

The mathematics behind Computertomography PD Dr. Swanhild Bernstein, Institute of Applied Analysis, Freiberg University of Mining and Technology, International Summer academic course 2008, "Modelling and Simulation of Technical Processes"



first row left: image fusion of CT and MRI first row right: Computertomography (CT) second row right: Magnetic Resonance Imaging (MRI) second row left: tumor search



### Historical remarks

- $\bullet$  C. Röntgen (1895) X-rays
- J. Radon (1917)– Mathematical Model
- G. Grossmann (1935) Tomography
- G. Hounsfield, McCormack (1972) Computerized assited tomography (CAT scan)



Abb. 1.4: moderner CT Scanner



Abb. 1.1: historischer Grossmann-Tomograph

Why does it work? The physical priniples.

- Tomography means *slice imaging,*
- Quantification of the tendency of objects to absorb or scatter x-rays by the *attunation coefficient,* involving *Beer's law.*



## Model

• *No refraction or diffraction:* X-ray beams travel along straight lines that are not "bent" by the objects they pass through.

This is a good approximation because x-rays have very high energies, and therefore very short wavelength.

 *The X-rays used are monochromatic:* The waves making up the x-ray beams are all of the same frequency.

This is not a realistic assumption, but it is needed to construct a *linear model* for the measurements.



## Model

- *Beer's law:* Each material encountered has a characteristic linear attenuation coefficient μ for x-rays of a given energy.
- The *intensity*, *I* of the x-ray beam satisfies Beer's law:

$$
\frac{dI}{ds} = -\mu(x)I
$$

Here, s is the arc-length along the straight line trajectory of the x-ray beam.



# The failure to distinguish objects



one object two objects same projection

#### Solution: more directions



Different angles lead to different projections. The more directions from which we make measurement, the more arrangements of objects we can distinguish.

### Analysis of a Point Source Device, 2D model, what do we measure?



A point source device for measuring line integrals of the attenuation coefficient.



### 2D model, what do we measure?

Beer's law:  $\frac{dI}{dr} = -\left(\mu_a(r,\phi) + \frac{1}{r}\right)I$ 

First order ordinary differential equation for the intensity I with boundary condition I at  $r=r_0>0$  equals  $I_0$ .

$$
\ln \frac{I(r_{\phi}, \phi)}{I(r_0, \phi)} = \ln \frac{r_0}{r_{\phi}} - \int_{a_{\phi}}^{b_{\phi}} \mu_a(s, \phi) ds
$$



# Analysis if a Point Source Device

The density of the developed film at a point is proportional to the logarithm of the total energy incident at that point:

density of the film =  $y \times \log$  (total energy intensity), where  $\gamma$  is a constant, we obtain:

$$
-\int_{a_{\phi}}^{b_{\phi}} \mu_a(s, \phi) ds = \gamma^{-1} \delta(\phi) - \ln \left[ \frac{I_0 \cos^2 \phi}{2\pi (L+l)} \right]
$$

This formula expresses the measurements as *linear function* of the attunation coefficient.



#### Oriented lines



t is the distant of the line from the origin, s is the parameter of the line.









$$
\mathcal{R}f(t, \vec{\theta}) = \int_{g_{t, \vec{\theta}}} f ds = \int_{-\infty}^{\infty} f(s\vec{\theta}^{\perp} + t\vec{\theta}) ds
$$

 The Radon transform can be defined, a priori for a function, f whose restriction to each line is *locally integrable* and

$$
\int_{-\infty}^{\infty} |f(s\vec{\theta}^{\perp} + t\vec{\theta})| ds < \infty, \quad \text{for all} \quad (t, \vec{\theta}) \in \mathbb{R} \times S^1.
$$

- This is really two different conditions:
- 1. The function is regular enough so that restricting it to any line gives a locally integrable function,
- 2. The function goes to zero rapidly enough for the improper integrals to converge.

In applications functions of interest are usually piecewise continuous and zero outside of some disk.

