{(x/CH_4)}$ .



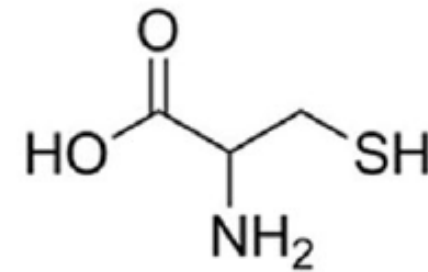
Reducing agent	Concentration in media	ORP (mV)	Reference
Na <sub>2</sub> S·9H <sub>2</sub> O	0.025–0.05%	– 571	(Bast 2001a; Breznak and Costilow 2007)
Cysteine-HCl	0.025–0.05%	– 340	(Bast 2001a; Breznak and Costilow 2007)
Dithiothreitol	0.01–0.05%	– 330	(Cleland 2002; Breznak and Costilow 2007)
FeS (amorphous hydrated)	4 µg mL <sup>-1</sup>	– 270	(Brock and Od’ea 1977)
Sodium thioglycolate	0.05–0.1%	– 140	(Bast 2001a; Breznak and Costilow 2007)
Ascorbic acid	0.05–0.1%	+ 58	(Bast 2001a; Breznak and Costilow 2007)
H <sub>2</sub> (PdCl <sub>2</sub> )	Variable	– 413	(Breznak and Costilow 2007)
Titanium(III)citrate	1–4 mM	– 480	(Zehnder and Wuhrmann 1976; Jones and Pickard 1980)

**Table 1** Commonly used reducing agents in anaerobic microbiology

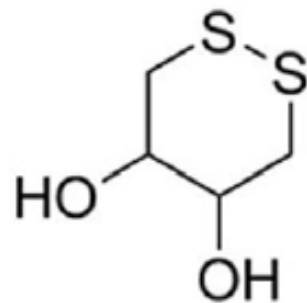
**Ascorbic acid**



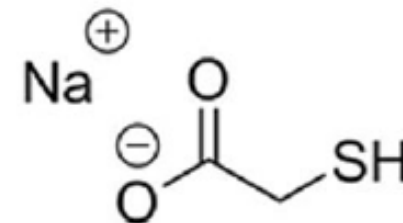
**Cystein-HCl**



**Dithiothreitol**



**Sodiumthioglycolate**



**Fig. 2** Chemical structures of selected reducing agents

# Anaerobic cultivation techniques



**Table 2** Redox dyes and their corresponding standard ORP values at 30 °C and pH 7.0

Redox dye	Colour			ORP [mV]	Reference	
	reduced	oxidized	oxidized/ reduced			
Methylene blue	 transparent	 blue		+11	(Bast 2001a; Breznak and Costilow 2007)	
Toluidine blue	 blue	 pink		-11	(Breznak and Costilow 2007)	
Resorufin	 violet	 pink	 transparent	-51	(Bast 2001a; Tratnyek et al. 2001; Breznak and Costilow 2007)	
Indigo disulfonate/ Indigo carmine	 yellow	 orange	 green	 blue	-125	(Tratnyek et al. 2001; Breznak and Costilow 2007)
Phenosafranine	 transparent	 red		-252	(Bast 2001a; Tratnyek et al. 2001; Breznak and Costilow 2007)	
Titanium(III)citrate	 violet	 transparent		-480	(Zehnder and Wuhrmann 1976; Bast 2001; Collins et al. 2005)	

# Anaerobic cultivation techniques



resazurin



methylene blue



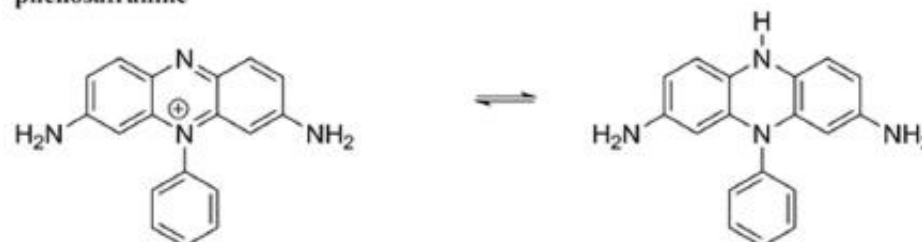
toluidine blue



indigo disulfonate

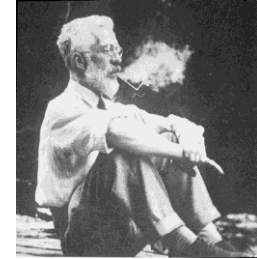


phenosafranine



**Fig. 3** Oxidized (left) and reduced (right) form of the redox dyes. The structure of titanium(III)citrate is not shown due to different forms of the oxidized form depending on the predominant pH in the medium (Collins et al. 2005)

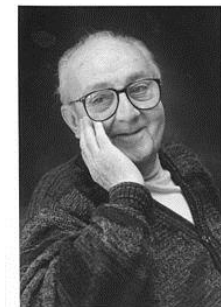
- **DoE was founded by Ronald Fisher (UK), who basically developed factorial experiments as well as **AN**alysis **Of** **V**ariance**



Ronald Fisher

- **George Box developed basis for optimisation of DoE designs (Response Surface Modeling (RSM))**

- „To find out what happens if you change something, is necessary to change it.“
- „Essentially all models are wrong, but some are useful“



George Box

- **Within the DoE concept Gen'ichi Taguchi (Japan) developed a qualitative approach (Taguchi-Methodology)**



Gen'ichi Taguchi

## Why do we need DoE?

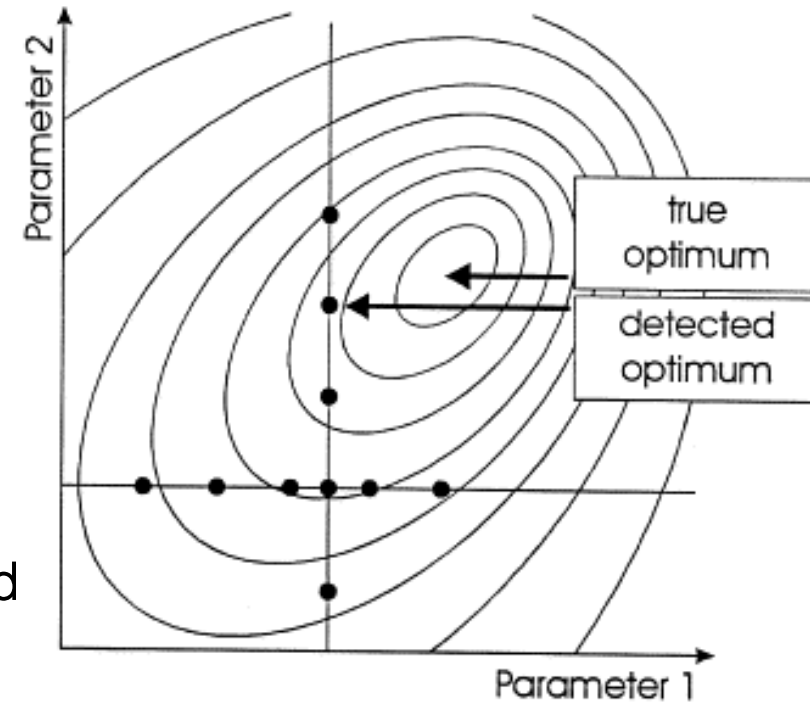
- **Which (process/cultivation/environmental) parameters have which influence on which variables (response of an organism)?**
- **How can we determine with a minimum of experiments which parameters and interactions of parameters are beneficial/detrimental for the cultivation of an organism in an experimental design space?**

