

The matrix formalism for light propagation in layered structures.

The propagation of light in a layered structure of homogeneous media with planar interfaces produces no diffraction, and can, hence, be described by impact (E_i), reflected (E_r) and transmitted (E_t) wave amplitudes of the electric field using simple matrix formalism (see Fig. 1):

$$\begin{bmatrix} E_i \\ E_r \end{bmatrix} = \mathbf{V}_0^{-1} \mathbf{R}_1^{-1} \dots \mathbf{R}_m^{-1} \mathbf{V}_f \begin{bmatrix} E_t \\ 0 \end{bmatrix} \equiv \mathbf{P} \begin{bmatrix} E_t \\ 0 \end{bmatrix}, \quad (1)$$

where matrices \mathbf{R}_j , $j=1\dots m$, belong to j -th layer of the structure and matrices \mathbf{V} are connected with substrate (index 0) and ambient (index f).

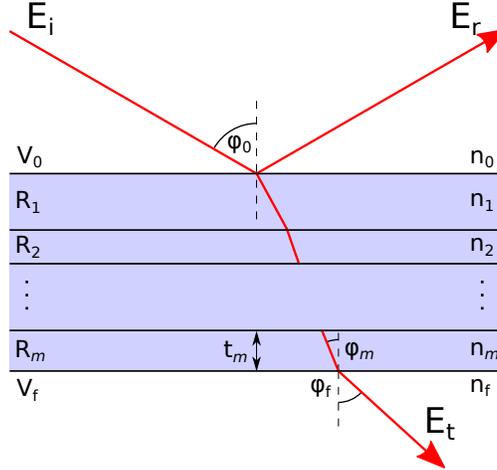


Fig. 1: Notation for light propagation through a layered structure. In SPR measurements, the light is impacting from substrate.

The expression

$$\mathbf{R}_j^{-1} = \begin{pmatrix} \cos\theta_j & -\frac{i \sin\theta_j}{\tilde{n}_j} \\ -i\tilde{n}_j \sin\theta_j & \cos\theta_j \end{pmatrix} \quad (2)$$

is formally polarization independent and $\det \mathbf{R}_j = 1$. Note, however, that definition of effective index of refraction \tilde{n}_j within the j -th layer is polarization dependent itself:

$$s : \tilde{n}_j = n_j \cos \varphi_j \quad p : \tilde{n}_j = \frac{n_j}{\cos \varphi_j}, \quad (3)$$

where n_j is the index of refraction of j -th layer. For angle φ_j at which the j -th layer is propagated the Snell's law brings

$$\cos \varphi_j = \sqrt{1 - \left(\frac{n_0}{n_j} \sin \varphi_0 \right)^2}; \quad (4)$$

analogical formula can be used to obtain the angle φ_f in the ambient. The phase θ_j acquired within the j -th layer is given by

$$\theta_j = 2\pi \frac{t_j}{\lambda} n_j \cos \varphi_j, \quad (5)$$

where t_j is the thickness of the j -th layer and λ is the vacuum wavelength of incident light. For the \mathbf{V} matrices we generally have

$$s : \mathbf{V} = \begin{pmatrix} 1 & 1 \\ \tilde{n} & -\tilde{n} \end{pmatrix} \quad p : \mathbf{V} = \cos \varphi \begin{pmatrix} 1 & 1 \\ \tilde{n} & -\tilde{n} \end{pmatrix},$$

which brings

$$s : \mathbf{V}_f = \begin{pmatrix} 1 & 1 \\ \tilde{n}_f & -\tilde{n}_f \end{pmatrix} \quad p : \mathbf{V}_f = \cos \varphi_f \begin{pmatrix} 1 & 1 \\ \tilde{n}_f & -\tilde{n}_f \end{pmatrix}, \quad (6)$$

$$s : (\mathbf{V}_0)^{-1} = \frac{1}{2\tilde{n}_0} \begin{pmatrix} \tilde{n}_0 & 1 \\ \tilde{n}_0 & -1 \end{pmatrix} \quad p : (\mathbf{V}_0)^{-1} = \frac{1}{2\tilde{n}_0 \cos \varphi_0} \begin{pmatrix} \tilde{n}_0 & 1 \\ \tilde{n}_0 & -1 \end{pmatrix}. \quad (7)$$

The overall propagation matrix \mathbf{P} from eq. (1) allows to compute the complex reflectivity (distinguishing r_s and r_p by the appropriate entries of \mathbf{P} for each of the polarizations) as well as the complex reflectance ratio $\rho=r_p/r_s$. To this end, we will denote the polarization-dependent components of \mathbf{P} by the respective index:

$$p : \mathbf{P} \equiv \begin{pmatrix} a_p & b_p \\ c_p & d_p \end{pmatrix} \quad s : \mathbf{P} \equiv \begin{pmatrix} a_s & b_s \\ c_s & d_s \end{pmatrix},$$

so that $r_s=c_s/a_s$, $r_p=c_p/a_p$ and $t_s=1/a_s$, $t_p=1/a_p$. Consequently,

$$R = rr^*, \quad \text{but} \quad T = \frac{n_f \cos \varphi_f}{n_0 \cos \varphi_0} tt^*.$$