# Properties of the Radon transform • The Radon transform is linear:  $\mathcal{R}(af) = a\mathcal{R}f$  for all  $a \in \mathbb{R}$ ,  $\mathcal{R}(f+g) = \mathcal{R}f + \mathcal{R}g.$ The Radon transform of f is an even function:

$$
\mathcal{R}f(t,\vec{\theta}) = \mathcal{R}f(-t, -\vec{\theta}).
$$

• The Radon transform is monotone: if f is a non-negative function then

$$
\mathcal{R}f(t,\vec{\theta}) \ge 0 \quad \text{for every} \quad (t, \vec{\theta}).
$$

#### Pencilgeometry (Nadelstrahlgeometrie)



## Back-projection formula

• It is difficult to use the line integrals of a function directly to reconstruct the function:

$$
\tilde{f}(\vec{x}) = \frac{1}{2\pi} \int_0^{2\pi} \mathcal{R}f(\langle \vec{x}, \vec{\theta} \rangle, \theta) d\theta
$$



• Results of the recontruction by back-projection What is that??



# Fourier transform in 1D

• The Fourier transform of an absolutely integrable function f, defined on the real line, is

$$
\hat{f}(\xi) = \int_{-\infty}^{\infty} f(x) e^{-i\xi x} dx
$$

• Suppose that the Fourier transform of f is again an absolutely integrable function then

$$
f(x) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{f}(\xi) e^{i\xi x} d\xi.
$$



# Square integrable functions

• A (complex-valued) function f, defined on  $\mathbb{R}^n$ , is square integrable if

$$
||f||_{L^{2}}^{2} = \int_{\mathbb{R}^{n}} |f(\vec{x})|^{2} d\vec{x} < \infty.
$$

Examples: The function  $f(x) = (1 + |x|)^{-\frac{3}{4}}$  is not absolutely integrable but square integrable, the function

$$
g(x) = \begin{cases} \frac{1}{\sqrt{|x|}}, & |x| < 1, \\ 0, & \text{elsewhere.} \end{cases}
$$

is absolutely integrable but not square integrable.

# Fourier transform in nD

• The Fourier transform of an absolutely integrable function is defined by

$$
\hat{f}(\vec{\xi}) = \int_{\mathbb{R}^n} f(\vec{x}) e^{-i\langle \vec{\xi}, \vec{x} \rangle} d\vec{x} \n= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(x_1, \dots, x_n) e^{-ix_1\xi_1} dx_1 \dots e^{-ix_n\xi_n} dx_n.
$$

• Let 
$$
f \in L^2(\mathbb{R}^n)
$$
 and define  
\n
$$
f_R(\vec{x}) = \frac{1}{(2\pi)^n} \int_{|\xi| < R} \hat{f}(\vec{\xi}) e^{i\langle \vec{x}, \vec{\xi} \rangle} d\vec{\xi}
$$

then  $f = \lim_{R \to \infty} f_R$ .

• Parseval formula: If f is square integrable then

$$
\int_{\mathbb{R}^n} |f(\vec{x})|^2 d\vec{x} = \frac{1}{(2\pi)^n} \int_{\mathbb{R}^n} |\hat{f}(\vec{\xi})|^2 d\vec{\xi}.
$$



# Central Slice Theorem

 Let f be an absolutely integrable function. For any real number r and unit vector  $\vec{\theta}$ , we have the identity

$$
\widetilde{\mathcal{R}f}(t,\,\theta)=\int_{-\infty}^{\infty}\mathcal{R}f(t,\,\vec{\theta})\,e^{-itr}\,dt=\hat{f}(r\vec{\theta}).
$$

- For a given vector  $\vec{\xi} = (\xi_1, \xi_2)$  the inner product  $\langle \vec{x}, \vec{\xi} \rangle$ is constant along any line perpendicular to the direction  $\vec{\xi}$ . The central slice theorem interprets the compution of the Fourier transform of  $\vec{\xi}$  as a two-step process:
- 1. First, integrate the function along lines perp. to  $\vec{\xi}$ .
- 2. Compute the *one-dimensional* Fourier transform of this function of the affine parameter.



- 1. Choose a line L, determined by the direction  $\vec{\theta}$  (Cartesian coord.) or by the angle  $\gamma$ . Then the coorinate axis ξ shows in the same direction.
- 2. Integrate along all lines perp. to  $\vec{\theta}$  (those lines are parallel to the cood. axis η. We obtain the Radon transform  $p_{\gamma}(\xi)$ .
- 3. Compute the *one dimensional*
- Fourier transform  $\hat{p}_{\gamma}(q)$  of  $p_{\gamma}(\xi)$
- 4. With u=q cos  $\gamma$  and v=q sin  $\gamma$ , we get  $F(u,v) = \hat{p}_{\gamma}(q)$  and f(x,y) is equal to the *2D* inverse Fourier transform of F(u,v).