## Why do we need DoE?

- Classical way to perform an experiment is to vary one parameter (factor) at a time
  - OVAT (one-variable-at-a-time)

## Drawbacks

- Time consuming
- Interactions
- Maybe the optimum will not be identified

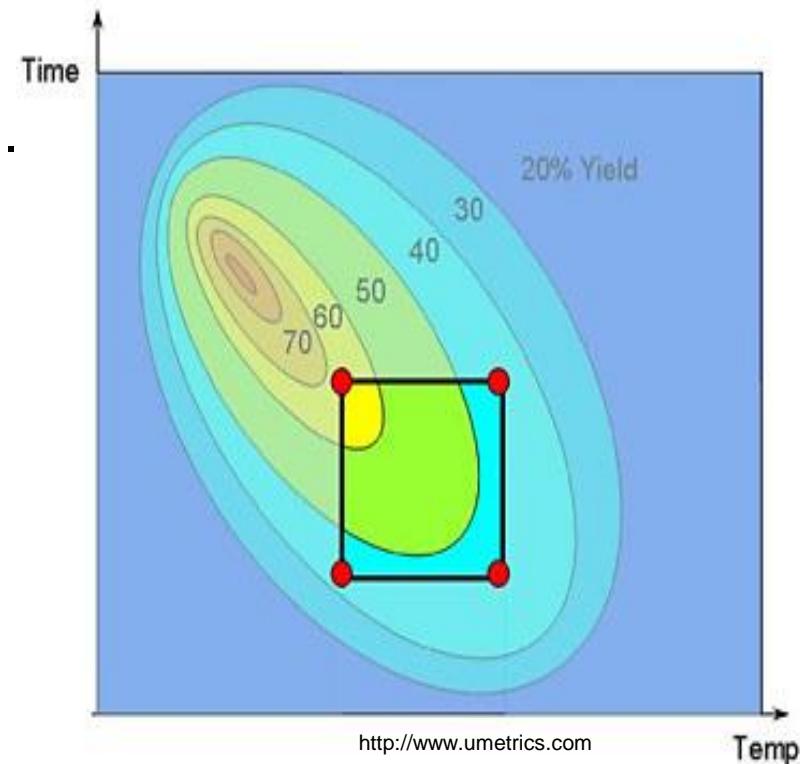


## Why do we need DoE?

- Determine parameters (independent variables), which influence responses (dependent variables).
- Optimise cultivation (process)
- Improve growth, product quality, quantity..

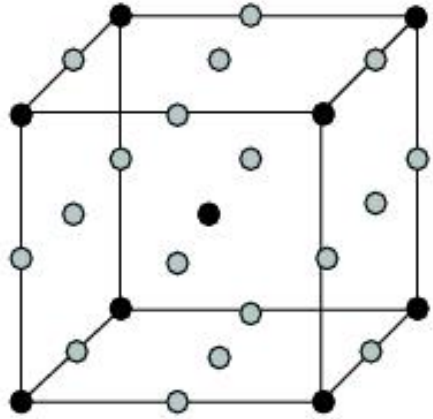
## DoE requires

- Planning of randomised experiments
- Dicipline
- Application of statistics

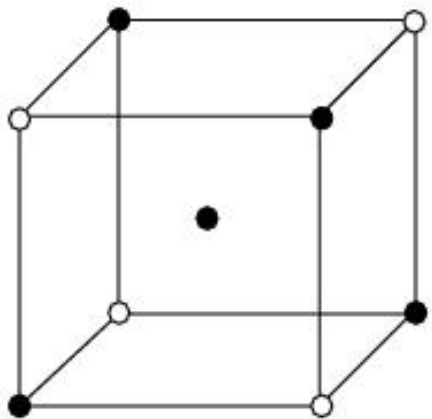




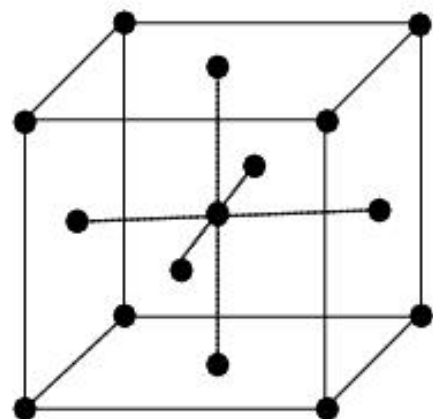
# DoE designs



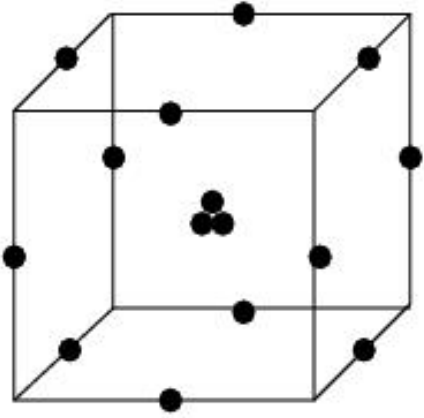
Full factorial



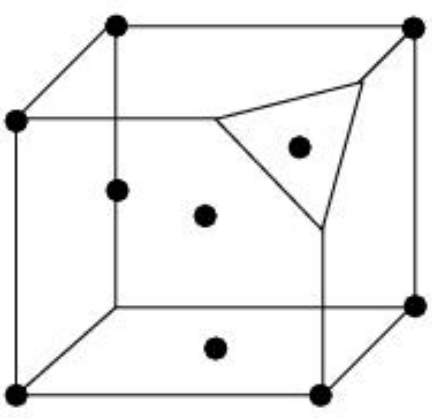
Fractional factorial



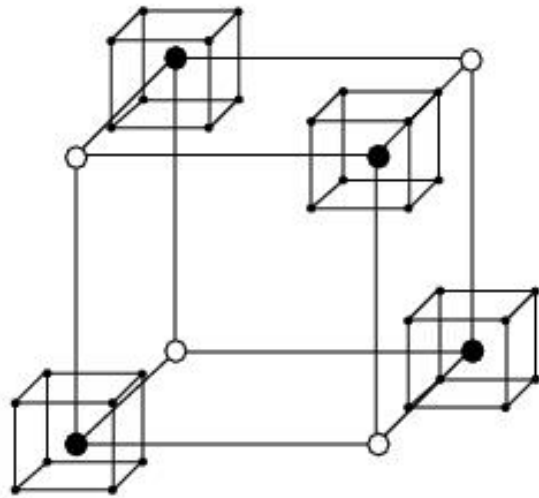
Central composite  
(face centered)



Box Behnken



D-optimal design



Taguchi design

## 1.) Screening

- Full or fractional factorial designs
  - Resolution V designs are best to be used, but also
  - Resolution IV designs are possible