#### In Cartesian coordinates.







#### In Polar coordinates.







Abdomen, Radon transform in Cartesian coord.



Now, we can try to do some reconstruction by the before mentioned procdure



#### based on 1 projection.





#### based on 4 projections.





#### based on 8 projections.





#### based on 30 projections.





based on 60 projections.

What is the difference to the back-projection formula?

# Radon Inversion Formula

 If f is an absolutely integrable function and ist Fourier transform is absolutely integrable too, then

$$
f(\vec{x}) = \frac{1}{(2\pi)^2} \int_0^{\pi} \int_{-\infty}^{\infty} e^{ir\langle \vec{x}, \vec{\theta} \rangle} \widetilde{\mathcal{R}} f(r, \vec{\theta}) |r| dr d\vec{\theta}.
$$

# Radon Inversion Formula

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$$

- **Filtered Back-Projection**
- 1. The radial integral is interpreted as a *filter* applied to the Radon transform. The filter acts only the affine parameter; is output of the filter is denoted

$$
\mathcal{GR}(t, \vec{\theta}) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \widetilde{\mathcal{R}f}(r, \vec{\theta}) e^{irt} |r| dr.
$$

2. The angular integral is then interpreted as the backprojection of the *filtered* Radon transform.

$$
f(\vec{x}) = \frac{1}{2\pi} \int_0^{\pi} (\mathcal{GR}) (\langle \vec{x}, \vec{\theta} \rangle, \vec{\theta}) d\vec{\theta}.
$$





#### back-projection **filtered** back-projection based on 1 projection



#### back-projection **filtered** back-projection based on 3 projections





#### back-projection **filtered** back-projection based on 10 projections



#### back-projection **filtered** back-projection based on 180 projections





#### back-projection **filtered** back-projection based on 180 projections



a) back-projection and b) filtered back-projection, based on 1, 2, 3, 10, 45 projections resp.

# Different Inversion formulas

We already had the Radon inversion formula:

$$
f(\vec{x}) = \frac{1}{(2\pi)^2} \int_0^{\pi} \int_{-\infty}^{\infty} e^{ir\langle \vec{x}, \vec{\theta} \rangle} \widetilde{\mathcal{R}} f(r, \vec{\theta}) |r| dr d\vec{\theta}.
$$

• We write | r| as sgn(r) r :

 $f(\vec{x}) = \frac{1}{(2\pi)^2} \int_0^{\pi} \int_{-\infty}^{\infty} e^{ir\langle \vec{x}, \vec{\theta} \rangle} \widetilde{\mathcal{R}f}(r, \vec{\theta}) \operatorname{sgn}(r) r dr d\vec{\theta}$ 

# A Different Inversion formula

We already had the Radon inversion formula:

$$
f(\vec{x}) = \frac{1}{(2\pi)^2} \int_0^{\pi} \int_{-\infty}^{\infty} e^{ir\langle \vec{x}, \vec{\theta} \rangle} \underbrace{\widetilde{\mathcal{R}f}(r, \vec{\theta})}_{\text{sgn}} \text{sgn}(r)
$$

• Where we write | r| as sgn(r) r  $\bullet$   $\mathcal{F}_{t\rightarrow r}$  denotes the 1D Fourier transform with respect to t.

$$
\left(\frac{1}{i}\mathcal{F}_{t\to r}\left(\frac{d}{dt}(\mathcal{R}f)(t, \vec{\theta})\right)\right)
$$

 $drd\theta$ 

• Suppose that g is square integrable on the real line. The Hilbert transform  $H$  of g is defined by  $\mathcal{H}q = \mathcal{F}^{-1}(\text{sgn}\,\hat{q}).$ 

If  $\hat{g}$  is also absolutely integrable, then

$$
\mathcal{H}g(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{g} \operatorname{sgn}(r) e^{itr} dr.
$$

We obtain 
$$
f(\vec{x}) = \frac{1}{2\pi i} \int_0^{\pi} \mathcal{H}(\partial_t \mathcal{R}f)(\langle \vec{x}, \vec{\theta} \rangle, \vec{\theta}) d\vec{\theta}.
$$

# Mathematical Model for CT

 We consider a two-dimensional slice of an three-dimensional object, the physical parameters of interest is the attenuation coefficient f of the two-dimensional slice. According to *Beer's law*, the intensity traveling along a line is attenuated according to the differential equation  $dL =$ 

$$
\frac{dI(t,\theta)}{ds} = -f I_{(t,\vec{\theta})},
$$

where s is arclength along the line.