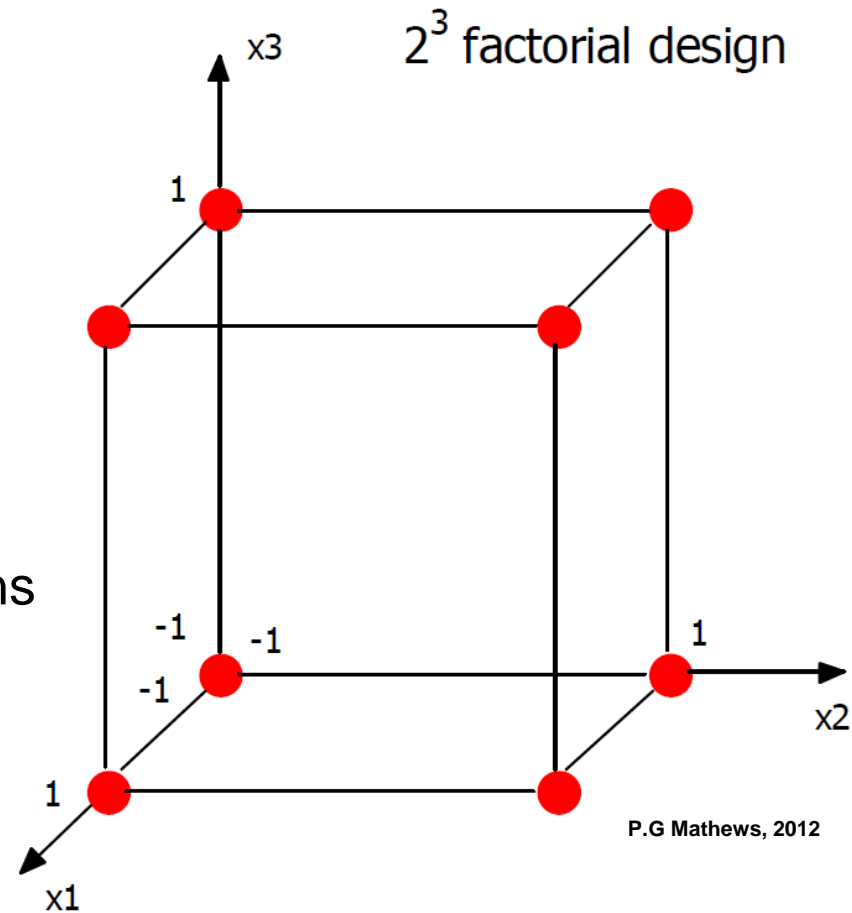
## 2.) Optimization or modelling

- Response Surface Model (RSM)
  - Central composite, Box-Behnken or Taguchi-design

## 3.) Verification

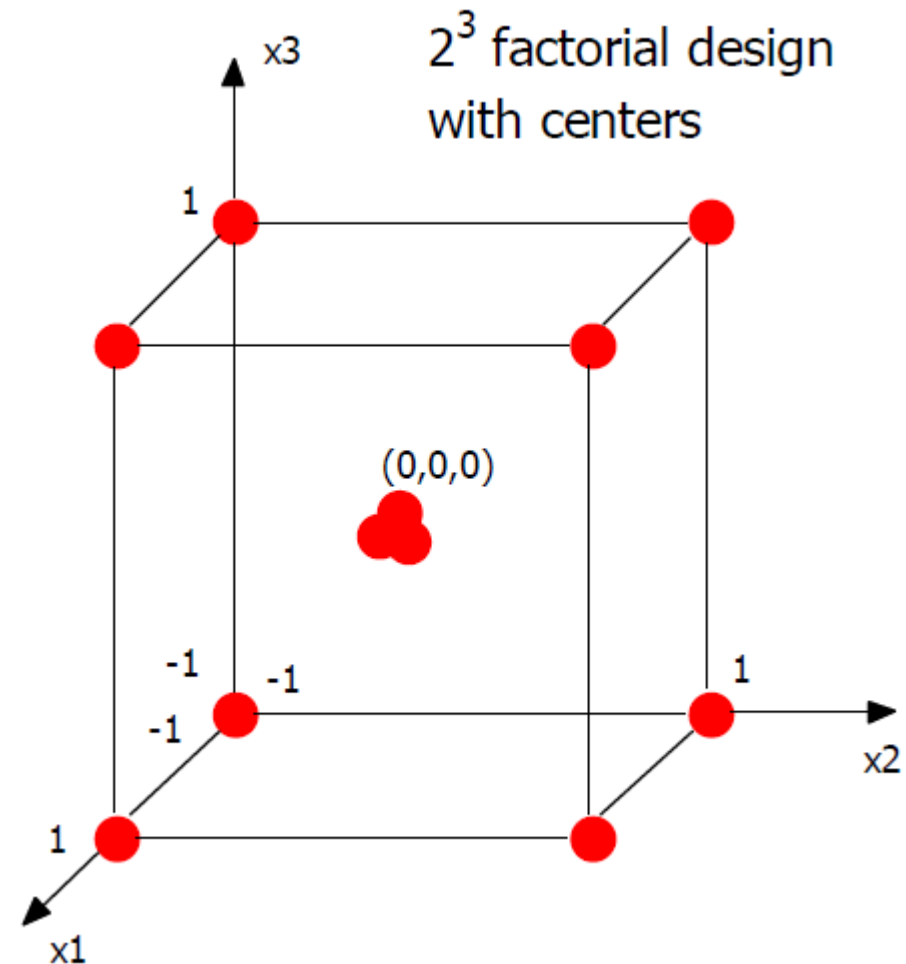
## Screening

- Good for first experiment(s)
- Can consider lots of variables
- Usually only two levels of each variable
- Relatively few runs
- Limited if any ability to identify interactions
- (depending on the design)
- Risky?



## Screening

- Useful for estimating main effects and interactions
- Fractional factorial design can be used for screening many factors to find the significant few



# DoE – Screening designs

		Number of Factors																				
		2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	
Runs	4	$2^2$	$2^{3-1}_{III}$																			
	8		$2^3$	$2^{4-1}_{IV}$	$2^{5-2}_{III}$	$2^{6-3}_{III}$	$2^{7-4}_{III}$															
	16			$2^4$	$2^{5-1}_{V}$	$2^{6-2}_{IV}$	$2^{7-3}_{IV}$	$2^{8-4}_{IV}$	$2^{9-5}_{III}$	$2^{10-6}_{III}$	$2^{11-7}_{III}$	$2^{12-8}_{III}$	$2^{13-9}_{III}$	$2^{14-10}_{III}$	$2^{15-11}_{III}$							
	32				$2^5$	$2^{6-1}_{VI}$	$2^{7-2}_{IV}$	$2^{8-3}_{IV}$	$2^{9-4}_{IV}$	$2^{10-5}_{IV}$	$2^{11-6}_{IV}$	$2^{12-7}_{IV}$	$2^{13-8}_{IV}$	$2^{14-9}_{IV}$	$2^{15-10}_{IV}$	$2^{16-11}_{IV}$	$2^{17-12}_{III}$	$2^{18-13}_{III}$	$2^{19-14}_{III}$	$2^{20-15}_{III}$	$2^{21-16}_{III}$	
	64					$2^6$	$2^{7-1}_{VII}$	$2^{8-2}_{V}$	$2^{9-3}_{IV}$	$2^{10-4}_{IV}$	$2^{11-5}_{IV}$	$2^{12-6}_{IV}$	$2^{13-7}_{IV}$	$2^{14-8}_{IV}$	$2^{15-9}_{IV}$	$2^{16-10}_{IV}$	$2^{17-11}_{IV}$	$2^{18-12}_{IV}$	$2^{19-13}_{IV}$	$2^{20-14}_{IV}$	$2^{21-15}_{IV}$	
	128						$2^7$	$2^{8-1}_{VIII}$	$2^{9-2}_{VI}$	$2^{10-3}_{V}$	$2^{11-4}_{V}$	$2^{12-5}_{IV}$	$2^{13-6}_{IV}$	$2^{14-7}_{IV}$	$2^{15-8}_{IV}$	$2^{16-9}_{IV}$	$2^{17-10}_{IV}$	$2^{18-11}_{IV}$	$2^{19-12}_{IV}$	$2^{20-13}_{IV}$	$2^{21-14}_{IV}$	
	256							$2^8$	$2^{9-1}_{IX}$	$2^{10-2}_{VI}$	$2^{11-3}_{VI}$	$2^{12-4}_{VI}$	$2^{13-5}_{V}$	$2^{14-6}_{V}$	$2^{15-7}_{V}$	$2^{16-8}_{V}$	$2^{17-9}_{V}$	$2^{18-10}_{IV}$	$2^{19-11}_{IV}$	$2^{20-12}_{IV}$	$2^{21-13}_{IV}$	
	512								$2^9$	$2^{10-1}_{X}$	$2^{11-2}_{VII}$	$2^{12-3}_{VI}$	$2^{13-4}_{VI}$	$2^{14-5}_{VI}$	$2^{15-6}_{VI}$	$2^{16-7}_{VI}$	$2^{17-8}_{VI}$	$2^{18-9}_{VI}$	$2^{19-10}_{V}$	$2^{20-11}_{V}$	$2^{21-12}_{V}$	

Color coding represents the design resolution:

green = resolution V design or higher, yellow = resolution IV design and red = resolution III design

Design Expert (Stat-Ease Inc., USA)

25-1

**Factorial Effects Aliases**  
[Est. Terms] Aliased Terms

[Intercept] = Intercept  
[A] = A  
[B] = B  
[C] = C  
[D] = D  
[E] = E  
[AB] = AB + CDE  
[AC] = AC + BDE  
[AD] = AD + BCE  
[AE] = AE + BCD  
[BC] = BC + ADE  
[BD] = BD + ACE  
[BE] = BE + ACD  
[CD] = CD + ABE  
[CE] = CE + ABD  
[DE] = DE + ABC

**Factor Generator**  
E = ABCD

**Factorial Effects Defining Contrast**  
I = ABCDE

**Resolution 5 design**

26-2

**Factorial Effects Aliases**  
[Est. Terms] Aliased Terms

[Intercept] = Intercept  
[A] = A + BCE + DEF  
[B] = B + ACE + CDF  
[C] = C + ABE + BDF  
[D] = D + AEF + BCF  
[E] = E + ABC + ADF  
[F] = F + ADE + BCD  
[AB] = AB + CE  
[AC] = AC + BE  
[AD] = AD + EF  
[AE] = AE + BC + DF  
[AF] = AF + DE  
[BD] = BD + CF  
[BF] = BF + CD  
[ABD] = ABD + ACF + BEF + CDE  
[ABF] = ABF + ACD + BDE + CEF

**Factor Generator**  
E = ABC  
F = BCD

**Factorial Effects Defining Contrast**  
I = ABCE = ADEF = BCDF

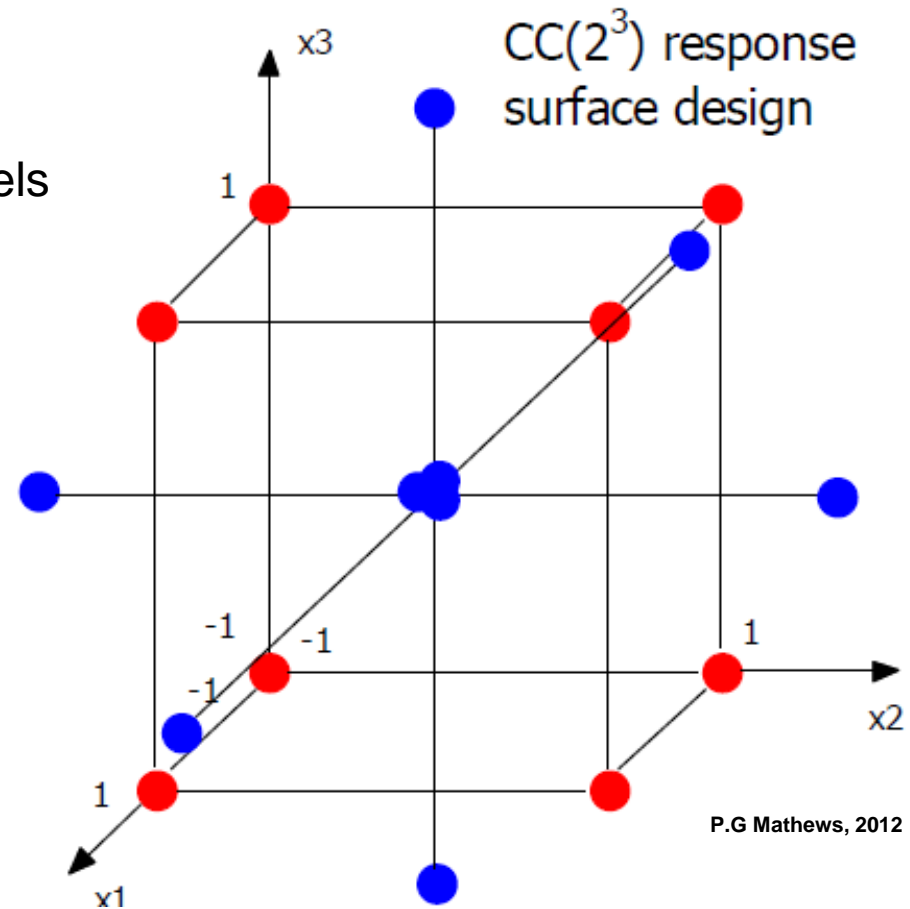
**Resolution 4 design**

## Optimization

- Good follow-up experiment to a screening experiment
- Fewer variables - generally the most important ones
- Often three or more levels of each variable
- Provide a more complex model for the process

## Central composite

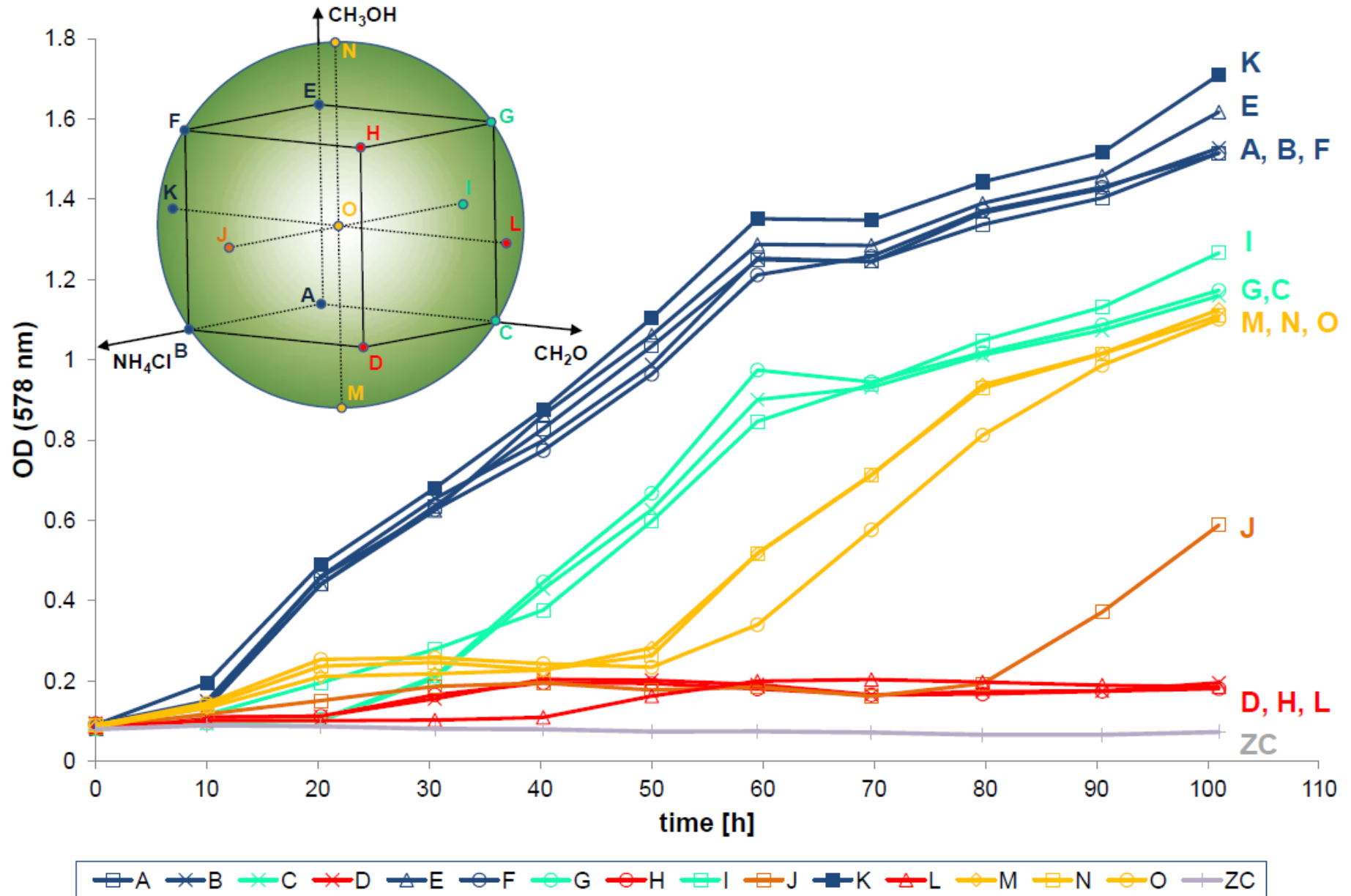
- Each numeric factor is varied over 5 levels
- plus and minus  $\alpha$  (axial points)
- plus and minus 1 (factorial points)
- usually three to six center points