 By comparing the intensity of an incident beam of x-rays to that emitted, we *measure* the *Radon transform* of f:

$$
\mathcal{R}f(t, \vec{\theta}) = -\log \left[\frac{I_{0,(t, \vec{\theta})}}{I_{i,(t, \vec{\theta})}}\right]
$$

 Using the Radon inversion formula, the attenuation coefficient f is reconstructed from the *measurements*  $\mathcal{R}f$ .



#### First generation CT scanner

- Single detector
- Translate rotate acquisition
	- Translates across patient
	- Rotates around patient
- Very slow
	- minutes per slice



#### Second generation CT scanner

- Narrow fan beam  $(10^{\circ})$ ٠
- Multiple detectors ٠
- Multiple angle acquisition ٠ at each position
	- Larger angle rotate
	- Translate still required
- Slow
	- $-20s$  per slice





#### Third generation CT scanner

- Fan beam
- Multiple (500 1000) rotating detectors
- Rotation only
	- no translation required
- Much faster
	- $-$  as fast as 0.5 s per rotation
- Most common modern scanner design





#### Fourth generation CT scanners

- Fan beam
- Static detectors all round gantry
- Only tube rotates
- Avoids ring artefact problems of 3rd generation scanners



## Radon transform - Polar grid Fourier transform – Cartesian grid





# Why fan beam?

#### Re-binning fan beam data

- 3rd generation CT scanners ٠ use a fan beam to measure projection data
- To get parallel projections, data from adjacent detectors in subsequent views can be combined



### Reconstruction Algorithm for a Parallel Beam Machine

 We assume that we can measure *all* the data from a finite set of equally spaced angles. In this case data would be

$$
\{\mathcal{R}f(t, k\Delta\theta): k = 0, \ldots M, \quad t \in [-L, L]\}, \quad \Delta\theta = \frac{\pi}{M+1}.
$$

 With these data we can apply the central slice theorem to compute angular samples of the two-dimensional Fourier transform of f,

$$
\hat{f}(r, \vec{\theta}(k\Delta\theta)) = \int_{-\infty}^{\infty} \mathcal{R}f(t, \vec{\theta}(k\Delta\theta))e^{-irt} dt.
$$

 Using the two-dimensional Fourier inversion formula and using a Riemann sum in the angular direction gives

$$
f(x,y) \approx \frac{1}{4\pi(M+1)} \sum_{k=0}^{M} \int_{-\infty}^{\infty} \hat{f}(r\vec{\theta}(k\Delta\theta)) e^{ir\langle (x,y),\vec{\theta}(k\Delta\theta)\rangle} |r| dr.
$$



## Concluding remarks

- The model present here is a CT-model, there exist other types of tomographical methods that are based on other mathematical models.
- All mathematical models are based on so-called integral geometry and connected with wave equations.
- Modern tomography even combines different methods:



 fusion of CT-scan (grey) and PET-scan (grey) PET = Positron Emission Tomography

*http://www.sdirad.com/PatientInfo/pt\_pet.htm*

# Concluding remarks

Most of the pictures are dealing with medical applications but Computer tomography can be applied to more applications, as for example:

#### *Material sciences*

Tomographic visualisation of a metallic foam structure *http://www2.tu-berlin.de/fak3/sem/GB\_index.html*

#### *Geology*

*http://www.geo.cornell.edu/geology/classes/Geo101/ 101images\_spring.html* Seismic tomography reveals a more complex interior structure.

#### *Archeology*

3D-Computer Tomography of Prehispanic Sound Artifacts.



Supported by the Ethnological Museum Berlin and the St. Gertrauden Hospital, Berlin. *http://www.mixcoacalli.com/wp-content/uploads/2007/09/ct2.jpg*







# Bibliography

- Charles L. Epstein, *Introduction to the Mathematics of Medical Imaging,* Pearson Education, Inc., 2003
- Thorsten M. Buzug, *Einführung in die Computertomographie,* Springer Verlag, 2004
- Esther Meyer, *Die Mathematik der Computertomogrphie,*  Seminarvortrag, *www1.am.unierlangen.de/~bause/Seminar/seminar.html*
- Other pictures are from *www.impactscan.org/slides/impactcourse/basic\_principles\_of\_ct/ www.sdirad.com/PatientInfo/pt\_pet.htm*