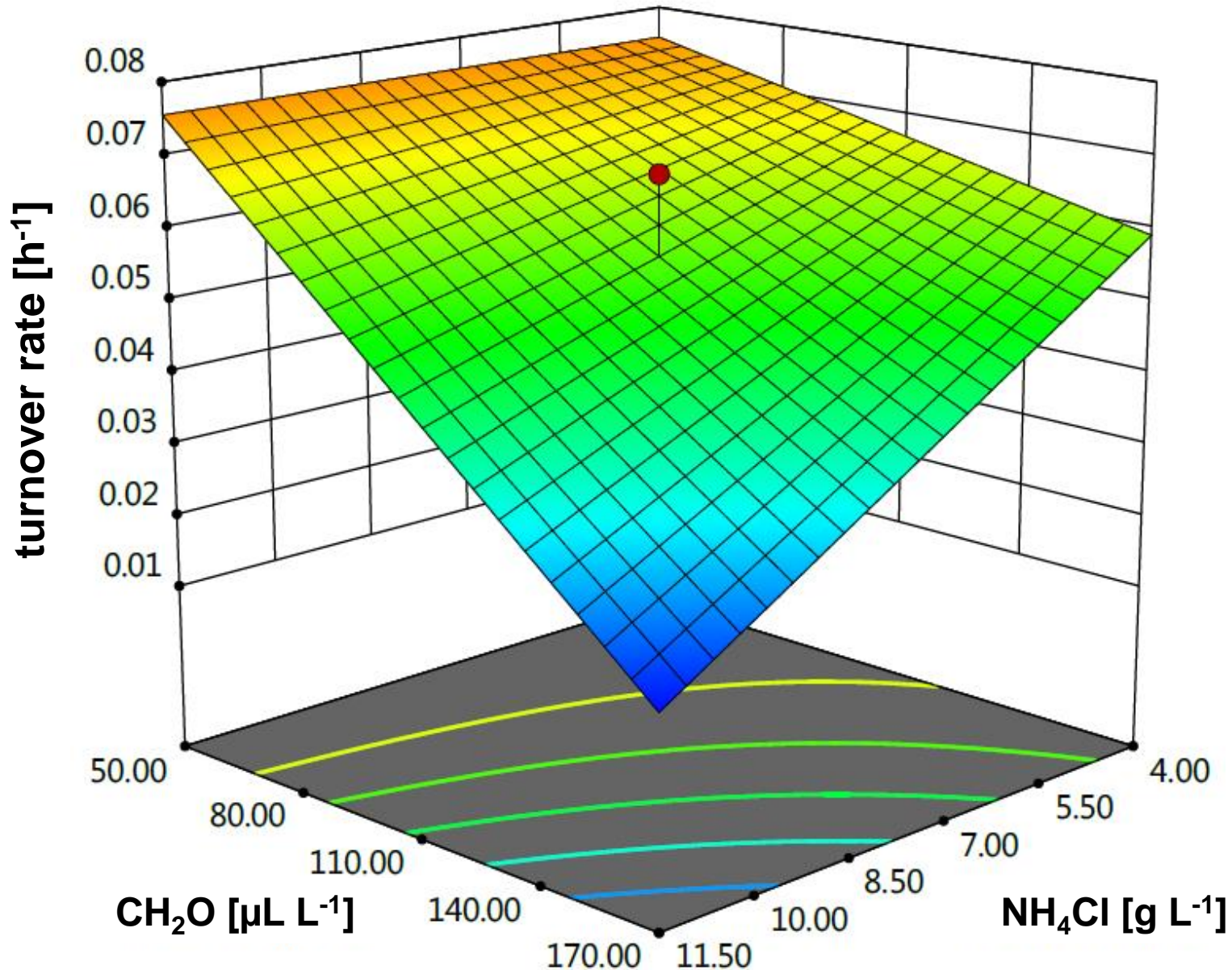
If factorial factors have to be added the central composite design will be duplicated for every combination of the categorical factor levels



# DoE – Examples closed batch



# DoE – Examples closed batch



Turnover rate in  $[\text{h}^{-1}]$  as function of  $\text{CH}_2\text{O}$  and  $\text{NH}_4\text{Cl}$  concentrations. The turnover rate reached its maximum value at low  $\text{CH}_2\text{O}$  concentration. At high  $\text{CH}_2\text{O}$  concentration the turnover rate is higher for low  $\text{NH}_4\text{Cl}$  concentrations. This study was based on a DoE approach.

# DoE – Examples batch

## Organism:

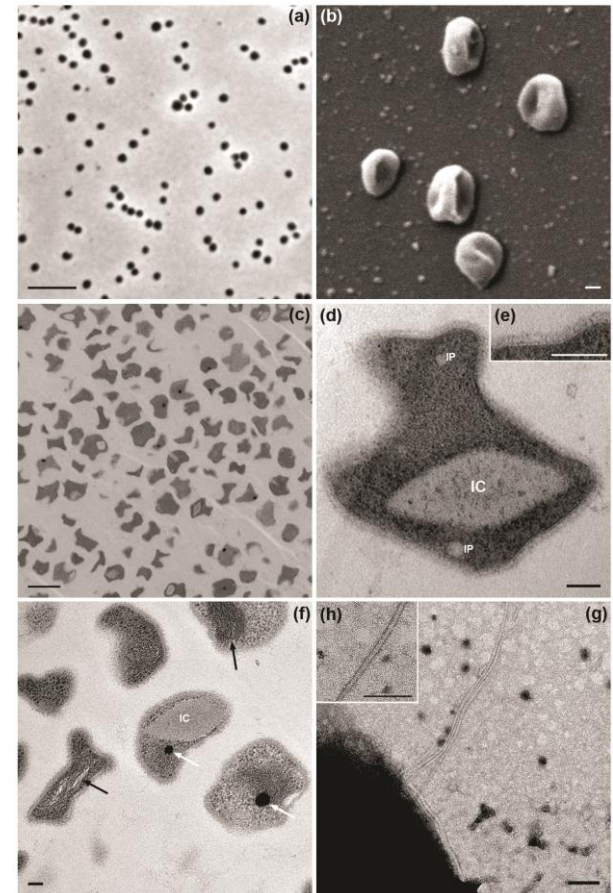
*Nitrososphaera viennensis*

## Factors:

- Ammonia concentration 1, 2.5 and 4 mM
- Pyruvate concentration 0.1, 0.8 and 1.5mM
- Temperature 37, 42 and 47 °C

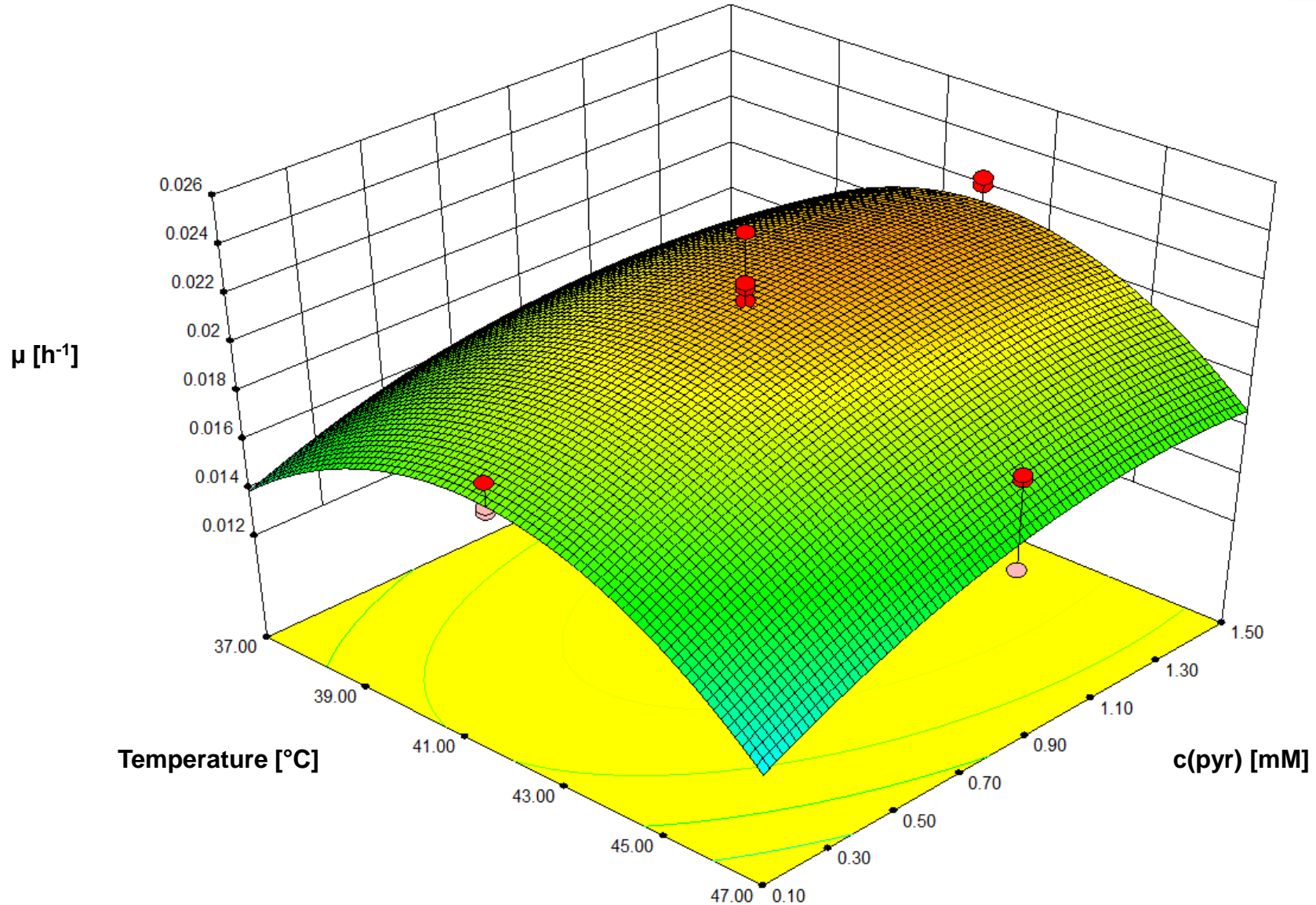
## Calculation of:

- $\text{NH}_4$  uptake rates [ $\text{mmol L}^{-1} \text{h}^{-1}$ ]
- $\text{NO}_2^-$  production rates [ $\text{mmol L}^{-1} \text{h}^{-1}$ ]
- Cell counts
- Specific growth rate [ $\text{h}^{-1}$ ] from  $\text{NO}_2^-$  production rate



Stieglmeier et al., 2014

# DoE – Examples batch

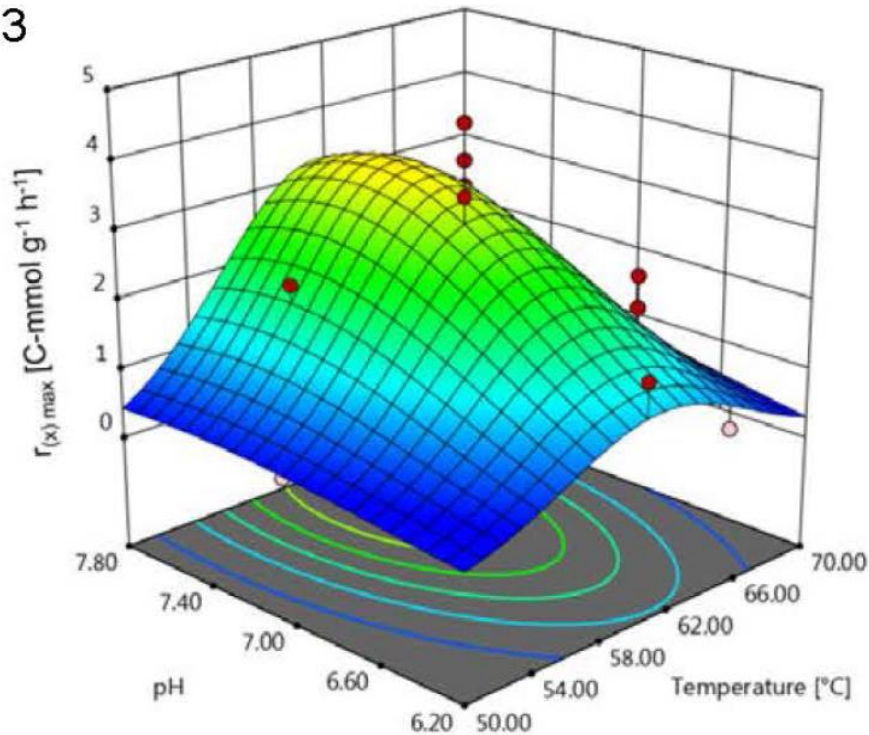


The graph illustrates the effect of pyruvate concentration ( $c(\text{pyr})$ ) [ $\text{mM}$ ] and temperature [ $^{\circ}\text{C}$ ] on the growth rate ( $\mu$ ) [ $\text{h}^{-1}$ ] of EN76<sup>T</sup> at a fixed ammonium concentration ( $c(\text{NH}_4^+)$ ) of 2.5  $\text{mM}$ . Based on the results of the closed batch cultivation and the subsequent generated response surface model (RSM), the optimal conditions for the cultivation of EN76<sup>T</sup> within this three-factorial design space could be retrieved. The optimal cultivation conditions using  $\mu$  as target value for maximization were calculated as follows:  $c(\text{pyr}) = 1.15$   $\text{mM}$ ,  $c(\text{NH}_4^+) = 2.03$   $\text{mM}$ , temperature = 42.02  $^{\circ}\text{C}$ , with a desirability of 0.854. Data points of the individual experiments are presented in red or rose colour.

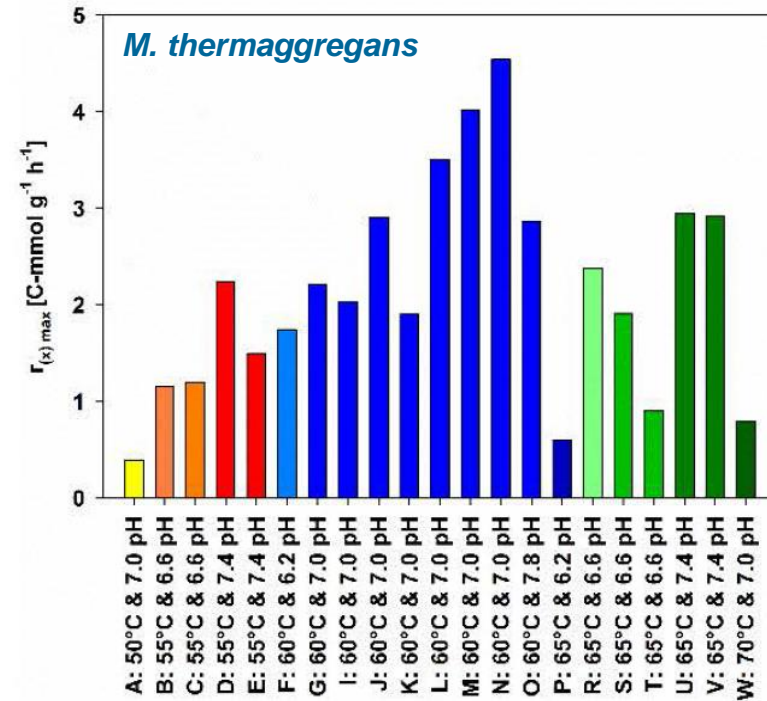
# DoE – Examples fed-batch



A.3



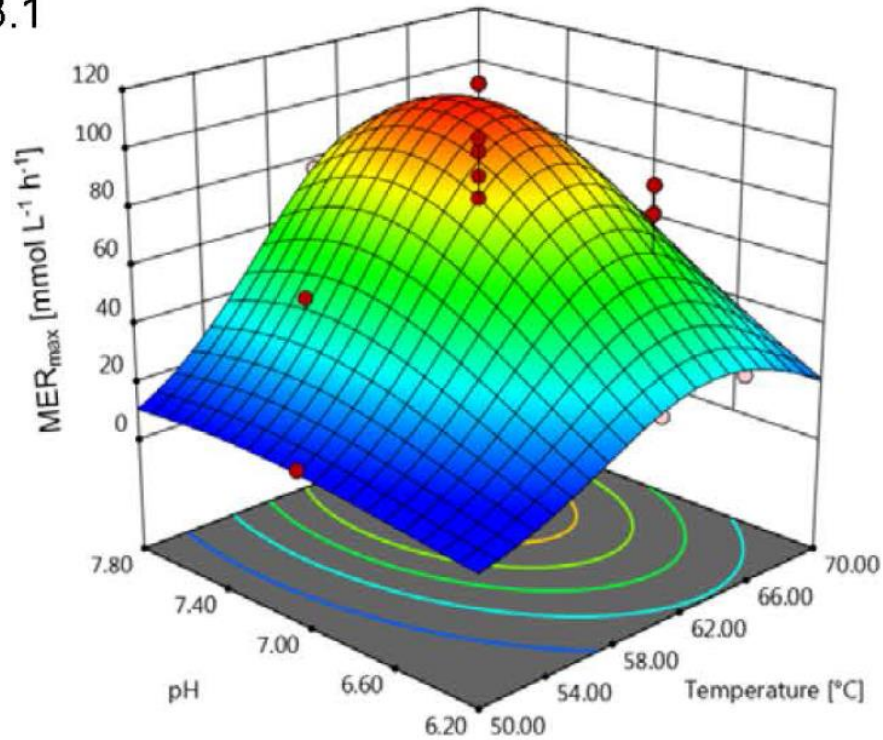
A.4



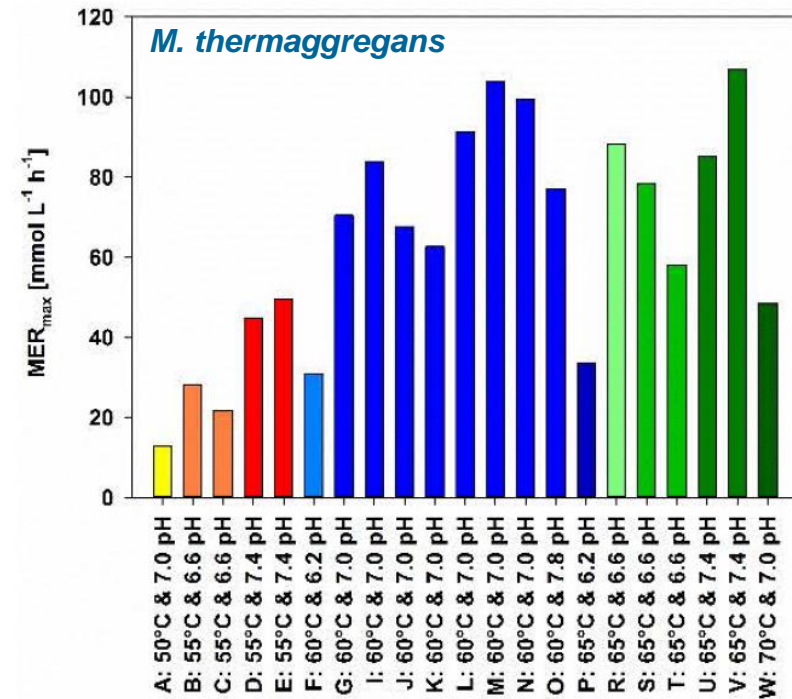
# DoE – Examples fed-batch



B.1



B.2

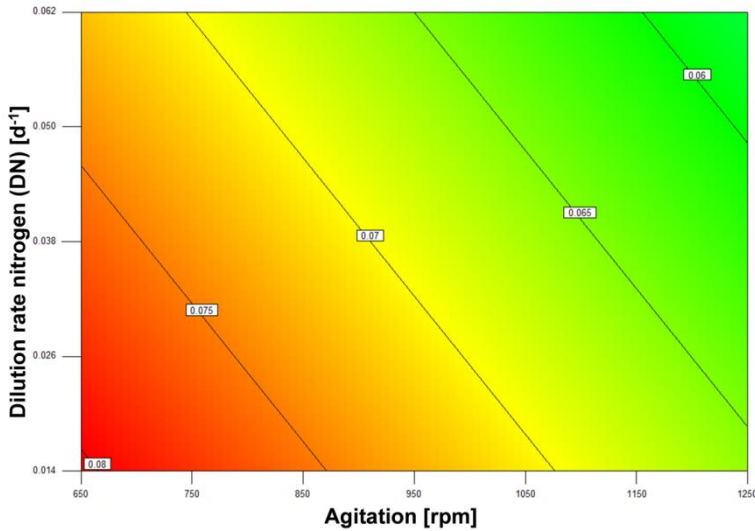


# DoE – Examples conti culture

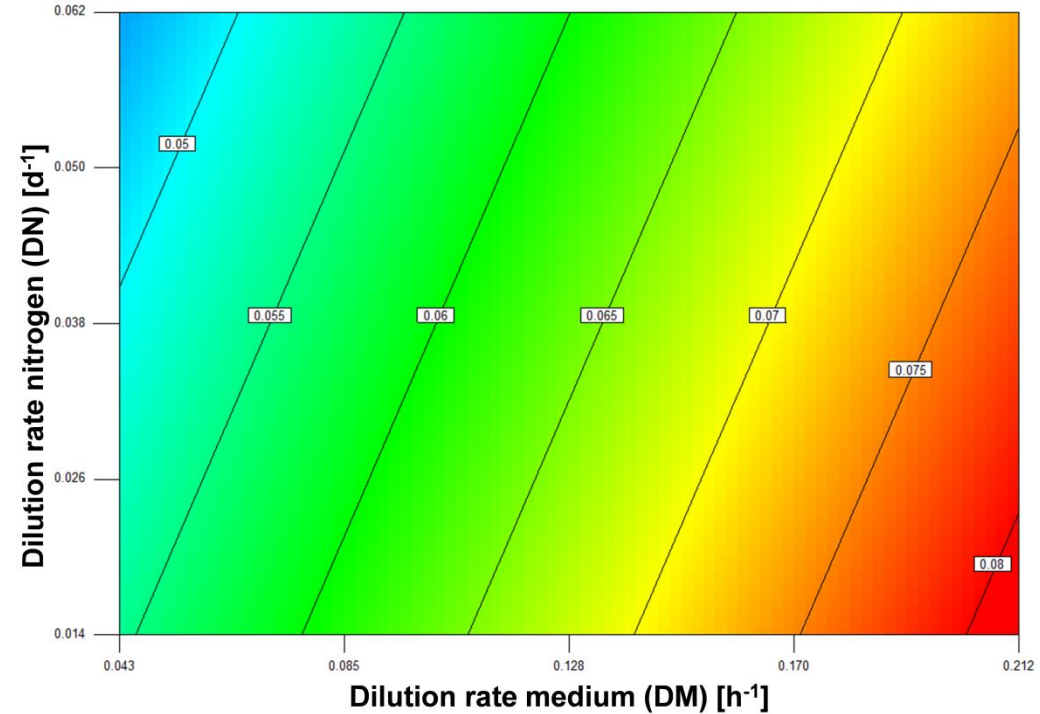


Run	DM [h <sup>-1</sup> ]	pH	DS [L L <sup>-1</sup> d <sup>-1</sup> ]	T [°C]	rpm	vvm [L L <sup>-1</sup> min <sup>-1</sup> ]	ratio (H <sub>2</sub> /CO <sub>2</sub> )	DN [L L <sup>-1</sup> d <sup>-1</sup> ]	C <sub>NH4+</sub> [mmol L <sup>-1</sup> ]	x [g L <sup>-1</sup> ]	MER [mmol L <sup>-1</sup> h <sup>-1</sup> ]	q <sub>CH4</sub> [mmol g <sup>-1</sup> h <sup>-1</sup> ]	CH <sub>4</sub> offgas [Vol.%]	Y <sub>(X/CH4)</sub> [C- mol/mol l]	r <sub>x</sub> [C- mmol L <sup>-1</sup> h <sup>-1</sup> ]	DoR-balance	C- balance	N- balance
1	0.043	6.16	0.012	60	654	0.16	3.0	0.014	54.2	0.92	16.4	17.8	4.5	0.07	1.21	96.8%	75.3%	84.1%
2	0.055	7.83	0.013	60	1243	0.19	4.9	0.051	111.9	1.35	45.1	33.4	13.6	0.05	2.25	95.7%	101.8%	142.3%
3	0.211	7.84	0.010	60	1242	0.49	3.0	0.019	26.6	1.14	105.0	91.9	11.6	0.07	7.35	98.5%	80.7%	84.5%
4	0.057	6.16	0.049	61	1243	0.50	5.0	0.016	37.4	3.80	114.0	30.0	12.9	0.06	6.73	94.6%	99.5%	95.0%
5	0.21	6.16	0.053	61	1245	0.20	3.0	0.042	58.5	0.88	71.4	80.9	28.4	0.08	5.72	101.9%	95.6%	103.5%
6	0.059	6.15	0.011	70	1242	0.50	3.0	0.062	128.7	2.76	99.2	36.0	10.5	0.05	4.96	97.2%	124.0%	108.3%
7	0.202	6.15	0.012	70	1245	0.20	5.1	0.016	38.2	0.79	65.2	82.8	23.8	0.08	4.89	103.3%	93.7%	82.8%
8	0.161	7.85	0.009	69	650	0.16	3.1	0.044	64.3	0.27	17.8	66.0	5.0	0.08	1.33	101.6%	96.6%	100.7%
9	0.056	7.85	0.044	70	1245	0.19	2.9	0.014	44.4	1.75	65.2	37.2	26.0	0.05	3.00	97.0%	95.1%	110.4%
10	0.207	7.84	0.051	69	1245	0.49	5.0	0.048	44.7	1.29	111.3	86.7	12.7	0.07	8.13	98.2%	110.0%	101.9%
11	0.110	6.98	0.033	63	951	0.28	4.0	0.034	47.8	1.30	60.7	46.7	11.7	0.07	4.37	101.1%	82.4%	92.3%
12	0.111	6.99	0.025	64	947	0.29	3.9	0.018	37.8	1.26	61.5	48.7	11.5	0.07	4.31	103.7%	82.1%	94.0%
13	0.114	6.99	0.026	65	950	0.30	4.0	0.017	49.0	1.16	54.6	47.0	9.4	0.07	4.04	96.7%	129.8%	109.1%
14	0.107	6.99	0.020	65	946	0.29	3.9	0.026	45.6	1.05	59.5	56.7	11.0	0.06	3.39	95.1%	106.0%	105.2%
15	0.061	6.14	0.055	70	1245	0.20	5.1	0.045	100.3	1.77	67.8	38.2	25.8	0.05	3.32	101.1%	90.9%	109.3%
16	0.065	5.53	0.010	67	1242	0.49	2.9	0.055	96.6	1.98	99.2	50.0	10.7	0.04	3.97	95.4%	71.2%	112.5%
17	0.064	8.41	0.053	68	1242	0.19	2.9	0.004	18.2	2.06	66.4	32.2	27.1	0.06	4.01	106.0%	76.0%	93.0%
18	0.212	5.6	0.059	59	1242	0.19	2.9	0.047	39.7	0.84	71.2	85.0	31.5	0.08	5.43	103.5%	85.4%	84.3%

Multivariate model generation from a nona-factorial DoE



Plot of nitrogen dilution rate (DN) [d<sup>-1</sup>] versus medium dilution rate (DM) [h<sup>-1</sup>] in order to analyze growth to product yield ( $Y_{(x/CH_4)}$ ). Individual levels of  $Y_{(x/CH_4)}$  are indicated through lines and boxes within the graph. The analysis shows that  $Y_{(x/CH_4)}$  varies by adjusting DN, DM, or both. An increase of DN reduces  $Y_{(x/CH_4)}$ . However, an increase of DM increases  $Y_{(x/CH_4)}$ .



Plot of the nitrogen dilution rate (DN) versus the agitation speed in order to analyze  $Y_{(x/CH_4)}$  [C-mol/mol]. Individual levels of  $Y_{(x/CH_4)}$  are indicated through lines and boxes within the graph.  $Y_{(x/CH_4)}$  is highest at the lowest investigated range of both factors.



- **Modde (Umetrics, Sweden)**
- **Design Expert (Stat-Ease Inc., USA)**
- **Statistica (StatSoft, USA)**
- **R Commander**